# IGHTHAM MOTE, IGHTHAM, KENT PORTABLE XRF ANALYSIS OF THE WINDOW GLASS

**TECHNOLOGY REPORT** 

Brice Girbal and David Dungworth



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#### SUMMARY

The analysis of historic window glass has been undertaken with the purpose of determining the age the glass. Previous research has established how changes in raw materials and window glass manufacturing technologies are manifested in the composition of the glass and that this can be used as the basis for a glass dating technique. This report contains the analysis of 1,939 panes of window glass from Ightham Mote, Kent. All of the analyses were carried out *in situ* and non-destructively using a portable X-Ray Fluorescence (pXRF) spectrometer. The report contains a discussion of the problems encountered in attempting to obtain reliable data on light elements with pXRF, especially the effect surface corrosion. These problems have prompted a greater reliance on heavy elements, such as rubidium and strontium, whose detection is less affected by surface corrosion. The pXRF data has been analysed to show that 10% of the analysed panes are made of forest glass, that is glass manufactured before the last third of the 16th century. These panes may represent original 14th-century glazing or the alterations and addition to the windows commissioned by Sir Richard Clements in the early 16th century. Chemical analysis indicates that 34% of the analysed panes are made from high-lime, low-alkali (HLLA) glass and so likely to have been manufactured towards the end of the 16th century or during the 17th century. Only 3% of the analysed panes were made using seaweed ash and so datable to the 18th century or first three decades of the 19th century. The remaining 53% of the analysed panes were made using synthetic soda and so datable to the years after c1835. The distribution of the forest and HLLA glass suggests that many of these panes have been re-set and that some may even have been moved from window to window, room to room and possibly building to building.

#### **ACKNOWLEDGEMENTS**

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DATE OF RESEARCH

2010-2011

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#### INTRODUCTION

The preservation of the fabric of historic buildings must include an appreciation of a wide range of architectural materials. While stone and brick components are prominent components of a historic building, some other materials are less highly regarded. The transparency of window glass can occasionally mean that it is less noticed; in extreme cases it may even be replaced with modern glass. This is regrettable as the surface texture and tint of much historic window glass lend character to buildings. An essential requirement for making a historic window glass conservation decision is a clear understanding of the age of surviving glass. If glass is original then it will usually have greater value. This report describes the application of scientific analysis to enhance historic window glass conservation decisions.

### AIMS AND OBJECTIVES

English Heritage has undertaken significant research into historic window glass (Dungworth 2011). This research has been divided into two phases. In the first phase samples of historic window glass obtained from a wide range of architectural and archaeological contexts have been analysed using laboratory-based techniques (summarised below). This has established that a series of changes in glass composition have occurred over the past five centuries. The chronological changes in glass composition have been interpreted as the result of the rapid adoption of new technologies and raw materials as these have become available.

The second phase of this project has used a portable X-Ray Fluorescence (pXRF) spectrometer to investigate the chemical composition of historic windows, *in situ* and non-destructively. Several different buildings have been investigated (eg Dungworth and Girbal 2011) and Ightham Mote was selected because of the scale and complexity of the surviving glazing.

# HISTORIC WINDOW GLASS: A SUMMARY OF CURRENT KNOWLEDGE

Almost all glass produced in Britain during the medieval period was made using sand and terrestrial plant ashes (primarily bracken) and has a distinctive potassium-rich composition (Dungworth and Clark 2004). The arrival of French glassmakers in the 16th century saw a change to a high-lime low-alkali (HLLA) glass. HLLA glass was probably made using sand and the ash of hardwoods (such as oak). This HLLA glass remained in use until the end of the 17th century when it was superseded by a glass made using sand and seaweed (kelp) ash (Dungworth *et al* 2009; Parkes 1823; Watson 1782). This kelp glass dominated the

window glass industry until the early part of the 19th century when it was abandoned in favour of soda-lime-silica (SLS) glass made using synthetic soda (Cooper 1835; Ure 1844; Muspratt 1860).

Table 1. Average chemical composition of historic window glass at different times (Dungworth 2011)

Phase	1	2a	2b	3	4a	<b>4</b> b	5a	5b
Start		c1567	c1600	c1700	c1835	c1870	c1930	c1960
End	c1567	c1600	c1700	c1835	c1870	c1930	c1960	
Na <sub>2</sub> O	2.5±0.3	1.4±0.7	2.4±1.4	7.9±0.7	12.7±0.9	12.9±2.1	13.9±0.5	13.3±0.4
MgO	$7.3 \pm 0.7$	$3.4 \pm 0.5$	$3.0\pm0.7$	$5.3 \pm 0.3$	0.2±0.1	$0.2 \pm 0.2$	$2.8 \pm 0.2$	3.8±0.1
$Al_2O_3$	1.6±0.5	$2.8 \pm 1.0$	$3.0 \pm 1.3$	$2.6 \pm 0.6$	0.6±0.1	1.2±0.3	$0.9 \pm 0.6$	1.3±0.2
$SiO_2$	55.8±2.5	60.4±1.8	60.9±2.0	66.5±1.4	$70.8 \pm 1.2$	71.9±0.4	72.2±0.7	72.2±0.5
$SO_3$	0.3±0.1	0.2±0.1	$0.4\pm0.2$	0.2±0.1	0.4±0.1	$0.4 \pm 0.2$	$0.4 \pm 0.2$	$0.2 \pm 0.1$
Cl	$0.4 \pm 0.2$	$0.3 \pm 0.2$	0.2±0.1	0.6±0.1	$0.1 \pm 0.1$	<0.1	<0.1	<0.1
$P_2O_5$	$3.2 \pm 0.4$	$2.1 \pm 0.2$	$2.1 \pm 0.6$	$1.1 \pm 0.2$	< 0.2	< 0.2	< 0.2	< 0.2
$K_2O$	11.4±1.5	5.6±1.6	5.1±1.9	4.2±0.2	$0.1 \pm 0.1$	$0.5 \pm 0.2$	$0.1 \pm 0.1$	0.6±0.1
CaO	15.3±1.6	21.5±1.9	$21.1 \pm 1.7$	$10.4 \pm 1.0$	14.0±0.8	12.9±1.6	9.7±0.8	8.3±0.6
MnO	1.26±0.30	$0.94 \pm 0.37$	0.24±0.20	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
$Fe_2O_3$	0.65±0.13	$1.01 \pm 0.20$	1.31±0.29	$0.71 \pm 0.14$	0.22±0.06	$0.21 \pm 0.06$	$0.13 \pm 0.03$	0.12±0.01
$As_2O_3$	< 0.20	< 0.20	< 0.20	< 0.20	0.22±0.16	< 0.20	< 0.20	< 0.20
SrO	0.07±0.01	$0.09\pm0.02$	0.07±0.01	0.45±0.10	0.03±0.01	0.02±0.01	$0.01 \pm 0.01$	$0.01 \pm 0.01$

Nicholas Leblanc invented a process for the manufacture of synthetic soda at the end of the 18th century. Common salt was heated with sulphuric acid to produce sodium sulphate (soda saltcake). The sodium sulphate was then heated with lime and charcoal or coal to produce sodium carbonate. Initially, glass could only be made with sodium carbonate, but glassmakers soon discovered that the sulphate could be used directly if it was combined with charcoal or coal. Glass made for the century or so following the 1830s was a simple soda-lime-silica (SLS) glass with low levels of impurities (Dungworth 2009). The plant ashes used before the introduction of Leblanc soda all naturally contained enough calcium (lime) to ensure that the glass manufactured was durable. Leblanc soda contained no calcium and from the 1830s lime was an essential ingredient in window glass recipes (batch).

The early decades of the 20th century saw the introduction of mechanisation in the window glass industry (Cable 2004; McGrath and Frost 1937). Ultimately, mechanisation allowed continuous production of huge quantities of flat glass; however, it was accompanied by problems of devitrification —small crystals would tend to form in the glass. This problem was overcome by replacing a proportion of the calcium in the batch with magnesium (Turner 1926) and virtually all window glass made in Britain since 1930 has contained 2–5wt% magnesia (Smrcek 2005). An examination of the magnesium content of flat glass produced since the introduction of mechanisation suggests that there are two groups: one with 2.5–3.0wt% MgO and one with 3.5–4.5wt% MgO. Contemporary technical literature does not provide an explanation for this; however, it is likely that the introduction of the float process (Pilkington 1969) saw the re-emergence of

devitrification problems which were overcome by increasing the MgO:CaO ratio (from 0.3 to 0.4–0.5, Dungworth and Wilkes 2010).

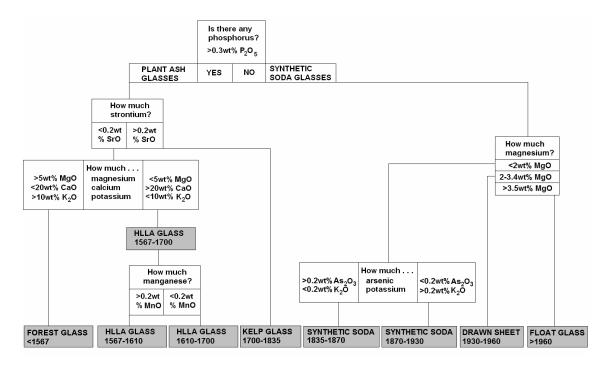


Figure 1. Model for assigning glass to chronologically significant compositional groups (Dungworth 2011)

The chemical analysis of over 800 samples of historic window glass suggests that such glass can be quickly assigned to a chronologically significant compositional group on the basis of a small range of oxides (especially MgO, P2O5, SrO, MnO and As2O3). A model for this process is given as Figure 1 and typical glass for each chronological phase is summarised in Table 1. The chemical analysis of window glass can provide important information about the date of manufacture and its installation. This information can provide a sound basis for informed conservation (Clark 2001) of historic window glass. Knowing the date of individual panes of glass in a building will allow the identification of original glazing and later repairs and replacements. This understanding is an essential prerequisite for appropriately valuing and managing the window glass in historic buildings (cf English Heritage 2005). The use of laboratory-based techniques can provide the necessary information; however, this is only possible where a window is broken or is undergoing renovation (cf Dungworth and Loaring 2009; Freestone et al 2010). As such this approach is of limited use for providing information about in situ glass. The solution proposed in this report is the use of a portable X-Ray Fluorescence (pXRF) spectrometer which will allow non-destructive in situ analysis.

#### **IGHTHAM MOTE: ARCHITECTURAL BACKGROUND**

Ightham Mote is a large, well-preserved moated site which is owned by the National Trust. The earliest surviving buildings, comprising an open hall, two solar ranges and a chapel (Figure 2), were thought to be constructed by Sir Thomas Cawne and dated to 'the middle years of Edward III's reign' (Starkey 1982). More recent research has shown that construction took place in the fourth decade of the 14th century (Pearson *et al* 1994, 74) and has indicated that there is no documentary evidence linking Cawne to Ightham Mote prior to the 1370s (Pearson 1994, 31).

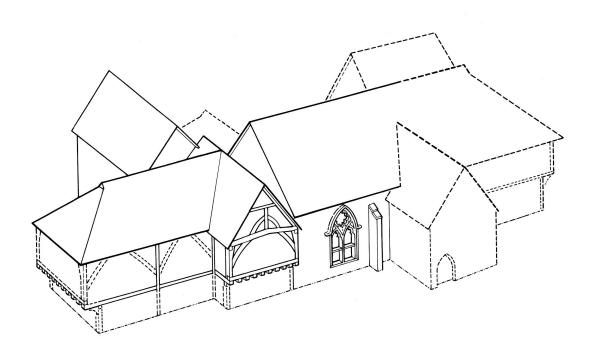


Figure 2. Reconstruction of the 14th-century buildings at Ightham Mote (Pearson et al 1994, Figure 22)

The I4th-century buildings lie within what is now the eastern range — the western range being added in the late I5th century by Edward Haut, who probably also enclosed the courtyard (Pearson 1994, 128). Sir Richard Clement purchased Ightham Mote in I521 and commenced a programme of repairs and alterations to support his aspirations for advancement at the royal court (Starkey 1982). The house was embellished with Tudor symbols (Figure 3), including the Tudor rose and the pomegranate of Granada (an explicit reference to Henry VIII's marriage to Catherine of Aragon, and allowing this glass to be dated to I521–I529). Armorial glass in some first-floor windows of the gatehouse (W37 and W38, see Figure 4) appears to represent Clement's arms and commemorate both of his marriages (Anne Whittlebury in I510 and Anne Barley c1530). The current setting of these windows suggests that the armorial badges have been retained but that the surrounding plain glass is later (late 18th century or early 19th century).



Figure 3. Ightham Mote window W02 (detail) containing Tudor badges



Figure 4. Ightham Mote window W37 containing Clement's armorial badges

The New Chapel was built by Clement and contains a richly decorated ceiling (Starkey 1982); however, the extant glass has an unusual provenance. Although it is thought that at least some of the glass is 16th century in date, much of it is of German origin (probably St Peter's, Cologne) from the Hampp hoard and only installed in the 19th century (Marsh 2009). The wide variety of glass tints in the plain glass panes of the windows in the New Chapel (as well as many other windows at Ightham Mote) suggests the collection of glass from several different sources (Figure 5). The glass in other windows (eg W01, W02,

W57 and W58) includes several different sizes of pane and suggests that they have also been glazed using glass from multiple sources (see Figure 12, Panel 1).

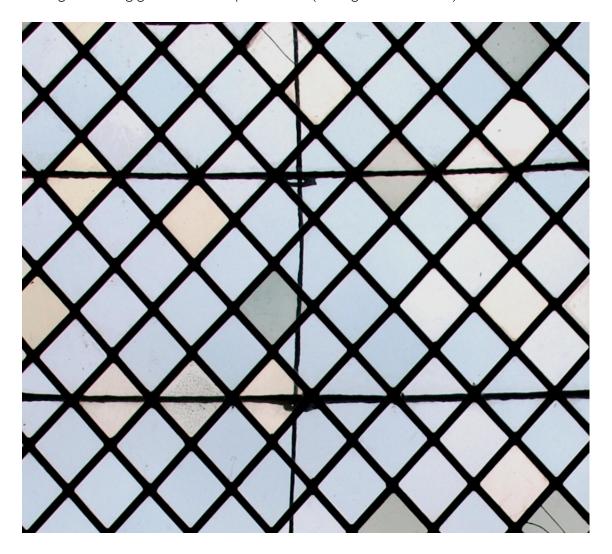


Figure 5. Ightham Mote window W45 (detail) showing a variety of glass tints

Ightham Mote was bought by the Selby family in 1591 and they retained ownership until the late 19th century. Sir William and Dame Dorothy Selby (1611–1641) developed the drawing room, rooms on the western range and the 'Jacobean' staircase.

According to Newman (1980, 345) most of the western and southern ranges were rewindowed c1800 with pointed windows and intersecting glazing-bars (Figure 6). In addition, the northern window of the drawing room (W40) contains 'an unexpected 18th-century Venetian window, superimposed on a large Jacobean window' (Newman 1980, 345). The painted glass roundel in this window (the Selby family symbol) is signed Eginton and dated 1810 — William Raphael Eginton was active from 1805 (Figure 7).



Figure 6 Ightham Mote window W07. Late 18thor early 19th-century window



Figure 7. Ightham Mote window W40 with the painted roundel signed Eginton 1810

Sir Thomas Colyer-Fergusson purchased the house in 1889 and undertook an extensive repair programme. It is known that many parts of the house underwent significant restoration at this time (Starkey 1982) and it is possible that some windows were altered. Colyer-Fergusson owned the property until his death in 1951. His grandson sold the house itself to a local consortium which hoped to renovate and preserve it. This proved to be beyond their means and in 1953 it was sold to Charles Henry Robinson. On his death in 1985, he bequeathed the house to the National Trust, who started a major programme of renovation in 1989.

The architectural history of Ightham Mote suggests that the extant windows have a variety of origins. It is possible that a very small amount of glass may be medieval in date; it is likely that a significant proportion of the glazing is of 16th-century date, although some of this is of German origin and only installed in the 19th century. Some windows can be easily identified as 18th- or 19th-century replacements. Other contemporary windows are likely to have made extensive use of older glass.

#### **METHODS**

The pXRF instrument chosen to undertake the *in situ* non-destructive analysis of the historic window glass at Ightham Mote was a Niton XL3t (Cu/Zn Mining Mode) which allowed the simultaneous determination of the concentration of over 20 elements including almost all of those determined using the laboratory-based techniques. The only element which was routinely determined using laboratory-based techniques but which could not be determined with the Niton XL3t was sodium. The Niton X3Lt uses a helium flush to improve the detection of light elements (especially magnesium, aluminium, silicon and phosphorus) but it was still not possible to determine sodium.

The duration of each analysis was minimised to allow the collection of data from the largest possible number of panes (see Dungworth and Girbal 2011 for details). The analysis of a wide range of reference materials allowed the estimation of the likely analytical errors, precision and limits of detection (Table 2). For the light elements the accuracy and limits of detection are slightly inferior to the data that can be obtained using laboratory-based techniques and this is most marked for the lightest elements (especially magnesium). For heavier elements the accuracy and limits of detection are equal to or superior to those obtainable with laboratory-based techniques.

