# Iron Working Debris from Elms Farm, Heybridge, Essex

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#### Introduction

The site at Elms Farm, Heybridge, Essex (NGR TL847082) is a Roman settlement at the head of the Blackwater estuary. An area totalling 21 hectares across the eastern half of the settlement was investigated by Essex County Council Field Archaeology Unit on behalf of Bovis Homes and English Heritage. A range of features were excavated including roads, ditches, pits, post-holes and buildings and occupation continued from the late pre-Roman Iron Age through to the early Saxon period. The site is interpreted as a 'market village' (Atkinson & Preston 1998: 109).

### **Excavation Strategy/Collection Policy**

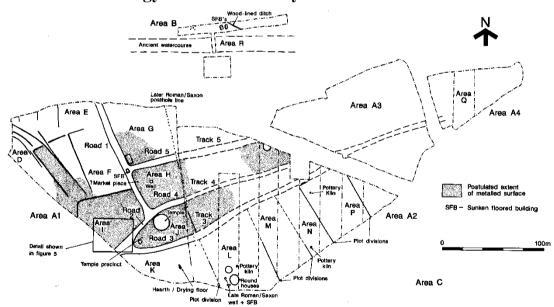


Figure 1. Plan of the main excavated area at Elms Farm, Heybridge showing areas D-R (After Atkinson & Preston 1997: fig 4, drawn by Iain Bell)

Initially, areas were mechanically stripped and all features were sampled by hand excavation. However, the density and complexity of deposits were greater than expected and the excavation strategy was altered with partial striping and selective sampling of features identified. In some cases, the areas stripped and sampled were selected to investigate good survival of stratigraphy, while in others the areas were

alternate 20 m strips to provide a 'random' sample (see figure 1). While the total area excavated was large and a large quantity of material was recovered there may be biases which will affect attempts to compare different areas.

Numerous hearths were excavated although the exact function of these was not always clear; many were probably domestic rather than industrial. Metal working wastes, including hammerscale) were recovered from a number of secondary contexts (ditches, pits, etc) especially in the southern part of the site. No metal working debris was found in primary contexts.

### **Nature of Occupation**

The site comprises a temple complex at the centre of a road and trackway network with numerous domestic and industrial features (round houses, ditches, pits, gullies, kilns, etc). Occupation commences in the late pre-Roman Iron Age and continues into the early Saxon period (see table 1). The Roman occupation at the site has conventionally been characterised as a 'small' or minor town (e.g. Rodwell 1975) with port facilities (Wickenden 1986). The recent excavations, however, suggest that the occupation was principally agricultural albeit with a local religious significance (Atkinson & Preston 1997: 109).

I	Middle/Late Iron Age transition	
II	Late Pre-Roman Iron Age	Mid 1 <sup>st</sup> century BC – mid 1 <sup>st</sup> century AD
III	Early Roman	Late 1 <sup>st</sup> century AD – mid 2 <sup>nd</sup> century AD
IV	Mid Roman	Late 2 <sup>nd</sup> century AD – mid 3 <sup>rd</sup> century AD
V	Late Roman	Late 3 <sup>rd</sup> century AD – mid 4 <sup>th</sup> century AD
VI	Latest Roman – Early Saxon	Late 4 <sup>th</sup> century AD – 5 <sup>th</sup> century AD
VII	Later	6 <sup>th</sup> century – present

Table 1. Summary of phasing

# **Summary of results**

The metalworking debris was categorised on criteria of morphology, density, colour and vesicularity and each category was separately weighed. It should be stressed that many categories of iron working slags form part of a compositional and morphological continuum. Only certain classes of material are strictly diagnostic and can be unambiguously assigned to a single metalworking process. Others may derive from a restricted range of processes but, when found in association with the diagnostic types, may provide support for the identification of these activities. Categories and the criteria on which they are based may vary between specialists; those currently used by the Centre for Archaeology are defined below.

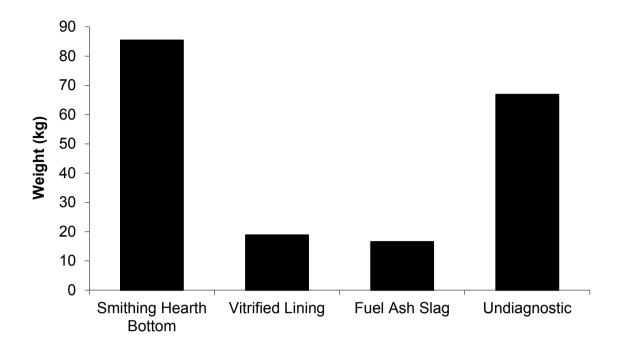


Figure 2. Weights of all metal working debris from Elms Farm, Heybridge

A total of 187.727kg of metal working (and possible metal working) debris has been identified. The categories which have been identified from Elms Farm are smithing hearth bottoms, vitrified lining, undiagnostic and fuel ash slag. Significantly no slags diagnostic of iron smelting were identified. The proportions of the categories of metal working debris identified are shown in figure 1. All of the debris which is diagnostic of a particular process was produced by iron smithing.

### **Explanation of classification**

In the debris from Elms Farm, Heybridge, evidence for smithing was recognised in two main forms; bulk slags and micro slags. Of the bulk slags produced during smithing only the **smithing hearth bottoms** are unlikely to be confused with the waste products of smelting and are therefore considered to be diagnostic of smithing. These hearth bottoms are recognisable by their characteristic plano-convex form, having a rough convex base and a smoother, vitrified upper surface which is flat, or even slightly hollowed as a result of the downwards pressure of the air blast. Compositionally, smithing hearth bottoms are predominantly fayalitic (iron silicate) and form as a result of high temperature reactions between the iron, iron-scale and silica from either the clay furnace lining or sand used as a flux by the smith.

In addition to bulk slags, iron smithing also produces micro slags of two types. Flake hammerscale consists of fish-scale like fragments of the oxide/silicate skin of the iron dislodged during working. Spheroidal hammerscale results from the solidification of small droplets of liquid slag expelled during working, particularly when two components are being fire welded together or when a slag-rich bloom of iron is first worked into a billet or bar. Hammerscale is considered important in

interpreting a site not only because it is highly diagnostic of smithing but, because it is often allowed to build up in the immediate vicinity of the smithing hearth and anvil, it may give a more precise location of the activity than the bulk slags which may be transported elsewhere for disposal.