Table 2. Error and limit of detection (LoD) for the analysed oxides

Oxide	Error (1 sd)	Precision (1 sd)	LoD
MgO	0.3	0.3	2.0
$Al_2O_3$	0.7	0.1	0.5
SiO <sub>2</sub>	1.1	0.8	NA
$P_2O_5$	0.1	0.1	0.1
$SO_3$	0.05	0.02	0.2
Cl	0.05	0.02	0.2
$K_2O$	0.3	0.05	0.1
CaO	0.8	0.5	0.05
MnO	0.02	0.01	0.001
Fe <sub>2</sub> O <sub>3</sub>	0.05	0.01	0.001
CuO	0.02	0.01	0.001
ZnO	0.01	0.01	0.001
$As_2O_3$	0.01	0.005	0.001
$Rb_2O$	0.001	0.0002	0.001
SrO	0.005	0.0002	0.001
$ZrO_2$	0.005	0.0002	0.001

Tests undertaken on a range of flat glass have shown that a range of factors can have an impact on the quality of the chemical data that can be obtained using pXRF (Dungworth and Girbal 2011; Dungworth et al 2011). Tests on identical glass of varying thickness have detected systematic errors where the glass thickness is less than 2mm (Dungworth and Girbal 2011, Figure 4). The analysis of glass which has an applied layer of UV-absorbing film shows that light elements (up to calcium) are attenuated by such films and the degree of attenuation is inversely proportional to atomic number (Dungworth and Girbal 2011,

Figure 5). The pXRF analysis of weathered glass (especially where results could be directly compared with laboratory-based analyses of the same glass) has shown that it can be very difficult to obtain reliable, quantitative results from such glass (Dungworth and Girbal 2011, Table 6; Dungworth *et al* 2011). The effect of surface corrosion on the apparent composition of window glass as determined by pXRF has recently been examined in relation to some of the window glass from Thornhill church (Dungworth *et al* 2011). The weathered surface of glass usually has a different chemical composition to that of the uncorroded glass — in particular, it often contains reduced levels of alkalis and some other elements. Low-energy X-rays (typically <3kV) characteristic of light elements (Mg–K) are easily absorbed and a corroded surface may completely absorb such X-rays (leading to a reduction in their apparent concentration, or even a failure to detect them completely). The degree to which the pXRF detection of light elements will be affected by surface corrosion will be in inverse relationship to the atomic number of the element in question. The phenomenon will also be most marked in those glasses which display the most severe surface corrosion.

The examination of the data obtained from the pXRF analysis of historic window glass at lghtham Mote quickly showed that corrosion and other factors had a significant impact on the apparent chemical composition. Some panes of glass could easily be assigned to a particular glass type within the model proposed by Dungworth (2011) but others had compositions which could not be reconciled with the model described above (cf Figure 1). Some pXRF analyses indicated potassium and calcium concentrations that were well within conventional limits for HLLA glass but no phosphorus was detected. The absence of phosphorus would, according to the proposed model (Dungworth 2011), lead to these panes of glass be assigned to a post-1830, synthetic soda SLS group.

There are additional problems with some of the Ightham Mote pXRF data, although these only became fully apparent months after the data was acquired. Data was collected over a period of five days (Monday to Friday). On Thursday the protective polyimide film in front of the detector was replaced twice. The purpose of the film is to prevent dust and other material accidentally entering the instrument and damaging delicate components (such as the detector window). In addition, the protective film serves to maintain the helium flush inside the instrument when this is employed. The film is very thin (to reduce the attenuation of low-energy X-rays) and so is easily damaged. A visual examination of the film shortly before midday on Thursday prompted the replacement of the film. This was repeated at the end of the working day on Thursday. If all of the SLS glass results are examined in the order in which they were collected (Figures 8 and 9) it is apparent there are two periods on Thursday (9am to 12 noon, and 4:30pm to 7:00pm) when the results are anomalous (reduced silicon and spurious phosphorus measurements). With hindsight, it can be suggested that the protective film was compromised between 4pm Wednesday and 9am Thursday leading to a degradation of the helium flush and consequent effects on

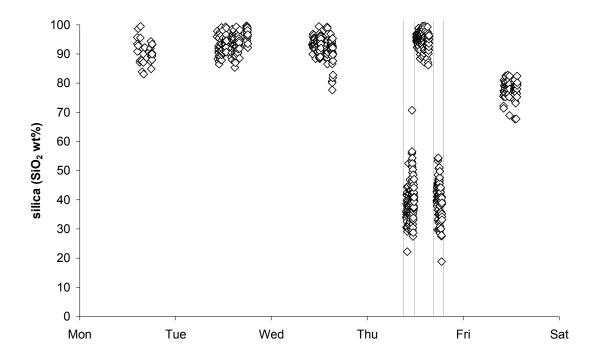


Figure 8. Apparent silicon concentration in all analysed SLS glass showing the effects of two episodes on Thursday when the protective film was compromised

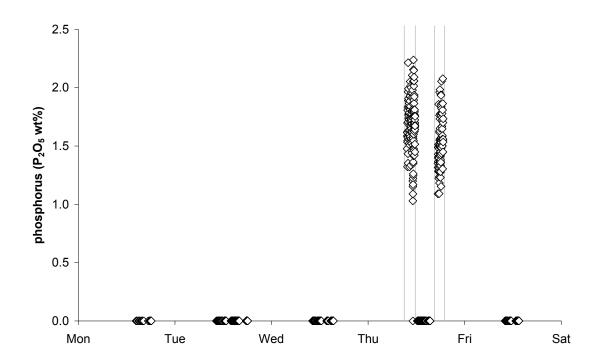


Figure 9. Apparent phosphorus concentration in all analysed SLS glass showing the effects of two episodes on Thursday when the protective film was compromised

the determination of many light elements. The reported silicon concentrations (Figure 8) are significantly lower than those on other days (and magnesium and aluminium were not

detected in any of these samples). In addition the pXRF reports the detection of phosphorus in these samples even though this element should be absent from SLS glass made using synthetic soda (Figure 9). The replacement of the protective film at Thursday lunchtime ensured subsequent data were reliable, but that the problem recurred in the mid-afternoon.

While the Dungworth (2011) model can be easily applied to quantitative data obtained through laboratory-based analyses of prepared samples, it appears to be less reliable when pXRF is applied to weathered glass. The data available so far suggest that this unreliability is most marked for the older and most weather glass.

In order to overcome the limitations imposed by the effects of weathering (and other factors) on the pXRF *in situ* analysis of window glass, the chemical composition of different types of glass has been reconsidered. The pXRF data appears to be least likely to be altered by weathering (and other effects) for heavy elements (eg rubidium and strontium). In addition, the pXRF actually offers superior limits of detection, accuracy and precision for these heavy elements (compared to the laboratory-based instruments used during the first phase of this project). While data collection for these heavier elements was not systematically carried out for these heavier elements during the first phase of the project, sufficient data is available to suggest that the major glass types described in Figure I can also be identified using just the concentrations of rubidium and strontium (Figure I0).

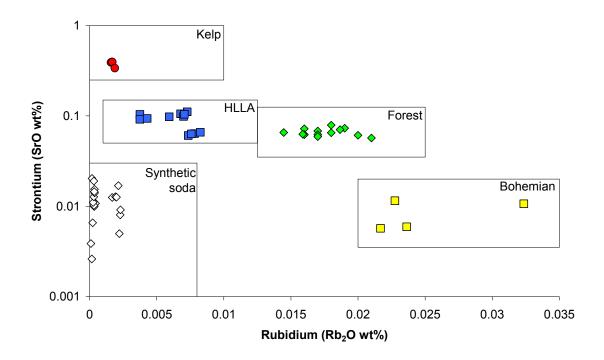


Figure 10. Rubidium and Strontium concentrations for some samples of historic glass (using data from Dungworth and Paynter 2010; Dungworth and Girbal 2011; unpublished ICPMS data)

#### **RESULTS**

A total of 1939 panes of glass from 32 windows were analysed using the pXRF; the data are reported in full in the appendices. The results are discussed below on a room by room (and occasionally window by window) basis. In some cases every available pane of glass was analysed (although panes smaller than the head of the instrument [~5cm] could never be analysed) but in most cases a selection of panes was made.

#### Great Hall

The Great Hall contains two windows (W01 and W02). W01 is in the Decorated style and probably originated as part of the original building; it does not, however, seem to be in its original location (Fowler and Kenwright 1988, 2). If this window has been moved then it is likely that at least a proportion of the glass will not be original. W02 is in the Perpendicular style and can be closely dated. The use of royal Tudor badges and badges commemorating the marriage of Henry VII and Catherine of Aragon indicate that the window was commissioned by Sir Richard Clement. As Clement only bought lghtham in 1521 and Henry approached the Pope for an annulment for his marriage to Catherine in 1529, the window must have originated in this period. Several glaziers have added their names and dates (James More 1793 and W Baker 1799) to panes in W02 and this has been interpreted by Starkey as representing the resetting of the glass. The variety of tints within this window, however, may indicate that at least a proportion of the extant glass represents later replacements (some possibly at the end of the 18th century).

#### W0I

This window contains a total of 473 separate panes of glass in five panels. The glass comprises small diamond-shaped panes of varied surface finish and tint — although none appear to be deliberately coloured. A total of 67 panes from four panels were analysed (14%); due to limited access none of the panes from the top central panel were analysed (Table 3). Even for those panels which were accessible, some panes were too small (<5cm across) to allow analysis with the pXRF.

The panes can be divided into a series of groups based on their tint and chemical composition. The most abundant group is a pale blue-green high-lime low-alkali glass (33 panes). This glass type could be identified through its calcium content, however, the apparent composition of a few panes diverged from the model set out previously (Figure I). Magnesium and phosphorus have been seen as important indicators of the use of plant ashes (Dungworth 2011) but the pXRF failed to detect these elements (Figure 11) in seven of the HLLA panes (ie a 'failure' rate of 21%). As discussed above, this 'failure' is likely to be due to the presence of corrosion on the surface of the glass. The trace elements rubidium and strontium provide a strong separation between the plant ash glasses (HLLA in this case) and the synthetic soda SLS glasses (Figure 12). Trace elements

in the HLLA glass (eg manganese, arsenic, rubidium, strontium and zirconium) suggest the presence of two slightly different compositional groups. HLLA1 has a rather low manganese content and may have been manufactured in 17th century (Phase 2b in Table 1), while HLLA2 has a higher manganese content and may have been made in the late 16th century (Phase 2a in Table 1).

Table 3. WOI panes analysed

Panel	Ref	Total	Analysed	Rate (%)
Top central		57	0	0
Upper left		112	18	16
Upper right	2	110	19	17
Lower left	3	97	15	15
Lower right	4	97	15	15
All		473	67	14

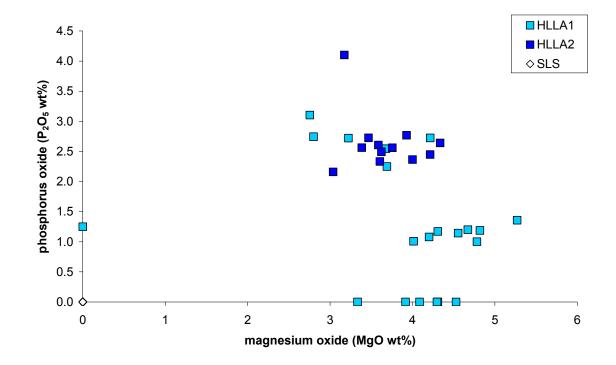


Figure 11. Magnesium and phosphorus content of the analysed panes from W01. The low levels of phosphorus detected in some of the HLLA glass (and its apparent absence from some samples) is likely to be due to the effects of surface corrosion.

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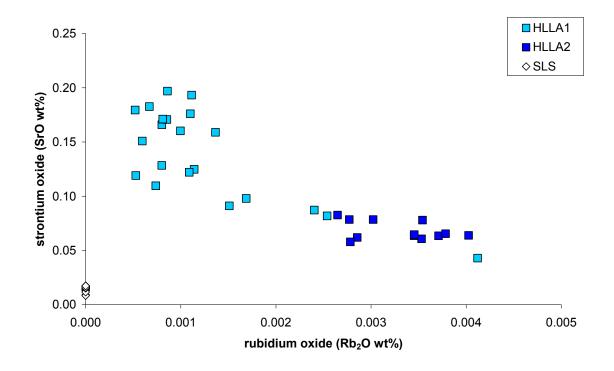


Figure 12. Rubidium and strontium content of the analysed panes from W01

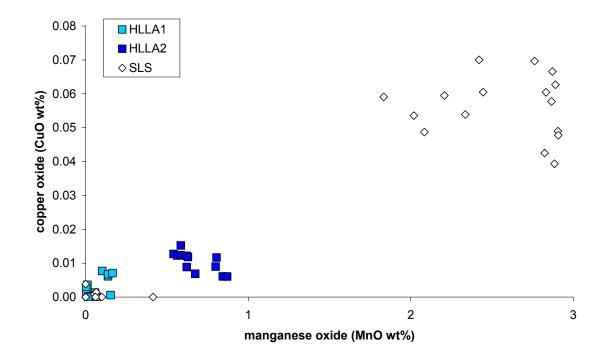


Figure 13. Manganese and copper content of the analysed panes from W01

All but one of the remaining analysed panes (8 pale green, 8 pale amber and 17 colourless) are made from soda-lime-silica (SLS) glass typical of the period from c1835 to c1930 (Phase 4 in Table 1). The colourless SLS has a low iron content and in most respects resembles ordinary plain glazing of the 19th century (cf Table 1). The amber and

pale green SLS glass contain elevated levels of manganese, iron and copper (Figure 13, Table 4). It is likely that these elements were deliberately added to ordinary SLS glass in an attempt to achieve tints which would match those of the HLLA glass.

Table 4. Average composition of the main glass types from W01

Туре	MgO	P <sub>2</sub> O <sub>5</sub>	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	CuO	Rb₂O	SrO	ZrO <sub>2</sub>
HLLAI	3.9	1.3	2.5	22.3	0.05	1.17	< 0.0	0.001	0.142	0.009
HLLA2	3.7	2.6	3.9	25.6	0.68	1.21	0.01	0.003	0.068	0.031
SLS (clls)	<2	<	<0.1	14.3	0.07	0.20	< 0.01	< 0.001	0.014	0.005
SLS (amber)	<2	<	0.1	12.6	2.87	0.62	0.05	< 0.001	0.016	0.003
SLS (pl gr)	<2	<	0.1	13.1	2.26	0.92	0.06	< 0.00	0.014	0.005

#### W02

Window W02 comprises over 1600 panes of glass (Figure 14). Most of these are small diamond-shaped panes of varied surface finish and tint. Due to limitations of physical access and time a selection of panes were analysed but this included most of those panes that were readily accessible.

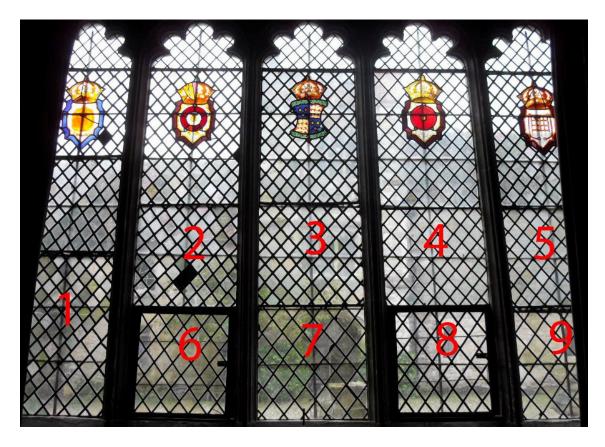


Figure 14. W02 showing the location of the analysed panels (note the different sizes of pane in Panel 1)

A total of 418 individual panes of glass from nine different panels were analysed (Figure 14, Table 5). For most of these panels all of the glass that could be analysed was analysed — the remaining panes being too small for pXRF analysis. The window contains a further 11 panels with approximately 920 panes which were not analysed. The upper parts of the window (including the decorated 16th-century glass) were not accessible. Overall, approximately 26% of the panes from this window were analysed.

Table 5. W02 panes analysed (does not include details of the unanalysed panels)

Panel	Total	Analysed	Rate (%)
	125	96	77
2	86	54	63
3	90	60	67
4	95	47	49
5	90	60	67
6	48	30	63
7	60	31	52
8	49	9	18
9	55	31	56
All	698	418	60

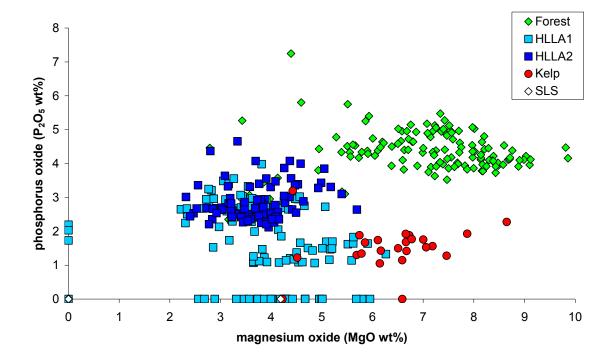


Figure 15. Magnesium and phosphorus content of the analysed panes from W02. The low levels of magnesium and phosphorus detected in some of the HLLA and kelp glass (as well as the apparent absence of these elements from some samples) is likely to be due to the effects of surface corrosion.

A careful consideration of the chemical compositions (including major and minor components, as well as trace elements) indicates that W02 contains 137 panes of forest

glass, 204 panes of HLLA glass, 24 panes of kelp glass and 55 panes of SLS glass (Table 7). In many respects the apparent chemical compositions correspond to the model set out previously (Table 1; Figure 1). On average, the forest glass contains more magnesium, phosphorus and potassium than the HLLA glass, while the kelp glass contains more magnesium than the HLLA glass, but less phosphorus (Figure 15). Nevertheless, the pXRF failed to detect either magnesium or phosphorus in 29 panes of HLLA glass (all from HLLA1) and 2 of the kelp panes (failure rates of 7% and 2%). The heavy, trace elements, however, allowed the accurate identification of the principal glass types (Figure 16).

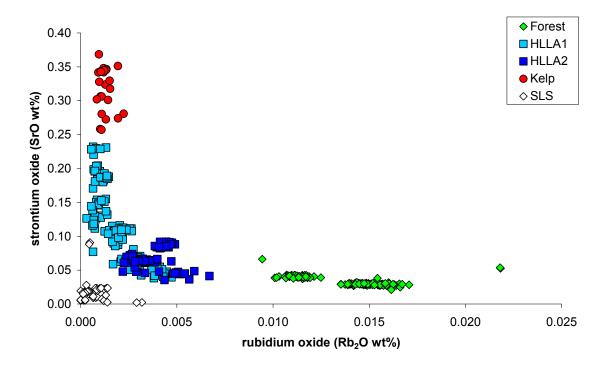


Figure 16. Rubidium and strontium content of the analysed panes from W02

The concentrations of a variety of minor and trace elements suggest the presence of several compositional sub-groups (Tables 6 and 7).

The forest glass can be divided into two sub-groups (as well as several outliers). Despite the differences in a few minor and trace elements (eg iron, copper, rubidium and strontium) these two glasses share almost identical overall compositions. It is likely that these two forest glasses were made using very slightly different raw materials. The significance of these differences is not immediately apparent. It is likely that these two glasses were made at different times or in different places, however, there is insufficient data available on medieval forest glass to allow a definitive statement. Nevertheless, the existence of two sub-groups and the limited variation within each suggests that these two sub-groups represent two different batches of glass manufacture. It is striking that this same division is apparent in forest glass from the New Chapel (see below).

The separation into HLLA1 and HLLA2 corresponds to that seen in W01 (higher manganese, copper, zinc, arsenic and zirconium in the latter sub-group) and the first sub-group (Phase 2a in Table 1) is probably earlier than the latter (Phase 2b in Table 1). The trace elements in both of these groups show some clustering which indicates at least the presence of several batches. These fine sub-groups may indicate glass obtained at different periods or from different sources, however, there are insufficient data on HLLA glass to allow any definitive statement. Some of these compositional clusters appear to be similar to some of those identified in other windows, such as those of the New Chapel (see below).

The presence of 24 panes of kelp glass was clearly identifiable through elevated strontium content (Table 7; Figure 16). Other aspects of the composition of this glass type, such as the low manganese content, are paralleled in kelp glass analysed previously.

The SLS glass present in W02 is identifiable through its low levels of strontium and rubidium (Figure 16). There are two analysed panes (W02.04.10 and W02.07.09) which in most respects appear to be SLS glass but which contain much higher levels of potassium (4–5wt%  $K_2O$ ) than would be anticipated from previous work (cf Table 1). The potassium concentration is much lower than the 'Bohemian' glass identified at Walmer Castle (Dungworth and Girbal 2011). The low levels of rubidium and strontium suggest the glass was not made using a plant ash and so it has been grouped with the SLS glass (this glass type is designated HiK).

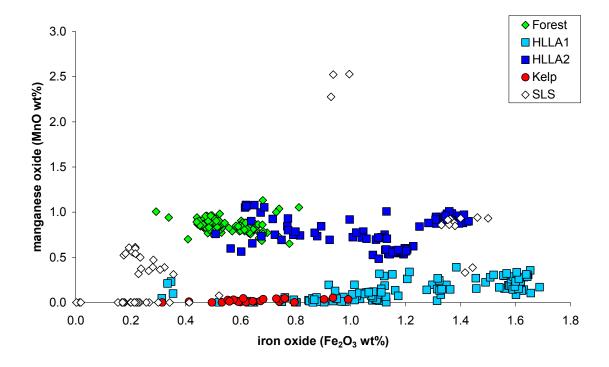


Figure 17. Iron and manganese content of the analysed panes from W02

Most of the SLS panes have iron and calcium contents that are typical of the 19th century (Phase 4 in Table 1), although some have much higher levels of iron ( $\sim$ 1.4wt% Fe $_2$ O $_3$ ). It is likely that the SLS glasses with elevated iron (Figure 17) were deliberately formulated to have a distinct colour in an attempt to match the colour of medieval window glass (cf Dungworth *et al* 2010). This SLS glass does not, however, match the deliberately coloured SLS glass in WO1 — this suggests that the installation of deliberately coloured SLS glass as part of the restoration of these two windows occurred at different times (or that the work was carried out by two different workshops).

Table 6. Average composition of the main glass types from W02

Туре	MgO	P <sub>2</sub> O <sub>5</sub>	K₂O	CaO	MnO	Fe₂O₃	CuO	Rb₂O	SrO	ZrO <sub>2</sub>
Forest I	6.3	4.7	9.4	15.8	0.82	0.64	0.03	0.011	0.041	0.014
Forest2	7.7	4.2	9.5	14.9	0.87	0.49	0.01	0.015	0.029	0.012
HLLAI	3.8	1.8	3.6	21.4	0.14	1.18	< 0.01	0.002	0.116	0.012
HLLA2	3.7	2.9	4.5	24.0	0.78	1.06	0.01	0.004	0.069	0.027
Kelp	6.2	1.5	3.6	11.0	0.02	0.64	< 0.0	0.001	0.306	0.005
SLS (clls)	<2	<	0.5	14.4	0.19	0.23	< 0.01	0.001	0.011	0.005
SLS (amber)	<2	<	0.1	12.7	2.44	0.95	0.06	< 0.00	0.016	0.005
SLS (v pl gr)	<2	<	0.7	17.1	0.90	1.39	< 0.0	0.001	0.023	0.008

Table 7. Proportion of different glass types within different panels of W02

Panel	Forest	HLLAI	HLLA2	Kelp	SLS	All
T	11 (11%)	22 (23%)	42 (44%)	3 (3%)	18 (19%)	96
2	27 (50%)	6 (11%)	14 (26%)	0 (0%)	7 (13%)	54
3	40 (66%)	7 (12%)	7 (12%)	0 (0%)	6 (10%)	60
4	18 (38%)	15 (32%)	2 (4%)	10 (21%)	2 (4%)	47
5	41 (68%)	8 (13%)	9 (15%)	2 (3%)	0 (0%)	60
6	0 (0%)	16 (53%)	9 (30%)	4 (13%)	I (3%)	30
7	0 (0%)	20 (64%)	0 (0%)	3 (10%)	8 (26%)	31
8	0 (0%)	0 (0%)	0 (0%)	0 (0%)	9 (100%)	9
9	0 (0%)	25 (81%)	0 (0%)	2 (6%)	4 (13%)	31
All	137 (33%)	119 (28%)	83 (20%)	24 (6%)	55 (13%)	418

In panel I, all of the forest, kelp and HLLA2 glass is found in the top left section of the window (ie the region with the smaller panes). The bottom right portion with the larger panes is made from HLLA1 and SLS glass (Figure 18). The distribution of SLS glass (eg the placement of a coloured pane in-between two colourless panes) suggests that the coloured and colourless panes were carefully placed to blend as much as possible with the existing glass. It is likely that the coloured SLS glass was deliberately made in order to blend with existing older glass panes, however, these panes generally have a stronger colour than the HLLA and forest glasses they were supposed to match. The variety of glass types (as well as pane size) suggest that this window was assembled using glass from several different earlier windows. The presence of a high proportion of HLLA glass could indicate that the window has a 17th-century origin. The presence of SLS glass indicates repairs (and possibly a complete assembly) occurred in the 19th century.



Figure 18. W02 Panel 1 showing the spatial distribution of glass types (green = forest glass; pale blue = HLLA1; dark blue = HLLA2; red = kelp; white = SLS [c = colourless, a = amber, vpg = very pale green], grey = not analysed)

Panels 2–5 display some similarities, in particular they all contain a high proportion of forest glass (Figures 19–22). Two-thirds of the glass in panels 3 and 5 is forest glass and this glass would have been manufactured before the late 16th century. This glass is of the general type that would have been used to make the Clement window (1521–1529); however, there is no certainty that any of this glass is original to this window.



Figure 19 W02 Panel 2 showing the spatial distribution of glass types (see Figure 18 caption)

As mentioned above, the trace elements (especially rubidium) suggest the presence of two sub-groups of Forest glass but examples of both sub-groups are present in each of these panels. The window clearly underwent extensive repair and restoration at some later date and, while this made use of medieval glass, this may not have originally been in this window.



Figure 20 W02 Panel 3 showing the spatial distribution of glass types (see Figure 18 caption)

The presence of HLLA, kelp and SLS glass indicates that some repair occurred after the late 16th century. It is possible that repairs were carried out as an when required over the following centuries, however, there are some indications that the windows are largely the product of rather late repair and that much of the HLLA and kelp glass was anachronistic when it was installed.

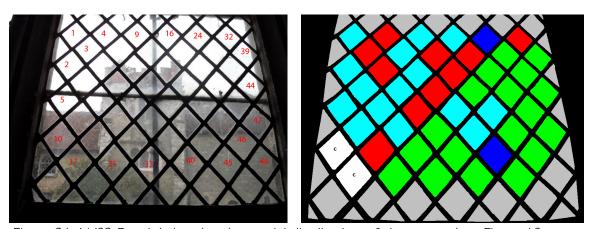


Figure 21 W02 Panel 4 showing the spatial distribution of glass types (see Figure 18 caption)

A significant proportion of the SLS glass in these panels was deliberately coloured (Figure 15), presumably to match the original glass, although, the deliberately coloured SLS glass is frequently more strongly coloured than the forest glass it was supposed to match. This clearly indicates that there was a period of repair and restoration in the 19th century. The spatial arrangement of the various panes (eg Figure 21) suggests that HLLA and kelp glass

were installed together even though there was little or no contemporary production of these two types of glass.

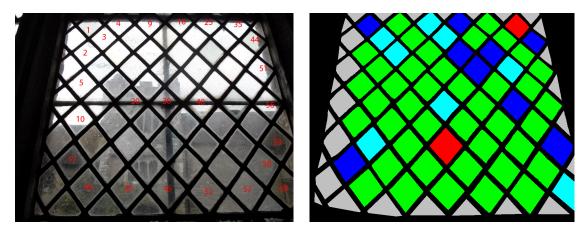


Figure 22 W02 Panel 5 showing the spatial distribution of glass types (see Figure 18 caption)

It is proposed that the windows underwent major repair/restoration in the 19th century and that the glaziers who undertook this work made use of window glass reclaimed from other windows (and these may not all have been at Ightham Mote). Most of the medieval forest glass belongs to one of two tight compositional groups which suggests that this glass derived from a restricted number of sources (and all may have originally been installed at Ightham).

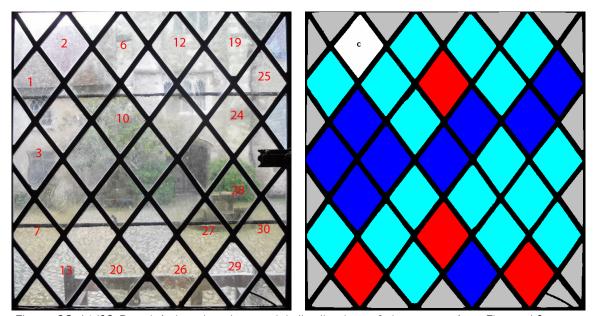


Figure 23 W02 Panel 6 showing the spatial distribution of glass types (see Figure 18 caption)

Panels 6–9 contain no samples of forest glass (Table 8, Figures 23–25): all of the glass was produced after the late 16th century and is not contemporary with the Clement window. Panel 6 contains HLLA (both sub-groups) and kelp glass (Figure 21) but has no glass that

was produced after 1830 (although the panel may have been assembled at almost any date after the late 16th century).

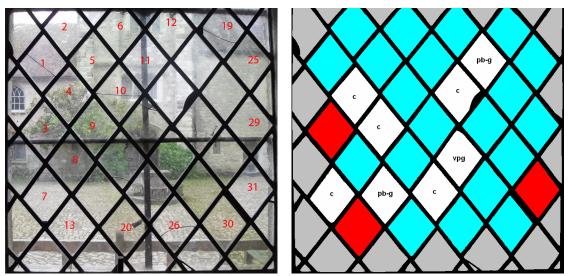


Figure 24 W02 Panel 7 showing the spatial distribution of glass types (see Figure 18 caption)

Panel 7 mostly contains HLLA1 glass (Figure 24) with a few panes of kelp glass and SLS glass (both colourless and deliberately coloured varieties). Panel 8 (not illustrated) contains only SLS glass and this all shares the same composition. The iron content of this glass suggests that it was produced in the 19th century (Phase 4 in Table 1). Panel 9 mostly contains HLLA1 glass (Figure 25) with two panes of kelp glass and four of SLS glass (colourless).

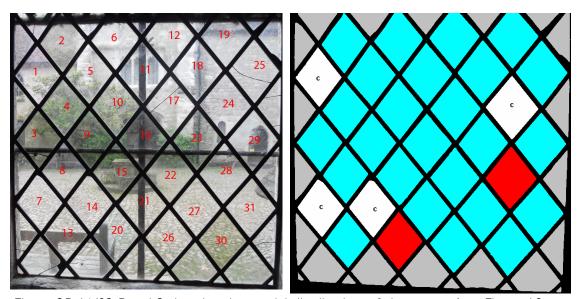


Figure 25 W02 Panel 9 showing the spatial distribution of glass types (see Figure 18 caption)

#### Outer Hall and Library

Five windows in the Outer Hall (W03) and Library (W04–W06) were analysed. Windows W03 and W07 are considered together as both are in the same style (probably early 19th-century) and face onto the courtyard. Windows W04–W06 are all in the same style (casement windows with small diamond-shaped panes) and face from the library over the moat.

#### W03 and W07

These windows both comprise a lower sash with eight rectangular panes and an upper sash with ten curved panes in a Gothic revival style (Figure 26). None of the panes has a strong tint. The relatively small number of panes in each window (18) allowed the analysis of all available panes in these windows.

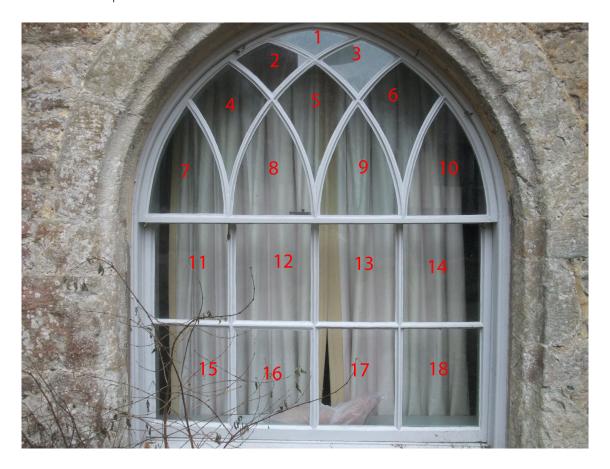


Figure 26. Window W07

Analysis shows that a few panes are kelp glass while all the others are SLS glass (Figures 27–28). The kelp glass displays little compositional variation and cannot be distinguished chemically from kelp glass in W02. The calcium and iron content of the SLS glass suggests

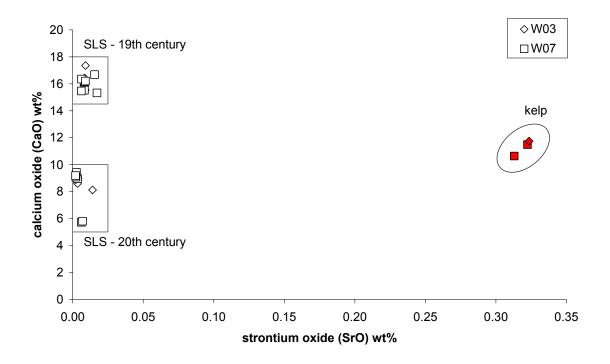


Figure 27. Calcium and strontium content of the analysed panes from W03 and W07

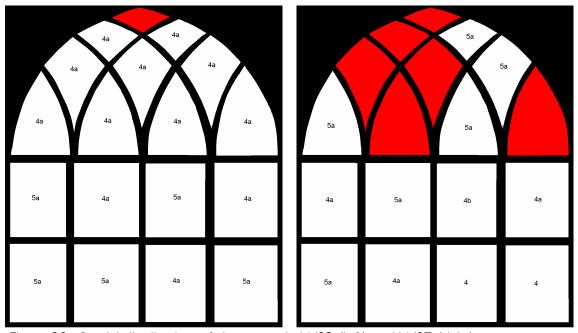


Figure 28. Spatial distribution of glass types in W03 (left) and W07 (right) (red = kelp, white = SLS, numbers refer to period types in Table 1)

that some is likely to be 19th-century (Phase 4 in Table 1) but that most would have been manufactured in the 20th century (Phase 5). Some of the panes contain low levels of calcium and so are most likely to be of 20th-century manufacture (after the development of drawn or float production techniques), however, magnesium was not detected in any of these panes. The reasons for the failure to detect magnesium are

uncertain, although surface weathering and/or adhering films of dirt may be responsible for the absorption of the low-energy X-rays characteristic of magnesium.