Three categories of slag not considered diagnostic are undiagnostic iron working slag, vitrified hearth lining and fuel ash slag. The debris classed as undiagnostic iron working slag is dense (having a composition which is predominantly favalitic) but the morphology of the slag lumps is irregular and similar materials may be produced by either smelting or smithing operations. Material listed as vitrified hearth/furnace **lining** can be formed during either iron smelting, iron smithing or non-ferrous metal working as a result of a high temperature reaction between the clay lining of the hearth/furnace and the alkali fuel ashes or fayalitic slag. The material consists of unmodified clay on one surface and vitrified clay on the other. Occasionally original blow hole is preserved in the vitrified linings. The lack of smelting slags from the site indicates that the vitrified linings derive from smithing hearths rather than smelting furnaces. Some of the vitrified hearth lining may derive from non-ferrous alloy working. The occasional slagged stones found may also have formed part of metal working hearths. Fuel ash slag is a very lightweight, light coloured (grey-brown), highly porous material which results from the reaction between alkaline fuel ash and silicates from soil, sand or clay at elevated temperatures. The reaction is shared by many pyrotechnological processes and the slag is not diagnostic.

The assemblage submitted for examination included some non-metallurgical: ferruginous concretions, iron artefacts, pottery and quern fragments. These were separated and are not reported on here. **Ferruginous concretions** form as a result of the re-deposition of iron hydroxides, similar to the natural phenomenon of iron panning, although the process is likely to be enhanced when nearby archaeological deposits contain iron-rich waste. Where testing with a magnet or high density/surface cracking indicated the presence of metallic iron, material was classified as **iron objects.** 

### **Chronological Distribution of Debris**

140kg of the iron working debris could be assigned to individual phases; the remainder was unstratified or came from features which could not be assigned to a single phase. The total weights of slag for each phase are shown in figure 2. A single fragment of vitrified lining (20g) came from the earliest phase of activity (I: the Middle/Late Iron Age transition). Most of the debris was recovered from phase II or III contexts (Late Iron Age–Early Roman).

The concentration of metalworking debris in phases II and III is underlined by the high proportion of vitrified lining from these phases (figure 3). Vitrified linings are the most fragile class of metal working debris recovered from Elms Farm and large quantities will only be recovered when it was deposited relatively quickly.

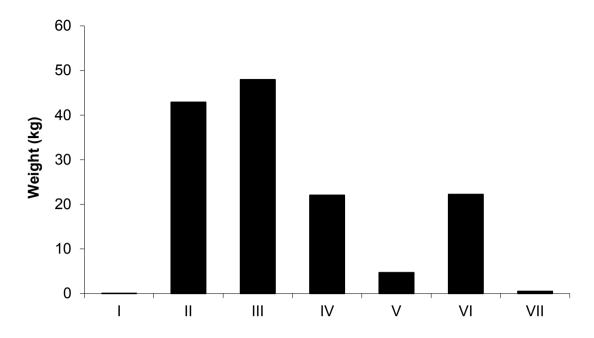


Figure 3. Weights of metal working debris assigned to each phase

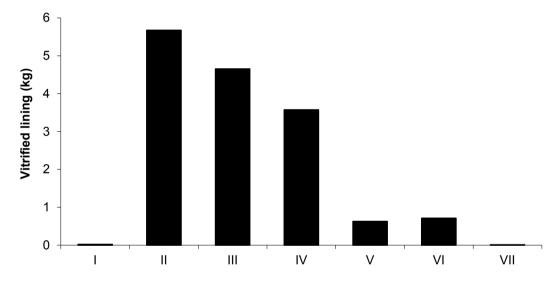


Figure 4. Weights of vitrified lining from each phase

Among the numerous pieces of vitrified lining examined there were seven with blow holes (the holes within the lining where air would be blown in using bellows). Three of the blow holes were recovered from phase II contexts, two from phase III, one from phase VI, one from phases IV–V and one unphased. This shows that the chronological focus for the iron smithing is clearly phases II and III. It is not clear, however, whether the iron smithing debris from phase III onwards is residual or represents continuing iron smithing but at a lower intensity.

## **Spatial Distribution of Debris**

The spatial distribution of the iron smithing debris can be seen in figure 4. As outlined above the areas were defined differently: some are effectively plots defined by the road and trackway network while others were alternate 20m strips. The location of areas D–R are shown in figure 5 (area W lies to the north-west of the main excavated area shown in figure5). The areas with the largest quantities of iron smithing debris are K, W, H, D and L. Figure 6 shows the spatial distribution of the vitrified lining. The vitrified lining is concentrated in areas K, L and W. The apparent concentration of vitrified lining in area W may be questioned as this area is much larger than most of the other areas and approximately half of the vitrified lining from this area derives from pottery kiln structures and may not be metallurgical. Five of the blow holes in the vitrified lining come from area K. It can be seen from the spatial distribution that the most significant concentrations of iron smithing debris come from south of track 3 and area K in particular.



Figure 5. Weights of iron working debris from each area (see figure 1 for the location of areas)

While much of the iron smithing debris was recovered from area K it is not certain that this was an area in which iron smithing was particularly focussed. Most of the contexts which contain large quantities of iron smithing debris are secondary (pits and ditches) and no structures or features positively linked to iron smithing were recognised during excavation. The kilns or ovens identified in this area are unlikely to be connected directly with iron smithing. The debris recovered may have been brought from elsewhere, although the large size of some of the pieces of (relatively fragile) vitrified lining suggests that the debris was not transported far before being dumped. It is possible that iron smithing was focussed in the area immediately south of the area excavated.

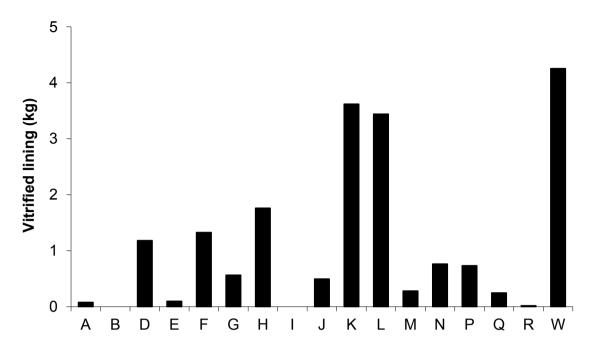


Figure 6. Weights of vitrified lining from each area (see figure 1 for the location of areas)

#### **Examination of the Iron Ingot or Bloom**

During the excavation a large cylindrical ingot or bloom of iron (sf 2676 context 11000) was recovered. The bloom is approximately 65mm thick and 210mm in diameter and weighs 22kg. The bloom is larger than other recorded weights for Roman blooms (see table 2).