The presence of kelp glass indicates that the windows were probably first created between c1700 and c1835 (Phase 3 in Table 1). Given the style of the windows it is likely that they were made towards the end of this period. The surviving panes of original kelp glass are restricted to the upper sash; it is likely that the lower sash has been subject to the most movement and that this has led to breakages and replacements. The presence of SLS glass suggests that accidental breakage has led to replacement at various times since then (including two from W07 which were probably installed after c1960).

#### Windows W04-W06

Windows W04–W06 are all constructed in the same style (Figure 29). These are casement windows containing large numbers of small diamond-shaped panes with few if any differences in tint, thickness or surface texture. Given the number of panes and the limited time available for analysis a few panes from each panel in each window were selected for analysis (~18% of the available panes).



Figure 29. Window W06 showing the analysed panes

One pane of glass (from W06) is a kelp glass while all the others are SLS glass. A range of elements all suggest that both 19th-century (Phase 4 in Table 1) and 20th-century glass (Phase 5) is present. The samples with relatively high calcium (>10wt% CaO) are likely to have been manufactured in the 19th century (Phase 4) while those with <10wt% CaO were probably made after the mechanisation of the flat glass industry (Phase 5). The panes with the lowest calcium (<6wt% CaO) may have been made after the development of the float process (Phase 5b). The pXRF did not detect magnesium in any

of the SLS glass although this should be present (2.5–4wt% MgO) in the Phase 5 glass. The failure to detect magnesium in these panes is almost certainly related to the problems noted with damage to the protective film over the pXRF and maintaining a helium flush. These windows were analysed between 9:40am and 11:40am on the Thursday morning (cf Figures 8 and 9).

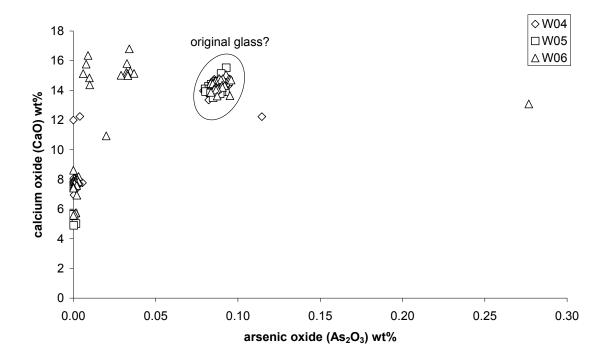


Figure 30. Arsenic and calcium content of the analysed panes from W04–W06

Among the 19th-century panes there is a tight compositional group (Figure 30, Table 8). The 82 panes of this glass were almost certainly made at the same time and place and installed at Ightham Mote at the same time. The absence of potassium from this glass, but the presence of arsenic, suggests manufacture between c1835 and c1870 (Phase 4a).

Table 8. Average composition of the principal (original?) SLS glass in W04–W06

Window	No	%	CaO	Fe <sub>2</sub> O <sub>3</sub>	$As_2O_3$	SrO	ZrO <sub>2</sub>
W04	26	54	14.1±0.3	0.13±0.01	0.087±0.004	$0.0081 \pm 0.0004$	0.0129±0.0009
W05	30	83	14.2±0.4	0.13±0.01	$0.087 \pm 0.004$	$0.0081 \pm 0.0004$	$0.0131 \pm 0.0009$
W06	26	37	14.4±0.4	$0.13 \pm 0.01$	$0.089 \pm 0.004$	0.0082±0.0004	0.0133±0.0012

#### Squire's Room (W09–W13)

The five windows of the Squire's Room (W09–W13) are broadly similar to those of the outward facing windows of the Library (W04–W06). These windows are casement windows each with 70–200 diamond-shaped panes; most of which have no distinct colour or tint. A total of 184 panes were analysed — a 28% sample.

The chemical analysis indicates that most panes are SLS glass, although four from W10 are kelp glass and three others could not easily be categorised. These last three panes contain more strontium than is normal for SLS glass but much less rubidium than would be expected for a plant ash glass.

The SLS glass can be divided into three compositional groups which correspond to Phases 4, 5a and 5b (Figure 31, cf Table 1). Most of the Phase 4 SLS glass contains little or no arsenic (but does contain small proportions of potassium) and so is likely to have been manufactured in Phase 4b (c1870 to c1930).

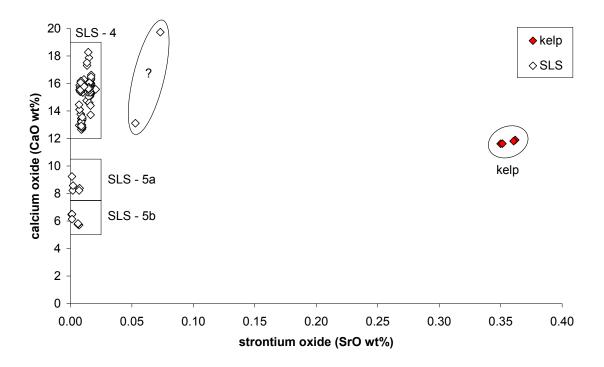


Figure 31. Strontium and calcium content of the analysed panes from W09–W13

### Butler's Pantry (W19)

The Butler's Pantry includes a casement window with diamond-shaped panes similar to those of the Library and the Squire's Room. The chemical analysis indicates that all these panes are SLS glass with the presence of four distinct compositional groups (Figure 32). Groups A–C contain relatively high levels of calcium and are likely to belong to Phase 4 (c1835–c1930). Magnesium was detected in group D (Table 9) helping to confirm that this glass belongs to Phase 5, and probably to Phase 5a (c1930–c1960).

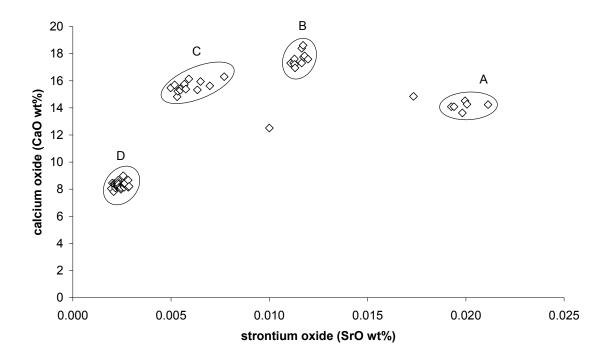


Figure 32. Strontium and calcium content of the analysed panes from W19

Table 9. Average composition of the principal SLS glass in W19

	No	MgO	K20	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	$As_2O_3$	SrO
Α	6	<2	0.63±0.03	14.1±0.3	0.46±0.03	0.28±0.03	0.57±0.02	0.0199±0.0007
В	11	<2	0.19±0.01	17.6±0.5	$0.26 \pm 0.02$	$0.27 \pm 0.02$	$0.27 \pm 0.02$	0.0115±0.0003
C	14	<2	< 0.05	15.6±0.4	< 0.02	$0.19 \pm 0.02$	< 0.01	$0.0059 \pm 0.0008$
D	34	$3.5 \pm 0.4$	< 0.05	8.3±0.2	< 0.02	0.07±0.01	< 0.01	0.0024±0.0002

#### Billiard Room (W29 and W30)

The windows of this room comprise diamond-shaped panes similar to those of the Library. All of these windows have UV-absorbing films on the interior surfaces and so only the two windows facing the courtyard (W29 and W30) were accessible (and analysed from the outside). All but three of the analysed panes share identical chemical compositions and were clearly made and installed at the same time. This is a SLS glass with a relatively high calcium content indicating manufacture in Phase 4 (Table 10). The absence of potassium and the presence of arsenic suggests the glass belongs to Phase 4a (c1835–c1870). Almost all of the elements detected showed concentrations that are indistinguishable from those of the original glass employed in the Library. The concentrations of zirconium, however, are sufficiently different to be sure that the window glass employed in these two rooms was obtained from different sources (and probably at different times).

Table 10. Average composition of the principal SLS glass in W29 and W30 compared to that in W04–W06

Window	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	As <sub>2</sub> O <sub>3</sub>	SrO	ZrO <sub>2</sub>
W29 & W30	<0.1	15.9±0.4	< 0.02	0.14±0.01	0.088±0.004	0.0082±0.0004	0.0063±0.0005
W04-06	<0.1	14.2±0.4	< 0.02	0.13±0.01	0.087±0.004	$0.0081 \pm 0.0004$	$0.0131 \pm 0.0010$

#### New Chapel (W41–W49)

While the ceiling of the New Chapel contains similar badges to Window W02 in the Great Hall, and so can be attributed to the 1520s, the windows obviously contain glass that was not original. The decorated glass (Virgin and Child, St George and St John the Baptist) is not of English manufacture and was probably obtained via Hampp who dealt extensively in stained glass removed from continental churches. The origins of the undecorated glass, which comprises small diamond-shaped panes with a variety of surface finishes and tints (Figure 5), are uncertain.

None of the decorated glass likely to have been obtained from St Peter's, Cologne, and installed at some point during the 19th century was analysed (W44 and W46). Due to limitations on time available for analysis a sample of the plain glass was analysed using pXRF (Table 11).

Table 11. Number of panes and number and proportion analysed from W41–W49

	Panes	Analysed	%
W41	266	50	19
W42	504	97	19
W43	495	64	13
W44	240	30	13
W45	480	64	13
W47	496	64	13
W48	512	47	9
W49	111	28	25
All	3104	444	14

The pXRF analysis showed several different types of glass were present (Figure 33), including forest, HLLA and SLS glass. As with the glass from W02, attempts to categorise the glass on the basis of light elements alone resulted in some misidentifications (Figure 34). The 34 panes of forest glass include one example where magnesium was not detected (a failure rate of 3%). Out of the 60 HLLA1 panes, magnesium was undetected in eight cases, and phosphorus in nine (a failure rate of 28%). The 135 panes of HLLA2 glass included 22 where magnesium was undetected (a failure rate of 16%). Among the 215 panes of SLS glass have been included 16 panes with levels of potassium (3–5wt%  $K_2O$ ) that are much higher than is normal for SLS glass. This glass (HiK) is similar to that from W02 mentioned above — it is not 'Bohemian' and, except for the potassium content, the closest parallel is SLS glass of Phase 4 or 5. Most of the remaining SLS panes

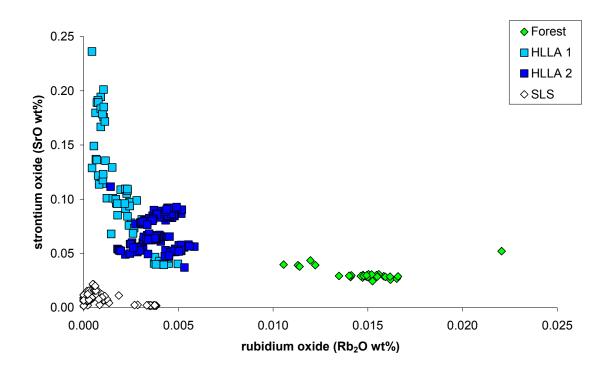


Figure 33. Rubidium and strontium content of New Chapel window glass (W41–W49)

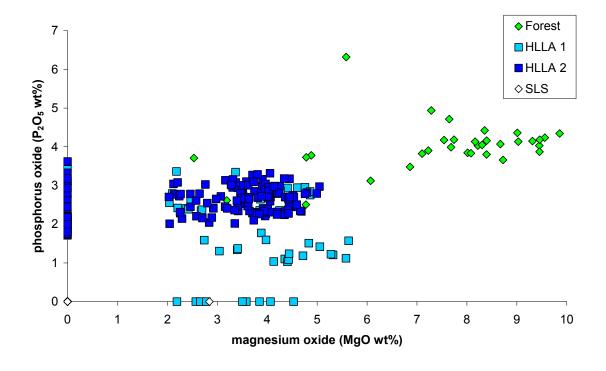


Figure 34. Magnesium and phosphorus content of New Chapel window glass (W41–W49). The low levels of magnesium and phosphorus detected in some of the HLLA and kelp glass (as well as the apparent absence of these elements from some samples) is likely to be due to the effects of surface corrosion.

have calcium concentrations which indicate that they belong to Phase 4 rather than Phase 5.

The forest glass appears to have two compositional groups similar to those seen in W02 (Figure 33, cf Figure 14). The HLLA glass has again been divided into HLLA1 (Phase 2a) and HLLA2 (Phase 2b). The concentrations of a range of minor and trace elements in the HLLA suggest the possibility of a number of compositional sub-groups, although there are no obvious correspondences with the possible compositional sub-groups present in the HLLA glass from W02.

Some of the SLS glass has iron concentrations similar to those seen in contemporary plain glazing, but some has higher concentrations of iron and some also contains manganese and/or copper (Figure 35). It is likely that these metals were deliberately added in order to provide the glass with a colour which would allow it to blend in with historic window glass. The tinted SLS glass includes a pale amber with relatively high concentrations of iron and manganese, a very pale blue-green with moderate iron and small amounts of copper, and a pale blue which contains very low levels of iron ( $\sim$ 0.05wt% Fe<sub>2</sub>O<sub>3</sub>) but some copper ( $\sim$ 0.2wt% CuO). None of the deliberately tinted SLS glass has a composition which matches exactly that seen in W02.

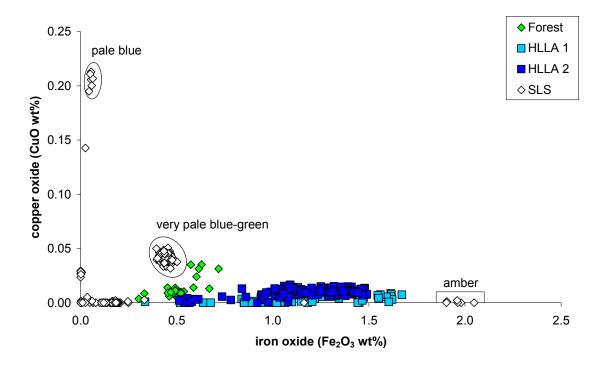


Figure 35. Iron and copper content of New Chapel window glass (W41–W49)

The presence of many different types of glass, especially deliberately tinted SLS glass suggests that these windows were assembled during the 19th century (Phase 4). The windows include some forest glass which could represent the original glass used in the New Chapel. The presence of two similar compositional sub-groups of forest glass in the

New Chapel and the Great Hall (W02) is noteworthy. It is likely that these two subgroups represent two different glass production sites (or possibly just separate periods when this glass was produced). The mixture of medieval forest glass from two different production sites in two different rooms suggests that this glass does not simply represent a random collection of medieval glass. Nevertheless the exact circumstances responsible for the glass ending up in its current locations are likely to remain uncertain.

Table 12. Number (and proportion) of analysed panes of different glass types from the new Chapel (W41–W49)

	Forest	HLLAI	HLLA2	SLS	All
W41	I (2%)	2 (4%)	31 (62%)	16 (32%)	50
W42	4 (4%)	15 (15%)	32 (33%)	46 (47%)	97
W43	6 (9%)	10 (16%)	21 (33%)	27 (42%)	64
W44	2 (7%)	I (3%)	2 (7%)	25 (83%)	30
W45	9 (14%)	10 (16%)	17 (27%)	28 (43%)	64
W47	5 (8%)	13 (20%)	16 (25%)	30 (47%)	64
W48	3 (6%)	4 (9%)	2 (4%)	38 (81%)	47
W49	4 (14%)	5 (18%)	14(50%)	5 (18%)	28
All	34 (7%)	60 (14%)	135 (30%)	215 (49%)	444

Table 13. Average composition of the main glass types from the New Chapel (W41–W49)

-	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	CuO	ZnO	As <sub>2</sub> O <sub>3</sub>	Rb₂O	SrO	ZrO <sub>2</sub>
Forestl	9.0	15.7	0.79	0.63	0.03	0.03	0.03	0.011	0.040	0.014
Forest2	9.4	15.8	0.88	0.48	< 0.01	0.03	0.02	0.015	0.029	0.012
HLLAI	3.5	21.8	0.11	1.19	< 0.01	0.01	0.01	0.002	0.111	0.012
HLLA2	4.2	24.2	0.75	1.15	< 0.01	0.03	0.10	0.004	0.069	0.026
SLS (colourless)	0.6	13.3	0.01	0.14	< 0.01	< 0.0	0.04	0.001	0.007	0.005
SLS (amber)	0.5	8.8	1.37	1.96	< 0.01	< 0.0	0.02	0.001	0.007	0.016
SLS (pale blue)	0.3	9.2	< 0.0	0.05	0.20	< 0.0	< 0.0	0.001	0.021	0.075
SLS (pale bl-gr)	0.2	14.9	0.08	0.44	0.04	< 0.01	0.06	< 0.001	0.011	0.002

# Chapel Corridor (W50)

This window comprises 174 diamond-shaped panes similar to those of the Library, of which 22 were analysed. The pXRF analysis indicates that all of the panes are SLS glass and that most have a high enough calcium content to suggest that they were manufactured in Phase 4 (c1835–c1930). Three panes contain relatively high proportions of potassium (HiK) for SLS glass (cf similar glass from the Great Hall and the New Chapel discussed above).