Site		Reference	Weight
Forewood, Sussex	Bloom	Smythe 1936–7	1.2kg
Lower Slaughter, Gloucestershire	Bloom	O'Neil & Brown 1966	11kg
Cranbrook, Kent	Bloom	Brown 1964	0.7kg
Corbridge beam	Beam	Bell 1912	7.5kg*
Catterick beam	Beam	Wright 1972; Starley 1997	7.5kg*

Table 2. Weights of Roman blooms (\* average values obtained by dividing the total weights of the beams by the number of metallographically identified blooms)

The ingot was recovered while topsoil was removed by machine but the exact find spot within area M was recorded and it is possible that it derived from pit 15573 or pit 15588 (phases II–III). Given the large size of the Elms Farm bloom and its provenance, it would be helpful if the bloom could be directly dated.

Samples were taken from the bloom to examine the microstructure in order to determine whether it is a bloom. In addition, metallographic examination was carried out to determine the carbon content of the metal and so whether or not the bloom could be directly dated using radiocarbon dating (at the time of writing this report the

radiocarbon dating of the bloom had not been completed). A metallographic sample was cut through the depth, but only 10 mm into the width of the bloom (the bloom was extremely hard; probably due to the presence of slag inclusions). The cut sample (55 by 10mm) was mounted in epoxy resin and polished to a 1 micron finish.

Macro-examination showed that the metal is moderately porous with some pores as large as 4 by 1.3mm. The sample was etched in nital and the microstructure examined using optical and electron microscopes.

The sample of the bloom has a heterogeneous microstructure with widely varying amounts of carbon and slag. Most of the iron is present as ferrite but there are small areas where pearlite (ferrite-cementite eutectoid) is visible (see figure 7) and this is most noticeable towards the outer parts of the bloom. The carbon content (estimated from the presence of pearlite) varies from virtually nil up to 0.8%. An overall estimate of the carbon content is difficult to make but probably lies in the region 0.01–0.1%.

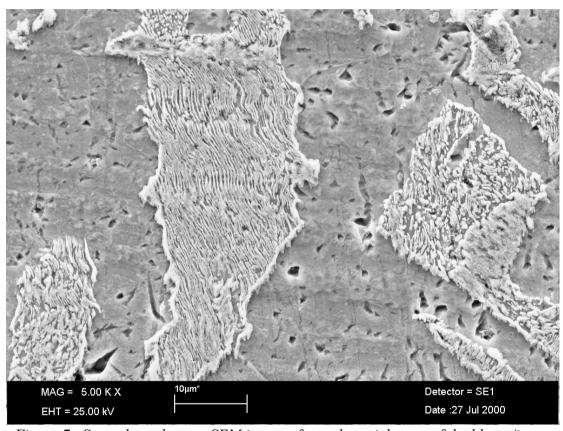


Figure 7. Secondary electron SEM image of a carbon-rich area of the bloom/ingot. The image of the polished and etched surface shows a series of equiaxed ferrite grains and some patches of pearlite (ferrite and cementite eutectoid)

Chemical analysis of the iron (using the energy dispersive spectrometer attached to the scanning electron microscope [SEM-EDS] — see table 3) showed that the bloom contained 1.3% phosphorous. Figures 8 and 9 show an SEM image and a phosphorous x-ray map of the iron-phosphorous eutectic (Stead 1900) which is occasionally present

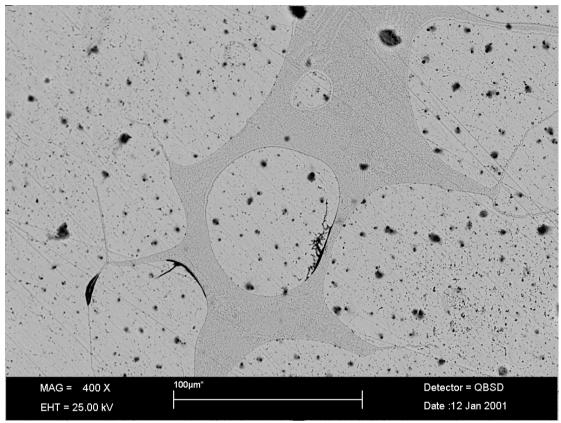


Figure 8. Back Scattered electron SEM image of iron-phosphorous eutectic

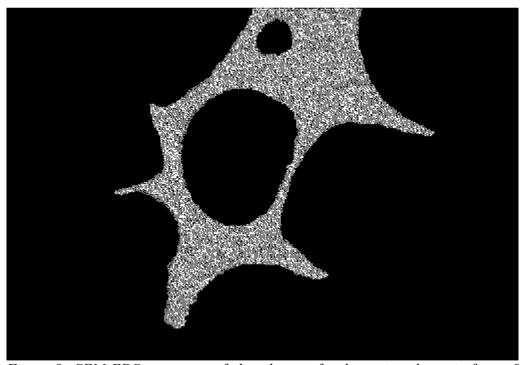


Figure 9. SEM-EDS x-ray map of phosphorous for the region shown in figure 8

within the metal. Microhardness tests of the metal yielded an average value of 280 (200 g weight, 5 measurements) which is in exact agreement with a phosphorous

content of 1.3% (Table 3, cf Tylecote & Gilmour 1986: table 2).

Site	Details	Reference	C%	P%	S%
Elms Farm	Metal		~0.1	1.3	0.02
Lower Slaughter		O'Neil & Brown 1969	~0.1	0.085	0.007
Cranbrook		Brown 1964	1.27	0.020	0.027
Little Waltham		Tylecote 1976	< 0.02	0.9-1.1	na

Table 3. Analysis (SEM-EDS, weight percent) of the bloomery iron and comparison with other published data on Roman blooms and ingots

The slag inclusions, which in some cases are over 1 mm across, do not display any particular orientation and indicate that the bloom has not been heavily forged. The slag inclusions consist of fayalite laths in a glassy groundmass (see figure 10) but no wüstite dendrites are present. The slag inclusions are frequently associated with ferritic iron (little or no carbon or phosphorous) which is poorly consolidated: having a dendritic or coral like structure (cf Blomgren & Tholander 1986).