## Oriel Corridor (W57)

This window comprises just over 1000 diamond-shaped panes in 20 panels, of which 176 have been analysed. The glass has a variety of tints and surface finishes. The pXRF analysis indicates the presence of several different types of glass (Figure 36). Most of these are HLLA (105 panes) and SLS glass (65 panes) but there are also five panes of forest glass and a single pane of kelp glass. The major elements again failed to provide an infallible means of identifying the glass type. The pXRF analysis of the 59 HLLA1 panes only detected phosphorus in 48 cases (a failure rate of 19%). Despite this magnesium was detected in a proportion of the SLS glass; and in these the magnesium was generally highest in those samples with the lowest calcium (ie in conformity with the model set out in Figure 1). The calcium and magnesium contents suggest that 30 SLS panes were produced in Phase 4, 30 in Phase 5a and five in Phase 5b. A proportion of the SLS glass contains elevated levels of iron and other colouring metals, compared to contemporary plain window glass; it is likely that these metals were deliberately added in order to achieve a tint which would allow these panes to blend in with the older glass in this window. This deliberately tinted glass mostly belongs to Phase 5a (c1930 to c1960) and includes two varieties: the first (and most abundant) contains slightly elevated iron  $(0.43\pm0.02\text{wt}\% \text{ Fe}_2\text{O}_3)$  and copper  $(0.010\pm0.003\text{wt}\% \text{ CuO})$  while the second contains more iron  $(0.89\pm0.02\text{wt}\% \text{ Fe}_2\text{O}_3)$ , no copper (<0.01wt% CuO) and significant quantities of manganese (1.00±0.02wt% MnO).

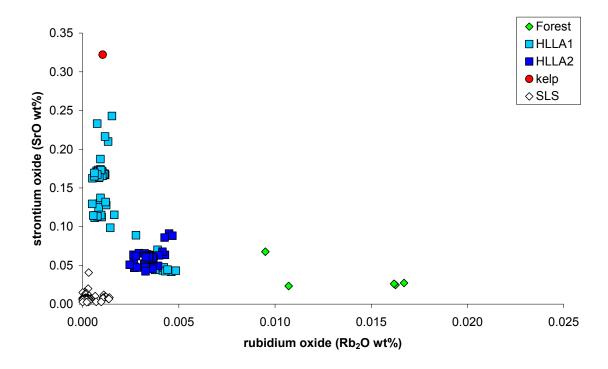


Figure 36. Rubidium and strontium content of Oriel corridor window glass (W57)

Table 14. Average composition of the major glass types from W57

	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	CuO	ZnO	As <sub>2</sub> O <sub>3</sub>	Rb₂O	SrO	ZrO <sub>2</sub>
Forest	9.1	15.5	0.96	0.46	0.01	0.03	0.01	0.014	0.034	0.010
HLLAI	2.6	20.8	0.06	1.15	< 0.0	0.01	< 0.01	0.001	0.143	0.009
HLLA2	4.3	24.9	0.60	1.06	0.01	0.03	0.10	0.003	0.059	0.030
SLS	0.2	12.0	0.10	0.33	< 0.0	< 0.01	0.12	< 0.001	0.008	0.005

## South West Stairs (W31)

This window comprises 273 small diamond-shaped panes with little or no tint or surface texture (58 were analysed). The pXRF analysis (< 0.002wt% Rb<sub>2</sub>O, < 0.02wt% SrO and  $0.16\pm0.04$ wt% Fe<sub>2</sub>O<sub>3</sub>) indicates that all of these panes are SLS glass of fairly recent manufacture (Phase 4 or 5). The light element data for these panes is, however, unreliable due to problems with the protective film and maintaining a helium flush. These windows were analysed between 5:30pm and 6:15pm (cf Figures 8 and 9).

# Charles Henry Robinson Dressing Room (W35)

This window comprises 260 small diamond-shaped panes with little or no tint or surface texture (47 were analysed). The pXRF analysis (< 0.002wt% Rb<sub>2</sub>O, < 0.02wt% SrO and  $0.13\pm0.04$ wt% Fe<sub>2</sub>O<sub>3</sub>) indicates that all of these panes are SLS glass of fairly recent manufacture (Phase 4 or 5). The light element data for these panes is, however, unreliable due to problems with the protective film and maintaining a helium flush. These windows were analysed between 5:00pm and 5:30pm (cf Figures 8 and 9). Most of the panes (41 out of 47) share identical composition with each other and with most of the glass from the outward-facing windows in the library (Table 15). It is likely that these windows (W04–W06 and W35) were installed at the same time (probably Phase 4a, c1835–c1870).

Table 15. Average composition of the principal SLS glass in W35 compared to that in W04–W06

Window	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	As <sub>2</sub> O <sub>3</sub>	SrO	ZrO <sub>2</sub>
W35	<0.1	14.5±0.5	< 0.02	0.14±0.01	0.089±0.005	0.0082±0.0004	0.0119±0.0008
W04-06	<0.1	14.2±0.4	< 0.02	0.13±0.01	0.087±0.004	$0.0081 \pm 0.0004$	0.0131±0.0010

# The Tower and Archaeology Room (W66–W70)

The Tower (including the room on the second floor used to display some archaeological materials) forms part of the western range likely to have been added in the 15th century. Glass from five windows was analysed: including three fairly small windows on the stairs (W66–W68) and two large windows in the Archaeology Room (W69 and W70). The windows are all composed of small diamond-shaped panes of varying tint and surface

finish. Time limitations required that only a sample (230) of the 989 panes were analysed and these included a range of glass types (Figure 37, Table 15). As with other windows discussed above, the apparent concentration of some minor elements (such as magnesium and phosphorus) produced potentially misleading results which would have led to some panes being assigned to the incorrect compositional group (37% of the HLLA1 panes and 14% of the kelp panes).

Forest glass was detected in both of the Archaeology Room windows (W69 and W70) but was absent from the windows on the stairs (Table 16). All but one of the forest glass panes appear to belong to the higher rubidium sub-group (cf Figure 16). HLLA glass was found in all but one window and includes both the earlier sub-type (HLLA2) with the elevated manganese and the later sub-type (HLLA1).

Table 16. Numbers of different types of window panes analysed from the Tower and Archaeology Room (W66–W70)

	Total	Forest	HLLAI	HLLA2	kelp	SLS	Analysed
W66	43	0	0	9	0	6	15
W67	37	0	6	2	3	3	14
W68	21	0	2	0	1	9	12
W69	456	6	16	47	4	34	107
W70	432	6	3	33	6	34	82

Table 17. Average compositions of the glass types from W66–70

	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	CuO	ZnO	As <sub>2</sub> O <sub>3</sub>	Rb₂O	SrO	ZrO <sub>2</sub>
Forest2	9.2	15.4	0.87	0.51	0.01	0.03	0.01	0.015	0.030	0.012
HLLAI	3.8	20.8	0.10	1.11	< 0.0	0.01	< 0.0	0.002	0.116	0.011
HLLA2	3.3	23.7	0.68	1.22	< 0.0	0.03	0.14	0.003	0.066	0.024
kelp	3.6	11.0	0.01	0.60	< 0.0	< 0.0	< 0.0	0.001	0.318	0.005
SLS	0.2	14.0	0.20	0.32	< 0.0	< 0.0	0.15	< 0.001	0.011	0.004
SLS (HiK)	2.9	5.9	< 0.0	0.02	0.08	0.03	0.16	< 0.001	0.002	0.006

A substantial proportion (37%) of all the analysed panes are SLS glass which would have been manufactured after c1835. Most of this SLS glass contains relatively high levels of calcium and was probably made during Phase 4 (c1835–c1930). Almost all of the low-calcium glass contains levels of potassium that are much higher than would be expected for Phase 4 or 5 glass (SLS HiK in Table 17). The exact origins of this glass are uncertain, however, it is likely that the glass is of relatively recent manufacture (19th- or 20th-century).

The SLS (and SLS HiK) glass includes some with iron concentrations that are typical of plain window glass of the 19th and 20th centuries, however, some contains elevated levels of iron as well as manganese and/or copper (Figure 38). There is little doubt that these metals were deliberately added to the glass used for these panes in order to achieve particular colours or tints.

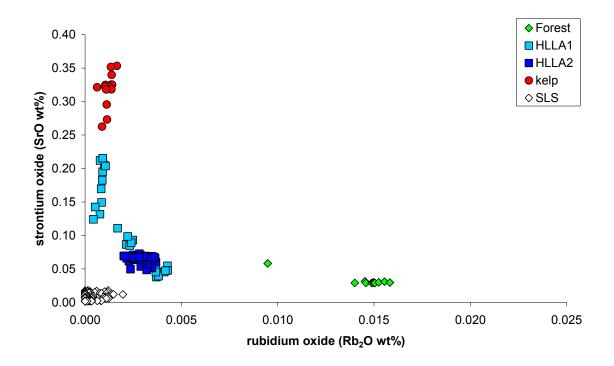


Figure 37. Rubidium and strontium content of the Tower and Archaeology Room window glass (W66–70)

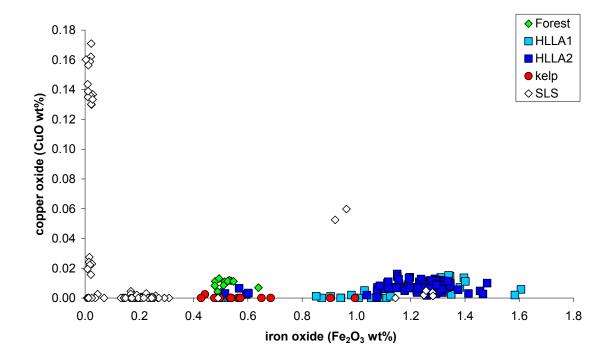


Figure 38. Iron and copper content of the Tower and Archaeology Room window glass (W66–70)

## DISCUSSION

The analysis of 1939 panes of glass from Ightham Mote provides a wealth of information on the suitability of pXRF for characterising historic window glass. The following discussion looks in detail at the pros and cons of pXRF and the nature (chemical composition) of the extant historic window glass at Ightham Mote.

## pXRF for in situ analysis of historic window glass: pros and cons

The main advantage offered by pXRF is the fact that it is not only a non-destructive technique but that the procedure can be used on *in situ* window glass and does no damage to the glass. No other analytical technique currently available can deliver non-destructive and damage-free chemical analysis for extant historic window glass. Where a window is undergoing conservation treatment it will often be possible to take samples and the analysis of such samples has the potential to provide detailed information on the nature of the glass. Nevertheless, there are many windows for which conservation treatment is not scheduled but which would benefit from a better understanding through chemical analysis.

The current state of pXRF detector technology allows the analysis of a window in as little as 30 seconds. This allows the acquisition of very large datasets that would not be feasible even if samples could be taken. While 1939 panes were analysed using pXRF at Ightham over a five-day period, the laboratory-based analysis of almost 800 glass samples for the first phase of the project took nearly five years to complete. A dataset as large as that acquired at Ightham Mote, however, requires considerably more than five days to fully analyse and interpret.

Table 18. Comparison of detection limits

Oxide	SEM/XRF (lab)	pXRF
Na <sub>2</sub> O	0.1	NA
MgO	0.1	2.0
$Al_2O_3$	0.1	0.5
$P_2O_5$	0.2	1.0
$K_2O$	0.1	0.1
CaO	0.1	0.05
MnO	0.02	0.01
$Fe_2O_3$	0.02	0.01
CuO	0.02	0.01
ZnO	0.02	0.01
$As_2O_3$	0.02	0.01
$Rb_2O$	0.005	0.001
SrO	0.005	0.001
$ZrO_2$	0.005	0.001

Limits of detection achievable with pXRF for some heavy elements were substantially better than those achievable using the laboratory-based instruments employed in the first phase of this research project (Table 18). Even lower limits of detection would be possible with some laboratory-based techniques (eg ICPS), however, the sample would be destroyed during the course of analysis.

The precision for many heavy elements is better than those achievable using the laboratory-based instruments employed in the first phase of this research project (Table 19). This allows greater confidence in identifying batches (Freestone *et al* 2009).

Table 19. Comparison of precision

Oxide	SEM/XRF (lab)	pXRF
Na <sub>2</sub> O	0.1	NA
MgO	0.1	0.3
$Al_2O_3$	0.1	0.1
$P_2O_5$	0.2	0.1
$K_2O$	0.1	0.05
CaO	0.1	0.5
MnO	0.01	0.01
$Fe_2O_3$	0.01	0.01
CuO	0.01	0.01
ZnO	0.01	0.01
$As_2O_3$	0.02	0.005
$Rb_2O$	0.005	0.0002
SrO	0.005	0.0002
$ZrO_2$	0.005	0.0002

The pXRF instrument used was provided with a helium flush in order to enable the determination of light elements (especially magnesium and phosphorus) which were deemed significant for the identification of glass types (cf Dungworth 2011). The practical maintenance of a good quality helium flush proved to be challenge in the 'field'. On two occasions (on the Thursday) the protective film on the nose of the instrument was compromised leading to a loss of helium flush and a degradation of data quality for light elements (Figures 8 and 9). The quality of the helium flush had no significant effect on the determination of heavy elements (calcium and heavier elements).

The pXRF analysis of some of the plant ash glasses (and a few SLS glasses) provided unreliable estimates of light element composition, even where there were no grounds for suspecting a problem with the helium flush. It is likely that the weathering on the surface of some glass and any films of dirt will have affected the pXRF analysis. It is well known that glass undergoes chemical alteration at its surface especially when exposed to moisture (Dungworth *et al* 2011). The exposed surface of glass will generally lose a proportion of alkalis (and some other elements). The severity of such chemical weathering depends on the nature of the local environment (humidity, temperature, etc) and the inherent stability of the glass. Where pXRF analysis is carried out on the weathered surface of glass it is anticipated that the result will be compromised to a

certain degree. Depending on the analytical configuration (especially the voltage of the primary X-ray beam) the characteristic X-rays will be generated at a range of depths into the glass and this could include both the weathered surface and the underlying unaltered glass. The analytical result will in this case be a composite of both weathered and unweathered glass. The contribution made by the weathered and the unweathered glass will vary with the thickness of the weathered surface layer; in the most severe cases characteristic X-rays might only be detected from the weathered surface layer. The relative contribution to the analytical result made by the weathered surface and the underlying glass will also vary from element to element. Light elements only produce low-energy X-rays which are relatively easily absorbed, and so the characteristic X-rays for light elements that are detected, tend to come from close to the surface (Figure 39).

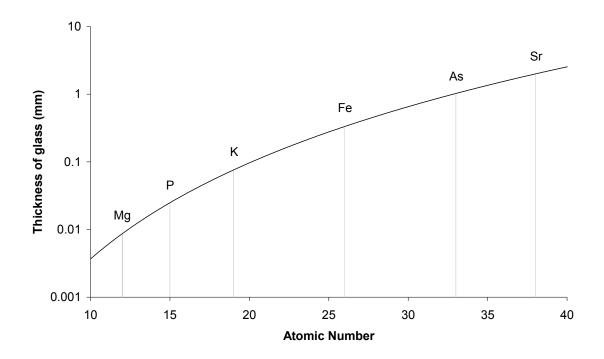


Figure 39. Relationship between atomic number and depth from which characteristic X-rays are detected (for K-series X-rays)

Surface layers make more of a contribution to the analytical result for light elements: for elements up to potassium it is largely the first 0.1 mm of glass which provides the characteristic X-rays (Figure 39). The thickness of weathered surface layers vary depending on the local environment and the intrinsic stability of the glass. Recent SLS glass has a high intrinsic chemical stability and weathered surfaces are generally very thin (<0.001 mm), except in the most severe environments. Earlier plant ash glasses tend to have low proportions of silica and so have low intrinsic stability leading to weathered surfaces up to 1 mm in thickness (depending on their local environment). Thus, it is the older and less stable glasses that are most susceptible to weathering and so more likely to yield a pXRF result which does not accurately reflect the true composition of the glass.

The classification of some SLS glass was initially hampered by the presence of relatively high levels of iron and other metals. The plain window glass analysed during the first phase of this project (Dungworth 2011) showed plant ash glasses with relatively high iron concentrations  $(0.5-1.7 \text{wt}\% \text{ Fe}_2\text{O}_3)$  while SLS glasses had much lower proportions (<0.4 wt% Fe<sub>2</sub>O<sub>3</sub>). The suspicion that the lghtham Mote SLS glasses with elevated iron contents were deliberately made this way is confirmed by the elevated concentrations of other metals which provide glass with tint or colour (especially copper and manganese). The manufacture of such glasses is discussed further below.

The use of pXRF allows the analysis of large numbers of windows which would not otherwise be available for examination. The *in situ* analysis of windows at Walmer Castle identified a type of glass (Dungworth and Girbal 2011) not identified during the first phase of historic window glass research (Dungworth 2011). This was a potassium calcium silicate glass, the closest parallel for which could be found in glass manufactured in Bohemia. Further detailed characterisation of this glass type is continuing through the laboratory-based analysis of similar glass from Kenwood House, London. The use of Bohemian window glass at Walmer Castle and Kenwood House would appear to be an example of extremely wealthy clients obtaining prestigious and expensive glass from an obscure source. Such glass would not have been routinely used and so was not identified during the first phase of laboratory-based analysis (which was largely based on samples from fairly modest buildings and archaeological contexts). It is possible that the analysis of the lghtham Mote windows has identified another, 'new' type of glass (HiK). This has generally been grouped with the SLS glass but displays some unusual chemical characteristics, such as relatively high potassium. This glass is discussed in more detail below.

# Glass types from Ightham Mote

The *in situ* pXRF analysis of window glass from Ightham Mote has allowed the identification a number of major compositional types. Most of these are well known from previous research. The different types were initially isolated using a variety of elements (Figures 40 and 41), especially those identified during the first phase of the project as most significant (phosphorus, magnesium, potassium, calcium and strontium). The problems encountered using pXRF to obtained light element concentration data led to increasing reliance on heavy elements such as rubidium (Figures 42 and 43).

The pXRF analysis has shown that,

```
10% are forest glass, manufactured before c1567, 34% are HLLA glass (c1567–c1700), 3% are kelp glass (c1700–c1835), 3% are HiK glass of likely late 18th- or early 19th-century manufacture, and 50% of the analysed panes are SLS glass, manufactured after c1835 (Figure 44).
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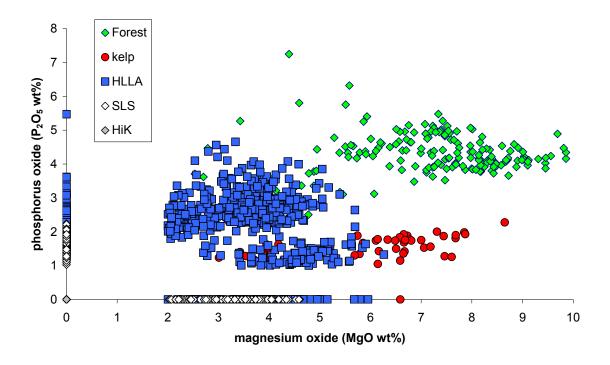


Figure 40. Magnesium and phosphorus content of all analysed Ightham Mote glass (includes HLLA samples where magnesium and/or phosphorus was not detected [due to corrosion] and SLS samples with spurious phosphorus results due to loss of helium flush, cf Figure 9)

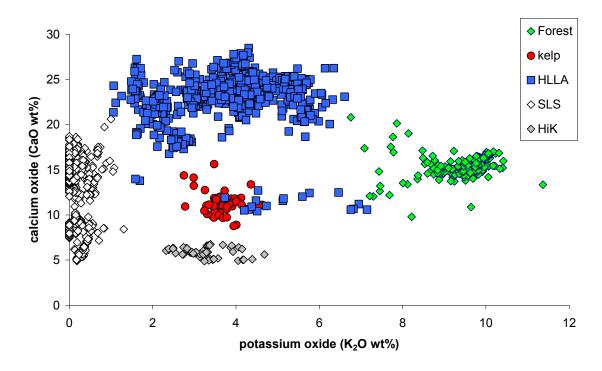


Figure 41. Potassium and calcium content of all analysed Ightham Mote glass

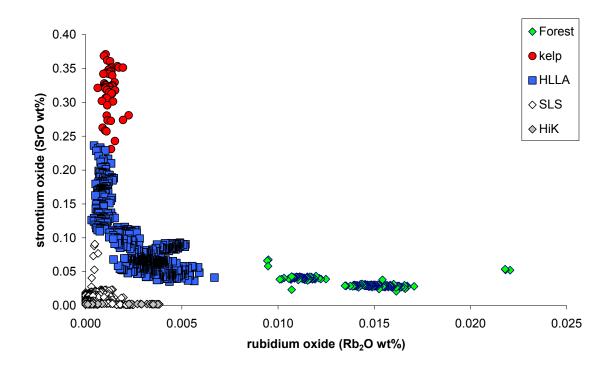


Figure 42. Rubidium and strontium content of all analysed Ightham Mote glass

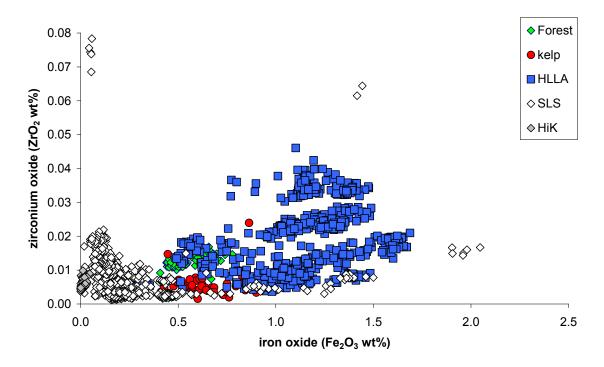


Figure 43. Iron and zirconium content of all analysed Ightham Mote glass

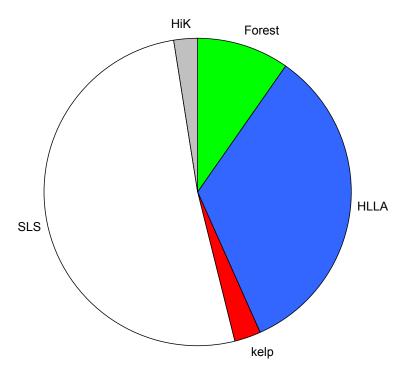


Figure 44. Proportions of different glass types at Ightham Mote

#### Forest Glass

A total of 188 panes have been identified as having been made from forest glass. In every case the concentrations of phosphorus and strontium indicated that glass had been made using the ash of a terrestrial plant. It is currently believed that the principle plant ash used was bracken or fern (Dungworth and Paynter 2010; Jackson *et al* 2005). In a minority of cases, however, the levels of calcium and/or potassium did not provide a reliable basis for distinguishing between forest glass and HLLA. The problem with these samples was clearly the presence and nature of weathered surfaces — the analysis of many of these samples showed the presence of high levels of sulphur that can be linked to corrosion of the glass (cf Dungworth *et al* 2011). Overall the forest glass shares the same overall composition as northern medieval forest glass (Table 20).

Table 20. Average major and minor element concentrations in all the Ightham Mote forest glass (and compared with some contemporary glass)

	MgO	Al <sub>2</sub> O <sub>3</sub>	P <sub>2</sub> O <sub>5</sub>	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>
Ightham Mote	6.9	2.4	4.2	9.4	15.3	0.9	0.5
Blunden's Wood	6.8	1.0	3.0	11.0	13.7	1.1	0.7
Idehurst	8.1	1.3	3.7	11.1	16.7	1.0	0.6
Knightons	5.9	2.5	3.0	10.0	16.7	0.9	0.8
Little Birches	7.8	1.2	3.4	12.5	13.4	1.5	0.5

Some of the minor and trace elements present in the forest glass indicate the presence of two compositional sub-groups (Figure 45, Table 21). These are designated Forest1 and Forest2. The compositional differences are undoubtedly small, however, they are significant given the analytical precision of the pXRF.

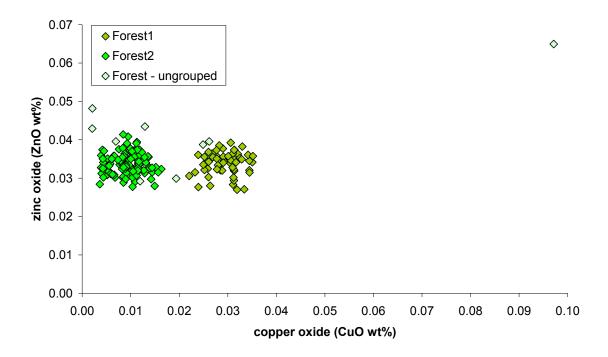


Figure 45. Copper and zinc content of the forest glass from Ightham Mote

The Forest I glass is found in the Great Hall (80), the New Chapel (31) and the Tower (11), while Forest 2 is mostly found in the Great Hall (52) and only five Forest I panes were found in the New Chapel (and none in the Tower).

Table 21. Average minor and trace elements in the two compositional sub-groups of forest glass

	No.	$Fe_2O_3$	CuO	Rb₂O	SrO	ZrO <sub>2</sub>
-	57	0.64±0.04	0.029±0.003	0.0113±0.0005	0.040±0.001	0.0142±0.0007
2	122	0.48±0.05	0.009±0.003	$0.0151\pm0.0008$	0.029±0.002	0.0119±0.0007

The significance of relatively distinct compositional sub-groups of glass (such as Forest I and Forest2) has recently been explored by Freestone and colleagues (Freestone *et al* 2009). The nature of pre-industrial glass making is likely to have ensured that each batch of glass manufactured would, even if made to the same basic recipe, have a subtly different chemical composition. Such chemical variation could arise through a variety of factors, the most important of which are likely to be slight variations in the nature of the raw materials used, the proportions of these raw materials, and differences in melting temperature. The identification of such subtle compositional differences and the attribution of these differences to different batches of glass manufacture is a relatively

straight-forward procedure if the analytical technique employed is capable of a high degree of precision. The identification of the significance of such batches is, however, somewhat more challenging. It is possible to imagine a single glasshouse which could produce two different batches on successive days and that these could then be identified through chemical analysis of the finished glass. Nevertheless, it is also possible to imagine that the batches were made at completely different glasshouses (perhaps separated by hundreds of kilometres) and at different times (perhaps even centuries apart). If the two lghtham Mote forest glass batches were the product of the first of these two scenarios, then it is likely that they were both ordered, manufactured, delivered and installed together. If, on the other hand, they represent the latter scenario then they probably result from two separate glazing episodes. Although both batches are found together in W02 in the Great Hall, it is likely that this window has undergone significant repair at later dates and could have used glass employed in earlier windows — the coexistence of both types in this window is not proof that they were originally supplied together.

The two batches share the same concentrations of major elements and are clearly made to the same basic recipe. The relatively high magnesium and low potassium content suggests that this glass was manufactured in England and not on mainland Europe (Dungworth and Paynter 2010). The differences in trace element concentrations (especially Rb, Sr and Zr) are sufficient to suggest that the two batches were probably not made at the same glasshouse. The difference in copper content is of uncertain significance; the proportion of copper in either batch is unlikely to have been deliberate or to have had an appreciable effect on the quality of the finished glass. It is unclear whether the copper originated as a trace element in a plant ash or derives from the use of cullet glass that could have included (stained) glass deliberately coloured with copper.

The forest glass would have been manufactured before c1567 and could have been installed at almost any earlier date. Some or all of the forest glass may have originally been installed into windows in the earliest 14th-century buildings; it could also represent repair, replacement and remodelling that took place when Sir Richard Clement owned Ightham Mote in the early 16th century. The forest glass would not have formed part of the original glazing of any windows installed by the Selby's or any later owners.

#### High-Lime Low-Alkali Glass

A total of 65 I panes have been identified as having been made of HLLA glass. The identification of this glass type was frequently hampered by the failure to detect magnesium (107 panes) or phosphorus (61 panes). In some cases the apparent proportion of calcium was much lower than would be normal for this glass type. The identification of HLLA glass, therefore, relied heavily on the use of the trace elements rubidium and strontium: HLLA contains less rubidium than forest glass and less strontium than kelp glass, but significantly more of both of these elements than SLS glass (Figure 42). The HLLA glass panes can be divided into HLLA1 (low manganese) and HLLA2 (higher manganese). These two groups have tentatively been identified as of chronological

significance (HLLA2 being made c1567–c1610 and HLLA1 c1610–c1700). The significance of this separations into two compositional sub-groups is strengthened by other minor differences, including iron and zirconium (Figure 46).

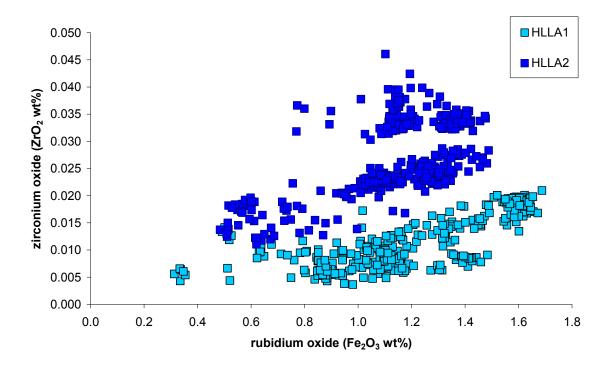


Figure 46. Iron and zirconium content of the HLLA glass from Ightham Mote

The distribution of HLLA1 and HLLA2 also suggests that the separation of these subgroups is meaningful. Some of windows that contained HLLA glass only had HLLA1 (or only HLLA2, eg Figures 24 and 25) while, in some of those windows with both types, the spatial arrangement of the panes suggests that the two types of glass were made at different times and/or places (eg Figures 18 and 21). Nevertheless, both HLLA sub-groups can be found throughout many of the Ightham Mote windows. In some cases the present arrangement of HLLA panes is likely to be the result of restoration and repair programmes that could have taken place long after HLLA glass ceased to be made.

If it is assumed that all of the HLLA glass was originally installed at Ightham Mote, then it can be concluded that it would have been installed during the period when the site was owned by the Selby family. It is most unlikely that any of this glass was originally manufactured after c1700.

The concentrations of minor and trace elements in both HLLA sub-groups suggests the presence of several batches (and numerous outliers), however, the systematic identification of these groups was hampered by the limited range of elements which displayed differences in concentrations and the apparent high degree of overlap.

## Kelp Glass

A total of 56 panes have been identified as having been made of kelp glass. The identification of this glass type was occasionally hampered by the failure to detect magnesium (I pane) or phosphorus (5 panes). The kelp glass was, however, almost always identifiable by the relatively high strontium content. Kelp glass dominated the market for plain window glass throughout the I8th century (and the first three decades of the I9th century) and yet only 3% of the analysed panes at Ightham Mote are of this glass type. This suggests that very little work was undertaken to replace or repair any windows at Ightham Mote during this period. The notable exceptions to this are the Gothic revival windows which face onto the courtyard (W03 and W07).