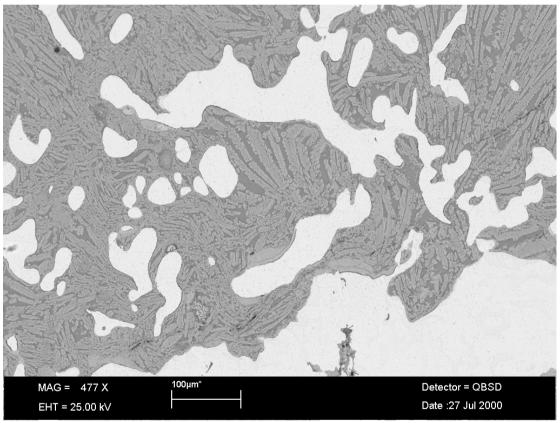


Figure 10. Back scattered electron SEM image of a mixed metal and slag area of the bloom/ingot. The image of the polished surface reveals the metallic iron (white), and slag (light grey = fayalite; dark grey = 'glassy' matrix)

The lack of wüstite in the slag suggests that the smelting conditions were very reducing and so the maximum yield of iron was obtained. The bloom would not, however have taken up appreciable amounts of carbon because the phosphorous

content of the metal inhibits the diffusion of carbon in iron (Stead 1918: 389).

Bulk SEM-EDS analysis of four areas of slag (and four spot analyses of the fayalite laths and the interstitial glass) are shown in table 4. The micro-morphology and composition of the slag is typical of bloomery smelting slags.

	Na <sub>2</sub> O	MgO	$Al_2O_3$	SiO <sub>2</sub>	$P_2O_5$	$SO_3$	K <sub>2</sub> O	CaO	TiO <sub>2</sub>	MnO	Fe
											О
Fayalite	< 0.3	1.1	0.4	26.5	0.6	< 0.1	0.2	0.5	< 0.1	3.4	66.5
Glass	< 0.3	< 0.2	16.6	39.6	3.5	0.3	4.6	7.3	0.9	1.4	24.1
Bulk	< 0.3	0.6	8.4	33.2	1.8	0.1	2.4	3.1	0.5	2.5	46.8

Table 4. Analysis of slag inclusions (SEM-EDS, weight percent, average of four determinations in each case)

The composition of the slag inclusions is characterised by relatively high phosphorous, manganese and aluminum contents. The composition of an iron smelting slag (and by extension the slag inclusions in a bloom) reflects the smelting technology and the composition of the ore, clay and fuel (Serneels & Crew 1997; Crew 1998). While there still remains much work to be done before the composition of slag inclusions can be used to determine the ore source (cf Hedges & Salter 1979; Høst-Madsen & Buchwald 1999), the composition of the slag inclusions in the Elms Farm bloom probably rule out the use of either the haematite ores of Cumbria or the limonite ore of the Forest of Dean. The bloom may well have been smelted from bogores which found throughout virtually the whole of the British Isles (including Essex).

The microstructures observed in the Elms farm bloom are comparable with those seen in other archaeological examples as well as those from modern experimental bloomery smelting. The bloom from Lower Slaughter, Gloucestershire (O'Neil & Brown 1966) is described as heterogeneous and quite porous. The relatively abundant slag inclusions showed no particular directionality (indicating little forging) and the carbon content varied from virtually nil to that of eutectoid composition (around 0.8%). The bloom from Forewood, Sussex (Smythe 1936–7) also had a heterogeneous microstructure (ferrite and some pearlite with plentiful slag inclusions). The size and shape of the slag inclusions showed that little or no forging of the bloom had taken place. Examination of the microstructure of experimental iron blooms have shown these to have a relatively high slag content (present as randomly shaped inclusions), the metallic iron is on occasion found as dendritic or coral-like structures within the slag inclusions and the metallic iron has a very variable carbon content (Blomgren and Tholander 1986).

To summarise, the examination of microstructure of sf 2676 has confirmed that it is a bloom. There is, however, no aspect of the microstructure of the bloom which would allow it to be positively identified as Roman in date as iron smelting technology changed relatively little between the Iron Age and the later Middle Ages.

#### **Conclusions**

The extensive excavations at Elms Farm recovered over 150kg of iron working debris. All of the diagnostic slags present indicated iron smithing (there were no slags diagnostic of iron smelting) and the stratified examples were concentrated in phase II and III deposits in areas K and L. The quantity of iron smithing slags recovered is not great considering the total area excavated and the duration of prehistoric and Roman activity on the site. Iron smithing is unlikely to have form a significant part of the local economy. The examination of the iron bloom has confirmed its identity but cannot, unfortunately, shed light on whether or not it is actually Roman in date. As the bloom is larger than other known Roman blooms, it is important that a direct date is obtained by radiocarbon dating. The bloom was definitely imported to the site but could have been smelted from a range of possible ores (including Essex bog ores).

### **Retention, Storage and Dispersal**

Iron working slag, being predominantly fayalitic, is not prone to deterioration and requires no special storage treatment. Material classed as "iron objects" was separated during the assessment, it is recommended that this is stored in a similar way to other ironwork. All of the metal working debris has been recorded and the unstratified material has been disposed of; all remaining metallurgical debris should be saved.