#### **SLS Glass**

Over half of all of the analysed panes at Ightham Mote are made of SLS glass. In many instances, the identification of this glass type was straight forward: it rarely contained any detectable phosphorus and often contained very low levels of iron oxide. In some cases the initial identification was hampered by the detection of phosphorus and of rather high levels of iron. The presence of phosphorus would normally have indicated that the panes were made using a plant ash as the flux and have indicated manufacture prior to c1835. A consideration of the phosphorus content of these panes in relation to the date and time they were analysed, however, clearly showed that these anomalous results all took place during two short periods on the Thursday (Figure 9). The cause of the anomalous results has been attributed to issues with maintaining a protective film on the nose of the instrument and the inevitable loss of helium flush. The problems with the helium flush led to problems detecting and quantifying a range of light elements during these two periods on Thursday (Figure 8). Once this instrumental problem was diagnosed as the cause of the anomalous light element results it was possible to discount the light elements and focus on the data from heavier elements.

The heavy elements present in the SLS glass usually allowed the unambiguous identification of this glass type, however, some confusion was initially caused by the, at times, rather high iron content (Figure 47). These high-iron SLS panes also often contained elevated levels of other colouring elements such as manganese and copper (Figure 48). These panes have been interpreted as having been made using SLS glass (after c1835) but with the deliberate addition of a range of colouring metals in an effort to match the quality of older glass at Ightham Mote.

The SLS glass (including the deliberately tinted or coloured panes) can all be attributed to the period after c1835. The calcium content of the SLS glass (Figure 49) suggests the presence of a high-calcium group (768 panes) likely to have been manufactured c1835—c1930 (Phase 5a) and a low-calcium group (228 panes) likely to have been manufactured after c1930 (Phase 5b). Magnesium was (with one exception) not detected in any of the high-calcium SLS glass (cf Table 1). Magnesium was detected in some of the low-calcium

SLS glass, however, the failure to detect this element in some low-calcium SLS glass is likely to be due to problems with the helium flush and/or surface weathering of the glass.

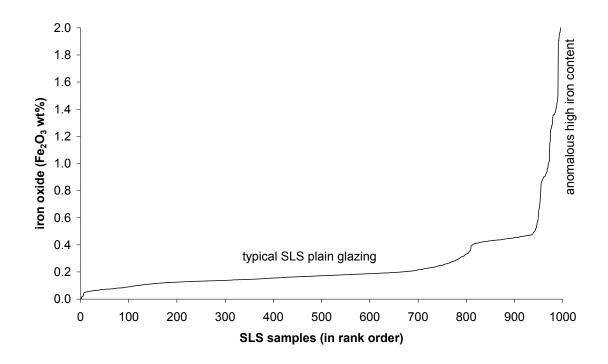


Figure 47. Iron content of SLS glass (in rank order)

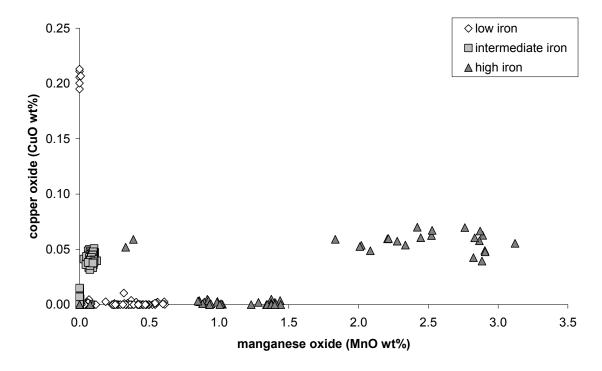


Figure 48. Manganese and copper content of SLS glass

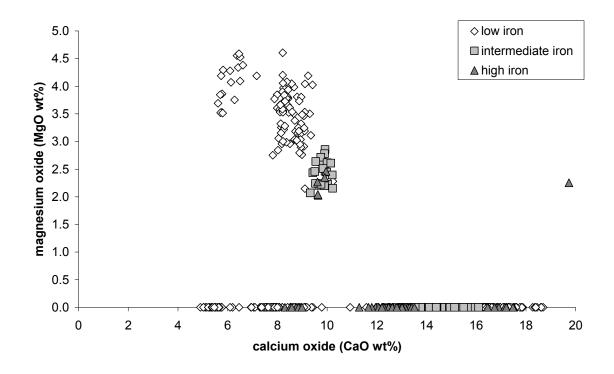


Figure 49. Magnesium and calcium content of SLS glass

## SLS (HiK) Glass

A total of 51 panes have been identified as having been made of a glass not previously encountered (Table 22). The concentrations of most elements in this glass (eg rubidium and strontium) are similar to most SLS glass, however, the glass contains much more potassium (3.3wt%  $K_2O$ ) than would be expected on the basis of all work to date on historic window glass (for the purposes of this report it is referred to as HiK). The pXRF analysis of windows at Walmer Castle (Dungworth and Girbal 2011) identified a potassium calcium silicate glass which had also escaped previous detection. The Walmer Castle glass contained very high levels of potassium (5–20wt%  $K_2O$ ) that left little doubt that it was based on the recipe used for Bohemian crystal and known to have been employed in Germany and Bohemia for the manufacture of window glass in the early 19th century (Smrcek 2005). The lghtham Mote HiK glass has a chemical composition which is quite similar to the Walmer Castle Potash3 glass, however, there are sufficient minor differences (eg the lghtham Mote glass has less than a tenth of the rubidium content) to suggest that these are not identical glasses.

Table 22. Average composition of HiK glass

	MgO	$Al_2O_3$	$P_2O_5$	K₂O	CaO	MnO	Fe <sub>2</sub> O <sub>3</sub>	CuO	$As_2O_3$	Rb₂O	SrO	ZrO <sub>2</sub>
Ightham	<2	<0.5	<	3.3	5.8	< 0.0	0.01	0.05	0.09	0.002	0.002	0.006
Walmer	<2	0.9	<	6.1	5.6	< 0.0	0.15	< 0.0	< 0.0	0.022	0.006	0.006

There are a range of minor elements present in the Ightham Mote HiK glass (eg Figure 50) which suggest that this glass was on occasion produced with a deliberate colour or tint. Most of the HiK glass was found in the Tower (28 panes) and New Chapel (19 panes).

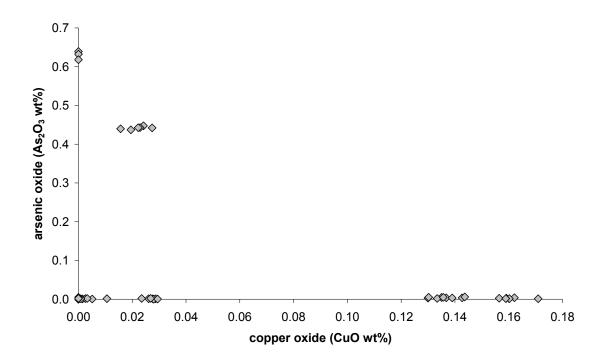


Figure 50. Copper and arsenic content of the HiK glass from Ightham Mote

The low iron, rubidium and strontium content of this glass is typical of SLS and flint glasses and it is unlikely to have been manufactured before the late 17th century. The parallels with Walmer Castle and Kenwood House suggest that the most likely period of manufacture is the late 18th century or early 19th century.

## Reproducing colour/tint in historic window glass

The SLS glass from Ightham Mote includes panes with elevated levels of iron (Figure 47), even though plain SLS window glass of the 19th and 20th centuries normally contains rather low levels of iron (<0.4wt% Fe<sub>2</sub>O<sub>3</sub>). Iron is the most significant impurity in glassmaking materials that can give a colour or tint to the finished glass. The low levels of iron in plain SLS glazing is undoubtedly the result of the deliberate selection of low-iron sand that would yield a glass largely free from any tint. This contrasts with most earlier glass which contains higher levels of iron and therefore usually has a discernible colour.

The high-iron SLS glass from Ightham Mote falls into two groups, the first (132 panes) with 0.4-0.5wt% Fe<sub>2</sub>O<sub>3</sub> and the second (54 panes) with 0.5-2.0wt% Fe<sub>2</sub>O<sub>3</sub>. Many of these panes also contain small but appreciable levels of manganese and copper (Figure 48). The

presence of these elements is most likely to be the result of deliberate policy by the glassmakers to produce glass with a specific colour or tint. Varying levels of manganese, iron and copper could and would provide the glass with a variety of tints from pale blue to pale green. This deliberately tinted glass may have been made to a carefully laid out recipe, however, the concentration of colouring elements in the Ightham Mote glass are generally much lower than would be suggested by a consideration of most 19th-century recipes (eg Cable 2008). Bontemps, however, recommends the production of,

antique white glass, which the English call cathedral glass. It will be understood that a glass manufacturer who makes large quantities of coloured glasses does not need to colour white glass by adding metal oxides, he needs only to add a small proportions of coloured cullet to larger proportions of his white window cullet to make antique glasses. For this purpose he will use mostly green and blue cullet, also amber coloured with iron and manganese, and ruby. (Cable 2008, 284)

## **CONCLUSIONS**

The pXRF analysis of 1939 panes of window glass at Ightham Mote were undertaken to test the suitability of the methodology and to shed some light on the history of glazing at the site.

The pXRF was used with a helium flush to enable the detection of light elements that were diagnosed as significant in identifying different periods of manufacture (Dungworth 2011). The limitations of the physical conditions of surviving historic glass (in particular weathered surfaces) and the difficulties in maintaining a helium flush while completing such a large number of analyses have shown that the detection of light elements is never certain. In some cases the presence of light elements may be missed, or their concentrations may be misreported, due to problems with corrosion or the instrument itself. The inherent analytical problems do not, however, seem to have had any significant effect on the determination of heavier elements (iron, etc). The heavy elements which have proved most useful for the identification of basic glass types have been rubidium and strontium. Strontium was already identified as a key element for identifying kelp glass but it is now clear that, used in combination with rubidium, it can help identify all of the other major glass types.

The pXRF identified examples of every major type of window glass (forest, HLLA, kelp and SLS) at Ightham Mote. A tenth of the glass is forest glass which would have been produced before c1567 and could have formed part of the original 14th-century glazing or of the early 16th-century glazing under Sir Richard Clement. Most of this forest glass survives as occasional panes within windows that also include a greater proportion of much later glass. In some cases it is possible that the forest glass which is present in these

windows has had a long history of use, possibly in more than one window, building or even site. It is clear that many of the older windows have undergone several periods of repair and restoration but that these are poorly documented. Untangling the original glass from later replacements and defining more than one period of repair based solely on the composition of the glass is far from straight forward, 'The absence of uniformity throughout gives a peculiar charm to the building' (Vallance 1933, 118).

A third of the analysed panes are made from HLLA glass that would have been manufactured between c1567 and c1700. In at least some cases, it is suspected that the current arrangement of the HLLA glass significantly post-dates its manufacture. It is possible that at least some of the HLLA glass was obsolete when it was introduced. It may have been reclaimed from different windows, buildings, or even sites but retained for use where *antique* glass was valued.

A very small proportion of the glazing can be dated to c1700–c1830 (the kelp glass, 3%). Just over half of the glass has a SLS composition that shows it was manufactured after c1835. Most of this SLS glass has a composition which indicates production prior to the mechanisation of the flat glass industry c1930. A proportion of the SLS glass appears to have been deliberately manufactured with a tint in order to match the older, surviving glass.

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# APPENDIX I. IGHTHAM MOTE FLOOR PLANS SHOWING THE LOCATIONS OF ALL ANALYSED WINDOWS

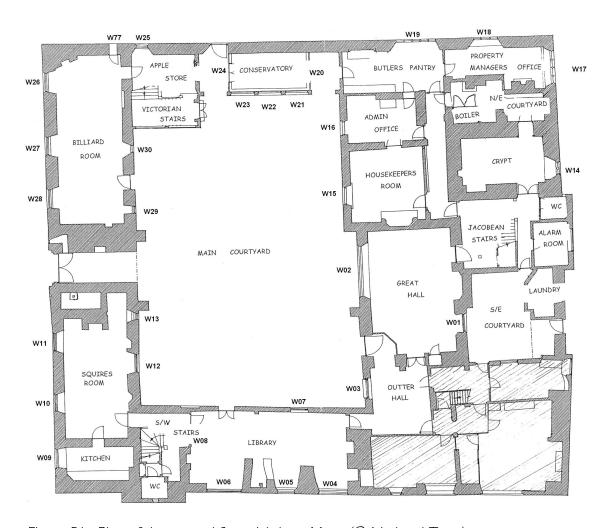


Figure 51. Plan of the ground floor, Ightham Mote (© National Trust)

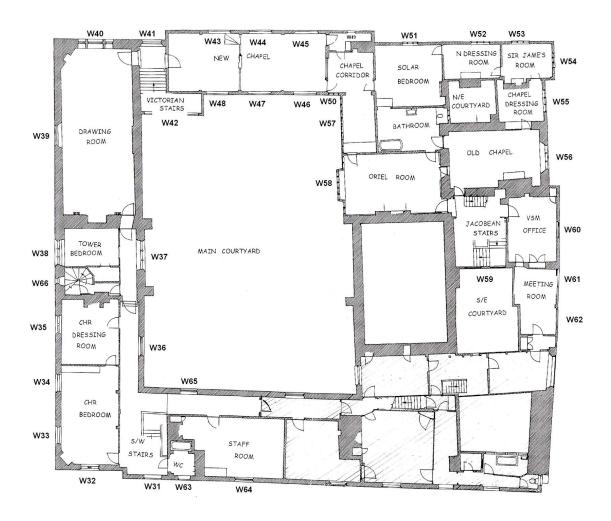


Figure 52. Plan of the first floor, Ightham Mote (© National Trust)

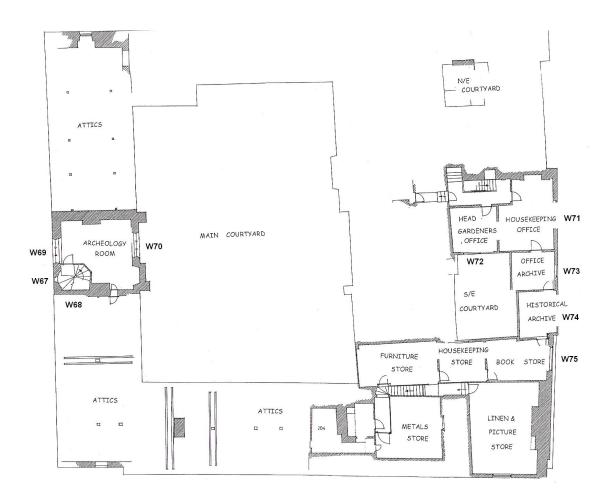


Figure 53. Plan of the second floor, Ightham Mote (© National Trust)

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APPENDIX 2. pXRF RESULTS (W = WINDOW; P = PANE; nd = NOT DETECTED)

A <sub>2</sub> O <sub>3</sub> SiO <sub>2</sub> P <sub>2</sub>	SiO <sub>2</sub> P <sub>2</sub>	۵,	S	اع	ō	K <sub>2</sub> O	CaO	MnO	$Fe_2O_3$	CnO	ZnO	$As_2O_3$	$Rb_2O$	S	$ZrO_2$
0.6 92.7 nd 1.0 nd	92.7 nd 1.0 nd	bu 0.1 bu	pu			Ō	15.1	pu	0.204	0.004	pu	0.346	pu	0.015	0.004
0.6 92.0 nd 0.9 nd	92.0 nd 0.9 nd	pu 6:0 pu	pu			Ъ	15.3	pu	0.190	pu	pu	0.342	pu	910.0	0.004
l.9 90.8 nd 0.6 nd	90.8 nd 0.6 nd	nd 0.6 nd	pu		0	7	12.4	2.871	0.766	0.067	0.01	0.548	pu	0.017	0.003
nd 9.0 bn 96.8	bu 9.0 bu 8.96	pu 9.0 pu	pu		ŭ	$\overline{}$	13.6	0.092	0.174	pu	pu	0.222	pu	0.015	0.005
4.6 87.0 1.1 1.7 0.5	87.0 1.1 1.7 0.5	1.1 1.7 0.5	0.5		2.5		18.4	0.029	1.426	pu	900.0	0.020	0.00	0.160	0.008
bu 6.0 bu	90.4 nd 0.9 nd	bu 6.0 bu	pu		o.	_	13.2	2.905	0.522	0.049	0.012	0.019	pu	0.017	0.003