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# Appendix: List of metal working debris from each context

Abbreviations: SHB: Smithing Hearth Bottom

VL: Vitrified Lining FAS: Fuel Ash Slag SS: Slagged stones UD: Undiagnostic HS: Hammerscale ng: Not Quantified

# All weights given in grammes.

Context		Phase	SHB	VL	FAS	SS	UD	HS	Total
33	W	VI	184	137					321
92	W	VI			26				26
401	W	III	1299	62	8		481		1850
403	W	III			1				1
404	W	III	623		85		120		828
405	W	III		5	3				8
423	W	II		7	2				9
424	W	II			1				1
441	W	II	175				40		215
444	W	IIB		48	7		267		322
461	W	II	381				68		449
463	W	III-IV					29		29
466	W	II	502	221	40		246		1009
497	W	II		75	38		164		277
503	W	II					21		21
506	W	II		11	128		303	nq	442
517	W	II					13	-	13
527	W	0					6		6
532	W	III	215				262		477
534	W	II-III	1092	43			286		1421
545	W	II		51					51
552	W	III-IV					116		116
567	W	III	209						209
578	W	III-VI		74					74
609	W	II							0
1000	W	IV				3			3
1007	W	IV					30		30
1030	W	IV			1				1
1563	W	IV		1563					1563
2035			208						208
2100	W	0	293						293
2103	W	IV			10				10
2108	W	IIB-IV	205						205
2118	W	II		3			50	nq	53
2160	W	IV			1			-	1
2165	W	II-III			1				1
2398	W	IV-V		8					8

Context 2423	Area W	Phase 0	SHB	VL	FAS 2	SS	UD	HS	Total
2919	W	III-VI	336		_				336
3011	W	IV	250		3				3
3063	W	IV	344		-		69		413
3500	W	0	J		19		U)		19
3501	W	III					54		54
3510	W	III			41				41
3559	W	III-VI			18				18
3566	W	III	336	834	746		1588	nq	3504
3570	W	III	1435	770	859		581	•	3645
3578	W	III		19	137		287		443
3579	W	III		20	211		49		280
3582	W	III					88		88
3586	W	III	105	48	14		105		272
3595	W	III	515				318		833
3596	W	III			39		37		76
3631	W	III-VI	133		21		211		365
3671	W	II	149	116					265
3675	W	III	90	137			13		240
3699	W	III	1478		142		324		1944
3700	W	III			61		74		135
3752	W	III	304						304
3754	W	III			33				33
3766	W	IV	352						352
3768	W	III	424						424
3783	W	IV					97		97
3793	W	III					102		102
4000	A	0	228	41			1482		1751
4004	K	0	124	136			571		831
4006	K	IV		11					11
4009	K	III					46		46
4011	K	IV					6		6
4025	K	II					1		1
4035	K	III					1		1
4037	K	IV					5		5
4049	K	III	376	218			376		970
4085	K	IV			21				21
4129	K	VI	4051	268	4068	105	9762	nq	18254
4140	K	VI					15		15
4142	K	0					22		22
4150	K	VI					35		35
4154	K	VI	229	30					259
4164	K	III					21		21
4167	K	III	,		6				6
4187	K	VI	1245	35	193		394	nq	1867
4200	K	III					292		292
4208	K	III	د د د				80		80
4225	K	III	1411					nq	1411
4239	K	VI			35				35
4259	K	II-III		22	34		178		234

Context 4273	Area K	Phase II-III	SHB	<b>VL</b> 37	FAS	SS	<b>UD</b> 27	HS	Total 64
4286	K	II	444				174		618
4294	K	IV	1574		106		950	nq	2630
4301	K	0					1	_	1
4307	K	0		131			243		374
4315	K	V					14		14
4325	K	0		36			4		40
4326	K	II-III					58		58
4328	K	II					20		20
4330	K	II-III					23		23
4334	K	II-III					45		45
4336	K	II		206			258		464
4364	K	V					2		2
4380	K	V				465			465
4395	K	III		85			143		228
4430	K	IV			61				61
4433	K	II		37					37
4434	K	II-III			40				40
4459	K	III		69					69
4460	K	III		51					51
4461	K	III		34					34
4462	K	II-III			5				5
4481	K	II					50	nq	50
4485	K	II					66		66
4493	K	II-III			21		23		44
4497	K	II-III					2		2
4537	K	III	221						221
4539	K	II	380	233	164		128	nq	905
4540	K	0					161		161
4579	K	III					19		19
4584	K	III			10		6		16
4596	K	III					2		2
4598	K	0					1		1
4609	K	IV					124		124
4657	K	II-III		8	9				17
4682	K	III			31				31
4683	K	0					106		106
4686	K	IV			62		369		431
4688	K	V					25		25
4689	K	IV-V					70		70
4690	K	0					1		1
4692	K	0	227		1		138		366
4699	K	II	428	379	974		297	nq	2078
4715	K	VI		15	8				23
4753	K	IV					2		2
4761	K	III					1		1
4794	K	III					48		48
4800	K	IV		61			77		138
4801	K	IV		26					26
4819	K	IV			1				1

Context 4820	Area K	Phase IV	SHB	VL	FAS	SS	UD 20	HS	Total
4823	K	III					1		1
4832	K	VI		1	3		5		9
4835	K	IV		1	1		3		1
4839	K	IV			1				1
4844	K	IV		185	1		229		414
4848	K	II-III		103			218		218
4869	K	IV					210		2
4870	K	IV		26			114		140
4874	K	V		115	50		583		748
4875	K	V		113	38		322		360
4880	K	IV		69	94		86		249
4881	K	0		09	94		14		14
4895	K	II			1		14		14
4893	K	IV			1 18				18
4909	K	0		19	10				19
			40	19			2.4		
4925	K	IV	49				34		83
4932	K	II					126		126
4934	K	II					155		155
4936	K	IV	122	22	10		32		32
4937	K	II-III	132	33	19 25				184
4944	K	II		10	35				35
4962	K	IV		10	34				44
4963	K	0			1		21		1
4974	K	III	215	20	1.1		21		21
4977	K	III	315	38	11		18		382
4985	K	II-III		1.7	8		89		97
4994	K	0		15			362		377
4999	K	II-III					1		1
5000	J	0					23		23
5146	J	III	600				63		63
5149	J	III	600				72		600
5162	J	V-VI					73		73
5207	J	V-VI					1		1
5211	J	IIA	1.4.4				58		58
5269	J	IIA	144				2.5		144
5275	J	V-VI					25		25
5337	J	IV					169		169
5374	J	V-VI			121		1		1
5376	J	V-VI			131		14		145
5393	J	IV					1		1
5427	I	0					113		113
5429	J	V-VI					1		1
5434	J	0	200				137		137
5518	J	IV	200						200
5559	J	0					22		22
5598	I	0	502						502
5601	I	0					178		178
5602	I	0					84		84
5603	I	0					232		232

Context		Phase	SHB	VL	FAS	SS 1	UD	HS	Total
5607	I	0			8				8
5608	I	0				1	140		140
5610	I	0				1	158		158
5628	I	0					36		36
5630	J	IV	197						197
5676	I	IIIB					57		57
5691	I	IIIB			27				27
5692	I	IIIB					1		1
5694	J	0	157			3	312		469
5709	I	IIIB			34				34
5732	J	0					42		42
5747	I	II-VI				3	314		314
5748	J	V	249				58		307
5783	J	II-III					1		1
5808	J	IIIB					78		78
5809	J	0					6		6
5858	J	V-VI		90			9		99
5877	I	IIIB		, ,			5		5
5883	I	IIIB	539				Ü		539
5907	I	IIIB	00)				97		97
5936	I	IIIB				1	102		102
5939	J	IV					150		150
5993	I	IIIB					185		185
6000	Н	0	445	293		٠	30		768
6008	Н	VII	308	275			50		308
6029	Н	IV	374						374
6053	Н	III	367	33	21				421
6057	Н	0	203	251	21				454
6095	Н	VII	180	231					180
6132	Н	IV	100			1	191		191
6148	Н	IV	121			,	171		121
6219	Н	IV	655						655
6240	Н	IV-VI	112						112
6250	Н	IV	112	52					52
6292	Н	III		7			55		62
6314	Н	IV		,			36		36
6349	Н	IV	1653				22		1675
6350	Н	IIB	1033	172		_	223		395
6367	Н	III-IV	196	1/2		4	48		244
	Н	III-I V IV	190				46		4
6396 6414	п Н						16		16
		III	2216	97		1.4			
6420	Н	IV	2216	87		10	591		3994
6421	Н	III	306	767	973	24	(22		306
6426	Н	III	2379	767	862	26	533		6641
6437	Н	III	166				02		166
6515	Н	0	402				92		92
6516	Н	III	492	21		3	555		1047
6522	Н	III		21			0.6		21
6523	Н	IIB-III					86		86
6533	Н	III					10		10

Context		Phase	SHB	VL	FAS	SS	UD	HS	Total
6538	Н	III					1		1
6552	Н	0					23		23
6572	Н	III	4.50				1		1
6589	Н	V	458						458
6609	Н	0	168	0			200		168
6642	Н	III	225	9			300		309
6672	Н	III	237						237
6710	Н	III					2		2
6750	Н	IIB					4		4
6760	Н	III					99		99
6774	Н	IV					87		87
6811	Н	IIA		69			• • •		69
6828	Н	IIA	151				309		460
6876	Н	IIA	4.40				1		1
6937	H	IIB-III	140						140
7000	G	0		141			536		677
7024	G	VII					2		2
7057	G	V	244				67		311
7059	G	IIB-III	492						492
7066	G	V					41		41
7071	G	IV		2			205		207
7073	G	0	460				102		562
7080	G	IV	236						236
7082	G	V	256						256
7086	G	V-VI	3295	140	1270				4705
7103	G	0					77		77
7116	G	III-VI	660				667		1327
7118	G	III					70		70
7140	G	III					142		142
7154	G	IV-V	220				1		1
7158	G	III	228				122		228
7173	G	III		4.4			132		132
7178	G	II		44	4				44
7186	G	II			4		4		4
7258	G	II			2		4		6
7298	G	II	222		1				1
7315	G	IV	232	1.6	242		116		232
7358	G	II	215	16	243		116		375
7376	G	II	315	20					315
7381	G	P		20			<i>5.4</i>		20
7390	G	IV	470	60			54		54
7417	G	II	478	69					547
7539	G	IV	140				1		140
7595 7597	G	0					1		1
7597	G	0					63		63
7598 7620	G	0		20			20		20
7620	G	III-VI		28	20		(0		28
7664	G	II			38		69		107
7682	G	III-V		104	2				2
7684	G	III-V		104					104

Context		Phase	SHB	VL	FAS	SS	UD	HS	Total
7705	G	IV	7.60	72			2		2
8000	Е	0	769	73			17		859
8016	Е	II		4				nq	0
8021	E	II		4			02		4
8065	Е	VI			10		92		92
8076 8077	E E	VI			12		1		12 1
8077	E E	III-VI IV		21			86		107
8141	E	V		21	43		2		45
8153	E	V			5		18		23
8167	E	V III			3		19		19
8214	E	III					6		6
8214	F	IIB		14			U		14
8500	г Р	0		30					30
8537	P	III		30			1		1
8543	P	III					18		18
8723	P P			37					
8723 8724	P P	III II		334			253 33		290
	P P						33		367
8739 8746	P P	VI		1	15		45		1
8740 8747	P P	IIB			15				60
8747 8795	P P	VI	237				113		113
	P P	III		120	212		1204		237
8804 8825	P P	III	1316 962	120 164	213		1304 733		2953 1859
8924	P P	III III	902	104			733 24		24
8924 8991	P P	III-IV			57		24		57
9008	D	IIIC			31		11		11
9008	D	IIIC		92			1		93
9109	D	II		92			63		63
9109	D	II					268		268
9237	D	0					1		1
9237	D	0	88				1		88
9242	D	0	415				146		561
9243 9247	D	IIB	413				72		72
9247	D	IIB					12		12
9250	D	IIB			221		12		221
9259	D	II	135	87	866		258		1346
9263	D	II	133	07	800		6		6
9265	D	III-IV					6		6
9272	E	III-I V					U		0
9280	D	IIA					37		37
9282	D	0					9		9
9288	D	IIA	310	90	61		930		1391
9297	D	IIA	510	70	01		930 7		7
9297	D	IIIC-IV	62		12		644		718
9317	D	IIIC-I V	02	18	12		044		18
9317	D	IIIC-IV		10			21		21
9321	D	IIIA-B		110			<i>L</i> 1		110
9344	D	III-IV		110			36		36
9365	D	0					49		49
7505	ט	U					77		77

Context		Phase	SHB	VL	FAS	SS UD	HS Tota	
9370	D	IIB	250	0.4	2.0	1050	250	
9388	D	IIB	761	94	26	1073	1954	
9415	D	IIA		22		37	59	
9416	D	IIA	2.2	113		656	769	
9417	D	IIA	99			97	190	
9418	D	IIA		83	16	22	12	
9419	D	IIA			12	161	173	
9420	D	IIIB	191				19	
9426	D	0				44	44	4
9427	D	0	1955		107	1302	3364	
9444	D	IIIC-IV	2145	326	28	301	2800	)
9446	D	II				1		1
9458	D	III				1		1
9469	D	IIIC-IV				230	230	C
9475	D	IIIC-IV		27			2	7
9480	D	IIIC-IV	171				17	1
9488	D	IIB	209			231	440	
9497	D	IIB	1359			368	172	
9510	D	0				64	64	
9533	D	0				49	49	
9549	D	IIIA-B				172	172	
9560	D	IIIB		22		1,2	22	
9565	D	IV		22		2		2
9592	D	IV				7		7
9610	D	IIA			1	,		1
9648	D	IIIB			1	73	73	
9660	D	IIA			2	73		2
9683	D	0			2	87	8′	
9695	D	IIIC		2		433	433	
9703	D	IIA		2		4		6
9715	D	0				142	142	
9720	D	0		4		1.5		4
9737	D	II-III				15	1:	
9749	D	IIIC		91			9:	
10011	Е	IV				43	43	
10017	Е	V			18		18	
10028	Е	IV			13	12	2:	
10033	E	II-III				1		
10073	F	0				25	25	
10088	F	IV	112				112	
10104	F	IV		206		43	249	)
10109	F	II		3			3	3
10121	F	III	210			31	24	1
10182	F	III				125	12:	5
10184	F	III			1			1
10194	F	IV				46	40	5
10249	F	0				177	17	7
10250	F	0	150	46	23	217	430	
10255	F	V	112		25		137	
10261	F	V	99		20		119	

Context 10280	<b>Area</b> F	Phase V	SHB	VL	FAS	SS	<b>UD</b> 118	HS	Total
10291	F	V					10		10
10296	F	V-VI			8				8
10304	F	0					18		18
10310	F	0					190		190
10320	F	IV	434						434
10330	F	IV				60	135		195
10350	F	III			1		73		74
10376	F	III			20				20
10379	F	0					118		118
10496	F	V					154		154
10502	F	V		47	50		99		196
10514	F	V-VI	194						194
10528	F	0					71		71
10539	F	V-VI					187		187
10540	F	III		90					90
10594	F	III		, ,			86		86
10621	F	IV				860	41		901
10642	F	V			7	000			7
10649	F	IV			,		1		1
10688	F	V	124				213		337
10751	F	V	394				213		394
10800	N	0	371				134		134
10869	N	II					134	nq	0
10897	N	IV					68	nq	68
10898	N	0					75		75
10909	N	IV-V					1		1
10930	N	0					165		165
11000	A	0	403	37	73		977		1490
11036	N	II	205	45	12		228		490
11105	N	0	203	73	12		55		55
11107	N	0					82		82
11138	N	II					78		78
11146	N	II					28		28
11153	N	II			245		209		454
11156	N	II		54	273		54		108
11216	N	II-III		34			86		86
11255	N	II-III					180		180
11263	N	II-III					1		1
11265	N	II	109				1		109
11203	N	III	109		7				7
11201	N	II			/		16		16
11300	N	II		145	194		10	na	
				143	194			nq	339
11369 11426	N N	II IV		13			3		15 3
	N N	IV					2		2
11436	N N						151		
11449 11474	N N	IIB II			10		131		151
11474					10				10
11492 11528	N N	II		11	1				1 11
11320	1.4	11		11					11

Context		Phase	SHB	VL	FAS	SS	UD	HS	Total
11559	N	IV						nq	0
11565	N	III		20					20
11577	N	IV					1	nq	1
12000	R	0	365						365
12019	R	IV			20				20
12026	R	IV-V					24		24
12043	R	0					28		28
12044	R	IV-VI	136		25				161
12045	R	IV-VI		17					17
12113	R	VI					87		87
12235	R	III			1				1
12246	R	III-VI					85		85
12346	В	0	1143				49		1192
13043	J	0					11		11
13048	I	IV	265				17		282
13093	I	IV			29				29
13148	I	IIIB			2)		1		1
13276	J	0	744				1		744
13281	J	IV	526						526
13289	J	0	320				129		129
13317	I	V					129		129
13317	J	V III					4		4
			402				4		
13400	J	III	492		2				492 2
13410	I	IIIB	200		2				
13419	I	II-VI	288				4		288
13452	J	IIIA					4		4
13551	J	IIB					2 3		2
13561	J	IIIA	1.5.5				3		3
13576	I	IIIB	155		4.0				155
13639	I	IIIA			18				18
13641	I	II-VI					19		19
13692	I	IIIA	721						721
13697	I	IIB						nq	0
13734	I	IIIB					121		121
13779	J	0		39					39
13791	J	II						nq	0
13803	J	0					60		60
13822	I	IIIB	334						334
13834	I	IIIB					37		37
13844	I	IIIB	400		13		1219		1632
13890	I	IIIB	355						355
14008	K	II			4				4
14022	K	IV-V	3358		1		1		3360
14032	K	II			1				1
14045	K	II	160		5		408		573
14046	K	II	212	411			350		973
14058	K	III					1		1
14062	K	II					1		1
14067	K	II-III					5		5
14089	K	IV-V					63		63

Context		Phase	SHB	VL	FAS	SS UD	HS Total
14093	K	IV-V	178		1	98	276
14204	L	VI		50	1	14	15
14206	L	IIA-B		50	105	207	257
14226	L	IIA-B		85	107	337	529
14235	L	IIC	• • •	15		115	130
14258	L	II	286	135		261	682
14259	L	IIC	200			189	389
14341	L	III				1	1
14346	L	0				1	1
14354	L	II				101	101
14381	L	IIC	559	312	3	543	1417
14407	L	IIA-B				2	2
14432	L	0		28		67	95
14466	L	IIC				25	25
14510	L	IIC	475			557	1032
14519	L	IIC				20	20
14521	L	IV	612	70	318	98	1098
14525	L	V			4		4
14533	L	IIA-B		25	186		211
14547	L	IIA-B			22		22
14548	L	IIA-B				1	1
14558	L	VI				7	7
14564	L	V			1	6	7
14569	L	IIC	220	101	40	30	391
14573	L	0	130				130
14583	L	IIC			13	39	52
14590	L	IIC			33		33
14591	L	V			1	2	3
14595	L	II		33	13		46
14600	L	IV				177	177
14609	L	0		36		45	81
14610	L	IV			3		3
14613	L	VI				3	3
14619	L	0				111	111
14625	L	II		124			124
14627	L	II				10	10
14662	L	0				18	18
14664	L	0				12	12
14679	L	IV		151			151
14684	L	IIB				3	3
14706	L	IIA-B		31			31
14711	L	III				32	32
14743	L	V				90	90
14753	L	0		159		83	242
14762	L	IIC				28	28
14784	L	IIA-B			1	1	2
14789	L	0		118		1	118
14800	L	V-VI		110		3	3
14807	L	IIA-B			22	74	96
14818	L	0			22	53	53
1 1010		J				33	33

Context 14824	<b>Area</b> L	Phase II	SHB	VL	FAS	SS	U <b>D</b> 29	HS	Total 29
14839	L	IIC		167	30		2)		197
14861	L	IIA-B		107	30		280		280
14862	L	IIA-B		78			242		320
14879	L	0		25			58		83
14884	L	II		23			80		80
14893	L	VI			1		80		1
14901	L	IIB			1				1
14902	L	IIB			1		18		18
14914	L	IIC		25			10		25
14936	L	III		23			60		60
14948	L	IIA-B		24			00		24
14948	L	IIC		24	11				11
15025	M	0			11		47		47
15044	M	0					87		87
15058	M	0					1		1
15122	M	VI					17		17
15122	M	IV					1		1
15232	M						18		
15281	M	VI 0		4			10		18 5
15288				4	12		1		12
15307	M M	II-III		5	4		2		12
	M	II-III		3	4		30		30
15308 15386	M	II-III II-III					5		5
	M				23		3		23
15420 15458	M	II II-III	222		23				23
15459	M	II-III	222					<b>10</b> G	0
15463	M	II-III III		5			134	nq	139
15464	M	II-III		3			134		139
		II-III IV	179				1		
15515	M M		1/9				17		179 17
15555 15586		II-III	329				17		329
	M	II-III							329 327
15587 15592	M M	II-III	327	10					
15611	M	II-III		10	2				10 2
15612	M	II-III		54	15		135		
		II-III V-VI		34	13				204
15667	M				3		172		172
15668	M	IV-V			3		23		3
15683	M	III			12		23		23
15686	M	II-III IV-V			13		2		13 2
15756	M		406				2		
15787	M	III	486						486
15816	M	II IV V	311				70		311
15857	M M	IV-V	245				78		323
15869	M	VI	527				1		1
15881	M	II-III	537				100		537
15889	M	III	567	1 /	0		108		675
15893	M	V-VI	007	14	8		11		33
15982	M	IV	997	15			4		1012
16016	Н	III					4		4

Context 16040	Area H	Phase IIB	SHB	VL	FAS	SS	UD	HS	Total
16051	Н	0	344				21		365
16073	Н	IV					67		67
16082	Н	III-IV			11				11
16230	Н	VI	92						92
16333	Н	VI	235						235
17012	Q	III		10	21		2		33
17016	Q	0					105		105
17031	Q	III					89		89
17033	Q	III		132			46		178
17037	Q	IV		152	50		301		351
17058	Q	III					10		10
17060	Q	IIA		18	5		4		27
17070	Q	IIA		10	11		5		16
17211	Q	III			1		3		4
17255	Q	IIB	180		•				180
17258	Q	IIB	100	16					16
17323	Q	IIA		10	32				32
17352	Q	IIA		70	146		200		416
18028	J	IIA		70	13		200		13
18200	I	IIIA			13				13
18229	I	IIIA			13				13
18240	I	IIIA			2				2
18256	J	IIA			2		1		1
18765	J	IIA					121		121
18812	J	IIB	317				121		317
18961	J	IIB	1976				119		2095
19005	P	0	1970				21		2093
19003	P	III	992	46			148		1186
19163	P	III	992	40	1		140		1
20000	L	0			1		111		111
20007	L	V-VI	145				111		145
20007	L L	IIC	711	24			211		946
20031	L	IIA-B	/11	39			171		210
20039	L L	IIA-B IIA-B	355	39			1/1		355
20040	L	IIA-B IIA-B	333	489			378		867
20041	L L	IIA-B IIA-B	230	409			3/0		230
20042	L	IIA-B	230	35					35
20072	L L	IIA-B	88	33					88
			00				25		
20101	L	IIA-B	571	527	((0		25		25
20147	L	IIC	571	537	668		49		1825
20148	L	IIC	1233	468	582		230	nq	2513
20149	L	0		28			<i>5</i> 1		28
20164	L	0					51		51
20194	L	V					37		37
20197	L	IIC	4 1 -				47		47
20200	L	IIC	415				<b>51</b>		415
20210	L	IIC					51		51
20230	L	IIC					88		88
20280	L	IV					116		116

Context		Phase	SHB	VL	FAS	SS	UD	HS	Total
20304	L	IIA		30					30
20331	L	IIB	174				77		251
21500	J	0	107						107
21503	J	IIA		40	30		20		90
21543	J	IIA					149		149
21568	J	IIIB					58		58
21614	J	IV		76					76
21615	J	IIIB	1375				862		2237
21686	J	VII		10					10
21705	J	IIIA					32		32
21710	J	VI					82		82
21917	J	V-VI					52		52
21971	J	III					16		16
22077	J	IIA		57					57
22078	J	IIB	236	140	15		296		687
22256	J	IIB					48		48
22328	J	IIB		6			85		91
22350	J	IIB		37	12		14		63
22352	J	IIIA					182		182
22354	J	IIB					118		118
22365	J	IIB					121		121
23001	N	0		4					4
23002	N	0	403				120		523
23005	N	II					9		9
23020	N	IV					39		39
23025	N	III		220					220
23056	N	IIB					55		55
23134	N	II					84		84
23283	N	III		249					249
24003	M	VI	484	120					604
24120	M	II-III	495				25		520
24133	M	0					94		94
24198	M	IV		20					20
24221	M	IV-V		33					33
24313	M	III					92		92