l.5 91.5 nd 0.9 nd	91.5 nd 0.9 nd	bu 6.0 bu	pu		0	_	13.3	2.907	0.569	0.048	0.01	0.021	pu	0.017	0.003
1.4 89.3 nd 0.9 nd	bu 6.0 bu £.68	pu 6.0 pu	pu		0		13.0	2.884	0.564	0.039	0.030	0.023	pu	910.0	0.003
4.1 77.2 2.6 0.7 nd	77.2 2.6 0.7 nd	2.6 0.7 nd	pu		4.		26.8	0.629	1.182	0.012	0.021	0.109	0.003	0.065	0.033
I.2 89.3 nd 0.8 nd	89.3 nd 0.8 nd	pu 8.0 pu	pu		0.		12.8	2.823	0.507	0.043	0.029	0.019	pu	910.0	0.004
nd 95.5 nd 0.6 nd	95.5 nd 0.6 nd	pu 9.0 pu	pu		pu		1.91	pu	0.132	pu	pu	0.087	pu	0.009	900'0
3.6 69.8 4.1 9.7 0.6	69.8 4.1 9.7 0.6	4.1 9.7 0.6	9.0		3.3		23.2	0.844	1.321	900.0	0.026	0.177	0.004	0.078	0.028
0.6 87.4 nd 2.7 nd	87.4 nd 2.7 nd	nd 2.7 nd	pu		pu		15.9	0.061	0.197	pu	pu	0.204	pu	0.015	900.0
I.8 86.5 nd 0.6 nd	9.5 nd 0.6 nd	nd 0.6 nd	pu		0.		<u>8</u> .	2.866	0.684	0.058	0.014	0.539	pu	910.0	0.003
4.6 81.0 2.7 1.2	81.0 2.7 1.2 nd	2.7 I.2 nd	pu		3.9		26.2	0.622	1.258	0.012	0.021	0.125	0.004	0.061	0.036
4.3 77.7 2.5 0.9 nd	77.7 2.5 0.9 nd	2.5 0.9 nd	pu		4.2		27.3	0.586	1.144	0.015	0.026	0.112	0.004	0.065	0.035
3.2 87.7 1.1 0.8 0.4	87.7 1.1 0.8 0.4	1.1 0.8 0.4	4.0		2.4		22.6	0.029	1.112	pu	0.008	0.005	0.00	0.183	0.007
2.7 85.0 nd 1.0 0.4	85.0 nd I.0 0.4	nd I.0 0.4	4.0		1.7		24.3	0.011	0.874	0.004	0.004	pu	0.00	0.119	0.007
2.7 74.6 2.7 5.0 0.7	74.6 2.7 5.0 0.7	2.7 5.0 0.7	0.7		2.6		25.8	0.154	1.017	0.00	0.013	0.04	0.00	0.122	0.017
0.7 92.4 nd 0.6 nd	92.4 nd 0.6 nd	pu 9.0 pu	pu		DU	_	12.4	0.077	0.230	pu	0.003	0.196	pu	0.013	0.005
l.5 88.6 nd 0.8 nd	bu 8.0 bu 9.88	pu 8.0 pu	pu		0.		13.5	1.833	1.007	0.059	0.019	0.018	pu	0.017	0.004
4.2 77.5 2.6 0.7 nd	77.5 2.6 0.7 nd	2.6 0.7 nd	pu		4.2		26.7	0.541	1.167	0.013	0.023	0.110	0.003	0.062	0.034
5.1 88.4 nd 0.5 0.4	88.4 nd 0.5 0.4	nd 0.5 0.4	4.0		2.4		18.3	0.020	1.40	pu	0.004	0.005	0.00	0.159	0.008
4.7 79.6 2.8 I.I nd	79.6 2.8 I.1 nd	2.8 I.I nd	pu		4.3		27.4	0.622	1.296	0.009	0.029	0.102	0.004	0.064	0.037
nd 97.5 nd 0.6 nd	97.5 nd 0.6 nd	pu 9.0 pu	pu		pu		13.6	0.062	0.193	pu	pu	0.215	pu	0.015	0.005
2.1 89.8 nd 0.8 nd	bu 8.68 pu	nd 0.8 nd	pu		0		13.0	2.084	0.864	0.049	0.012	0.020	pu	910.0	0.005
3.9 83.5 2.7 1.2 0.4	83.5 2.7 1.2 0.4	2.7 1.2 0.4	4.0		4.3		22.3	0.102	1.460	0.008	0.018	pu	0.003	0.082	0.014
2.4 91.1 nd 0.8 nd	91.1 nd 0.8 nd	pu 0.8 pu	pu		0.		13.1	2.019	0.88	0.054	0.0	0.020	pu	910.0	0.005
4.5 79.6 2.6 0.6 nd	79.6 2.6 0.6 nd	2.6 0.6 nd	pu		4.		28.0	0.585	1.156	0.012	0.023	0.113	0.003	0.064	0.035
2.9 85.8 1.2 1.1 0.5	85.8 1.2 1.1 0.5	1.2 1.1 0.5	0.5		7.0		23.3	0.018	0.879	pu	0.003	0.010	0.00	0.193	0.005

$ZrO_2$	0.003	0.034	0.003	0.005	0.004	0.004	0.003	0.010	0.004	0.015	0.028	0.004	0.004	0.018	0.012	0.004	0.007	9000	0.005	0.017	900.0	0.003	0.005	0.004	0.004	0.005	9000	0.005	9000	0.005	0.015	0.028
SrO	0.012	0.064	0.016	0.014	0.015	910.0	910.0	0.128	0.015	0.098	0.083	0.014	0.017	0.058	0.110	0.015	0.166	0.125	0.008	0.087	0.171	910.0	0.015	910.0	0.179	0.014	0.197	910.0	0.151	0.014	0.043	0.079
$Rb_2O$	pu	0.004	pu	pu	pu	pu	pu	0.00	pu	0.002	0.003	pu	pu	0.003	0.00	pu	0.00	0.00	0.00	0.002	0.00	pu	pu	pu	0.00	pu	0.00	pu	0.00	pu	0.004	0.003
$As_2O_3$	0.037	0.112	0.559	0.209	0.207	0.386	0.539	0.007	0.228	pu	0.123	0.225	0.015	0.041	910.0	0.013	0.011	pu	pu	900'0	0.077	0.295	0.261	0.023	0.009	0.222	pu	0.013	pu	0.214	0.015	0.139
ZnO	pu	0.022	0.020	0.00	0.003	pu	0.013	0.042	0.002	0.014	0.032	pu	0.027	0.027	900.0	0.014	0.008	0.009	pu	0.024	0.005	0.019	0.002	0.011	0.008	0.00	0.004	0.014	0.007	0.002	0.024	0.027
CnO	pu	0.012	0.063	0.00	pu	pu	090.0	0.00	0.00	0.007	9000	pu	0.070	0.007	pu	0.059	pu	0.003	pu	0.007	pu	0.055	pu	0.070	pu	pu	pu	090.0	pu	pu	900'0	0.009
$Fe_2O_3$	0.205	911.1	0.665	0.193	0.187	0.203	0.722	0.851	0.170	1.544	1.402	0.191	1.014	0.723	010.1	0.848	0.880	1.272	0.287	1.631	0.886	0.594	0.236	0.963	0.884	0.206	1.136	0.902	0.858	0.186	1.375	1.355
MnO	pu	0.564	2.890	0.065	0.099	pu	2.832	0.005	0.053	0.165	0.870	0.072	2.762	0.675	0.054	2.207	0.045	0.003	pu	0.139	0.026	3.122	0.415	2.421	0.017	0.071	910.0	2.446	0.032	0.075	0.138	0.800
CaO	15.3	27.6	6:11	13.5	13.4	15.0	12.3	22.7	14.0	21.9	25.2	13.2	12.8	20.5	22.9	12.9	22.0	23.2	15.0	23.8	21.1	12.6	14.3	13.4	21.7	13.9	21.1	13.0	24.7	13.4	23.3	23.3
$K_2O$	pu	4.	0.2	pu	pu	pu	0.2	<u>8</u> .	pu	2.9	3.5	pu	0.2	4.2	9.1	0.0	2.0	2.3	9.0	4.22	<u>~</u>	0.2	pu	0.0	L.7	pu	2.6	0.0	9.1	pu	5.1	3.4
D	pu	pu	pu	0.2	pu	pu	pu	4.0	pu	0.5	0.5	pu	pu	0.5	4.0	pu	0.5	0.3	0.2	4.0	9.0	pu	pu	pu	0.5	pu	0.5	pu	4.0	pu	pu	0.5
SO3	0.8	6.0	0.7	9.0	0.7	0.8	9.0	0.8	0.7	6.0	6.0	0.7	0.8	0.3	3.6	6.0		1.5	0.	0:	<u>~</u> .	0.	0.7	0.8	0.8	9.0	6.0	0.8	=	9.0	3.9	3.4
$P_2O_5$	pu	2.4	pu	pu	pu	pu	pu	pu	pu	2.2	2.3	pu	pu	2.6	1.2	pu	pu	1.2	pu	2.7	2.5	pu	pu	pu	0.	pu	4.	pu	pu	pu	3.	2.2
$SiO_2$	6.96	77.0	1.88	92.7	93.7	0.16	89.2	83.3	1.66	83.6	80.4	86.3	87.9	4.18	85.6	89.7	86.7	84.6	94.7	83.2	78.1	6.06	93.5	61.7	85.0	1.86	88.3	1.06	84.2	95.5	77.7	83.1
$Al_2O_3$	0.7	3.8	6:1	0.5	9.0	9.0	2.1	3.6	9.0	2.9	4.0	pu	2.2	5.7	4.3	6.	3.0	3.3	2.9	4.6	2.6	<u>~</u>	9.0	2.1	2.8	pu	3.3	2.1	2.5	pu	3.7	4.5
MgO	pu	4.2	pu	pu	pu	pu	pu	3.3	pu	3.7	3.6	pu	pu	4.3	pu	pu	4.	4.8	pu	4.2	3.7	pu	pu	pu	4.8	pu	5.3	pu	4.5	pu	2.8	3.0
Ь	13	4	15	17	8	61	20	_	2	$\sim$	4	2	9	_	$\infty$	6	0	=	12	13	4	14.3	15	_	2	$\sim$	4	2	9	7	<sub>∞</sub>	6
>	w01.2	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	w01.3	4.10w	4.10w	4.10w	4.10w	4.10w	4.10w	4.10w	4.10w	4.10w						

$ZrO_2$	0.005	0.009	0.009	0.007	0.028	0.007	0.014	0.014	0.034	0.037	0.034	0.035	0.005	0.033	0.004	0.023	0.035	0.011	0.004	0.005	0.024	0.032	0.012	0.011	0.033	0.010	0.025	0.033	0.014	0.032	0.032	0.014
S.	910.0	0.091	0.171	0.171	0.078	0.176	0.115	0.087	0.063	0.063	0.084	0.085	0.009	0.082	0.146	0.089	0.084	0.028	0.011	0.009	0.089	0.083	0.029	0.027	0.065	0.091	0.091	0.084	0.042	980.0	0.084	0.099
$Rb_2O$	pu	0.002	0.00	0.00	0.003	0.00	0.002	0.002	0.004	0.004	0.004	0.004	0.00	0.004	0.00	0.005	0.004	0.015	0.00	0.00	0.004	0.004	910.0	910.0	0.003	0.002	0.004	0.004	0.01	0.004	0.004	0.002
As <sub>2</sub> O <sub>3</sub>	0.021	pu	pu	0.008	0.	pu	pu	0.035	0.11	0.	0.140	0.128	pu	0.177	pu	0.105	0.149	910.0	pu	pu	0.122	0.135	0.045	0.051	0.121	pu	0.112	0.133	0.008	0.144	0.122	0.033
ZnO	0.014	900'0	0.007	0.009	0.030	0.008	0.019	0.014	0.022	0.020	0.030	0.026	0.005	0.028	0.005	0.027	0.032	0.032	0.002	0.00	0.029	0.027	0.035	0.036	0.026	0.003	0.028	0.028	0.032	0.027	0.026	0.018
Ono	0.054	pu	0.00	pu	0.012	pu	900'0	900'0	0.014	0.010	0.009	0.011	pu	0.011	pu	0.014	0.008	0.008	pu	pu	0.009	0.010	0.004	0.007	0.013	pu	0.013	0.014	0.025	0.010	0.020	0.001
$Fe_2O_3$	0.902	0.712	1.357	1.297	1.388	4. —	1.349	1.014	1.228	1.159	1.422	1.408	0.168	1.325	0.981	1.008	1.312	0.473	0.178	0.153	1.093	1.316	0.449	0.443	1.146	0.630	1.046	1.3	0.593	1.351	1.429	1.298
MnO	2.335	pu	0.058	0.024	0.805	0.029	0.194	0.195	0.622	0.555	0.895	0.880	pu	0.947	0.010	0.722	0.873	0.915	pu	pu	0.695	0.928	0.867	0.867	0.575	pu	0.785	0.947	0.834	0.915	0.899	0.195
CaO	13.1	0.	21.3	21.8	24.7	21.5	23.7	25.9	26.6	26.7	23.3	23.7	14.0	22.4	27.2	24.0	22.1	14. 4.		14.3	23.8	22.6	14.2	13.7	26.4	9.1	24.4	23.0	16.4	23.1	23.8	26.0
K <sub>2</sub> O	1.0	4.7	2.1	2.1	3.4	2.0	2.8	2.8	4.2	4.2	4.3	4.4	4.0	4.3	9.1	5.4	4.	9.6	9.0	9.0	5.4	4.3	9.5	9.2	4.0	4.5	5.4	4.3	8.6	4.4	4.4	2.5
ō	pu	9.0	9.0	9.0	0.5	0.5	4.0	9.0	pu	pu	pu	pu	pu	0.2	0.5	pu	pu	4.0	pu	pu	0.2	pu	6.0	0.5	pu	9.0	0.2	pu	4.0	pu	pu	9.0
SO	0.8	0.3	4.0	9.0	pu	9:1	0.	5.7	0.5	9.0			0.8	5.1	1.2	<u></u>	3.9	2.4	9.0	0.5	3.0	2.6		8.9	4.	4.0	2.4	9.1	9.0	3.0	0.8	5.4
$P_2O_5$	pu	pu	pu	0:	2.4	1.2	2.3	2.8	2.4	2.5	2.4	2.2	pu	3.0	pu	2.5	2.7	3.9	pu	pu	2.7	2.4	4.3	4.3	2.4	pu	2.9	2.4	5.0	2.4	2.2	2.9
SiO <sub>2</sub>	90.5	9.16	82.4	85.4	81.2	85.5	81.3	75.7	78.5	78.9	80.8	1.08	92.7	75.4	89.5	79.1	72.6	1.89	93.7	92.5	74.2	76.4	72.0	1.99	71.9	91.4	78.7	79.8	72.1	78.3	79.2	76.8
$Al_2O_3$	6.1	<u>~</u>	3.4	3.4	4.	3.8	3.	2.7	4.3	4.2	4.4	4.2	1.7	4.3	3.0	2.9	3.5	1.7	9.	9.	2.8	3.9	2.0	2.1	3.5	1.7	3.3	4.5	2.4	4.3	4.2	3.2
OgM	pu	4.5	3.9	4.0	4.0	4.3	4.0	2.8	4.0	4.0	4.0	3.9	pu	3.2	5.8	3.4	2.5	6.9	pu	pu	2.7	2.8	7.0	5.6	2.4	3.7	3.8	4.	7.4	3.2	2.8	2.7
<u>а</u>	01	=	12	~	4	15	_	2	$\sim$	4	2	9	_	∞	6	0	=	12	<u>~</u>	4	15	9		<u>&amp;</u>	61	20	21	22	23	24	25	26
≯	4.10w	4.10w	4.10w	4.10w	4.10w	4.10w	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1

$ZrO_2$	0.033	0.004	0.015	0.012	0.035	0.034	0.034	0.033	0.007	0.034	0.033	0.010	900'0	0.035	900'0	0.007	0.033	0.033	0.035	0.032	0.035	0.033	0.01	900'0	0.032	0.032	0.004	0.010	0.01	0.017	0.034	0.035
SrO	0.088	0.258	0.042	0.027	0.084	0.061	0.064	0.084	0.027	0.085	980'0	0.155	0.324	0.087	0.018	0.017	0.064	0.063	0.062	0.061	0.065	0.062	0.027	0.154	0.064	0.062	0.017	0.039	0.107	0.043	0.062	0.061
$Rb_2O$	0.005	0.00	0.01	0.014	0.004	0.003	0.003	0.005	910.0	0.004	0.004	0.00	0.00	0.004	pu	pu	0.004	0.003	0.004	0.004	0.004	0.003	910.0	0.00	0.003	0.003	pu	0.005	0.00	0.011	0.004	0.003
As <sub>2</sub> O <sub>3</sub>	0.143	pu	0.018	0.043	0.116	0.120	0.109	0.154	pu	0.182	0.120	0.017	900.0	0.128	0.447	0.447	0.162	0.164	0.112	0.174	0.108	0.118	0.034	0.008	0.124	0.112	910.0	pu	pu	pu	0.168	0.115
ZnO	0.028	0.007	0.035	0.033	0.027	0.028	0.021	0.029	0.030	0.027	0.028	0.007	pu	0.026	pu	pu	0.027	0.022	0.018	0.019	0.024	0.025	0.04	0.004	0.023	0.023	910.0	0.017	910.0	0.065	0.022	0.022
CuO	900'0	pu	0.031	0.009	0.009	0.013	0.018	0.015	0.007	0.011	0.011	pu	0.002	0.008	0.003	0.00	0.012	0.012	0.009	0.013	0.011	0.012	0.009	pu	0.012	0.010	0.057	pu	0.005	0.097	0.009	0.011
$Fe_2O_3$	1.350	0.741	0.618	0.530	1.394	1.193	1.198	1.365	0.338	1.412	1.369	0.851	0.495	1.383	0.194	0.211	1.165	1.126	1.136	1.08	1.197	1.192	0.463	0.847	1.142	1.130	0.929	1.102	0.920	0.740	1.183	1.206
MnO	0.982	0.009	0.835	0.773	0.874	0.541	0.566	0.936	0.941	0.972	0.948	0.017	pu	096.0	0.607	0.551	0.546	0.582	0.537	0.526	0.599	0.534	0.890	0.025	0.534	0.587	2.277	0.093	0.194	1.037	0.552	0.586
CaO	23.8	4.4	15.4	12.2	23.9	24.2	27.4	22.3	14.9	22.8	23.4	19.2	12.7	24.5	15.6	15.1	27.3	25.4	26.2	25.6	27.4	27.2	14.5	22.3	27.4	26.5	12.5	24.5	27.0	15.4	26.0	25.0
K <sub>2</sub> O	4.4	2.8	9.0	7.7	4.5	3.9	4.2	4.3	9.5	4.3	4.5	2.7	3.3	4.4	0.0	0.	4.	3.9	4.0	3.9	4.2	4.	8.6	2.1	4.0	4.	0.0	5.7	2.6	8.9	3.9	4.0
ס	pu	0.7	9.0	9.0	pu	0.3	pu	pu	0.5	0.2	pu	9.0	9.0	pu	pu	pu	0.3	9.0	pu	0.3	pu	pu	9.0	4.0	pu	pu	pu	pu	9.0	0.5	4.0	0.2
SO3	8.1	9.0	2.2	7.6	6.0	5.6	0.7	3.4	<u>.</u> 5	4.8	0.7	6.0	0.5	0.8	6.0	<u></u>	5.4	1.0	1.7	7.4	0.7	2.1	5.0	0.8	4.0	9.0	6.0	6.0	1.2	<u>4</u> .	9.	4.7
$P_2O_5$	2.4	1.2	4.5	3.1	2.3	3.4	2.7	2.5	4.2	2.8	2.3	1.2	<u>~</u>	2.2	pu	pu	3.6	4.4	2.9	3.6	2.5	2.9	4.8	pu	2.5	2.4	pu	2.2	2.0	3.9	4.7	2.7
SiO <sub>2</sub>	79.4	9.68	77.3	75.3	81.9	75.2	75.4	75.8	77.0	76.5	78.6	83.4	1.06	79.5	94.7	94.4	73.5	65.5	74.3	6.79	77.5	74.0	71.4	84.0	71.8	73.6	86.9	84.6	83.5	77.9	71.1	71.8
$Al_2O_3$	3.9	3.7	3.2	2.8	4.2	4.0	4.2	3.8	<u>~</u>	3.9	4.2	3.5	2.6	4.3	0.8	0:	4.0	3.6	4.0	3.9	4.3	3.9	2.2	2.7	3.6	3.6	2.2	3.7	2.7	2.9	4.0	3.5
OgM	3.6	4.5	5.5	5.5	3.9	2.6	3.2	2.9	6.6	3.2	3.5	3.9	7.0	3.8	pu	pu	3.9	2.8	3.7	<u>~</u> .	3.8	3.5	8.2	3.7	2.5	3.7	pu	2.3	4.	7.3	3.3	2.8
۵	27	28	29	30	3	32	33	34	35	36	37	38	39	40	4	42	43	4	45	46	47	48	49	20	51	52	53	54	55	26	57	28
≯	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1								

~	<u>.</u> ر		-	-	<b>~</b> !	~		٠.	_	.0	~	-	~	-	~	-			~	_	~	•	٠.	٠.		$\overline{}$	~		٠.	٠.	٠.	-
ZrO	0.00	0.00	0.00	0.03	0.032	0.00	0.00	0.00	0.007	0.01	0.033	0.03	0.033	0.02	0.023	0.03	0.035	0.015	0.00	0.017	0.00	0.00	0.00	0.00	0.0	0.010	0.00	0.00	0.00	0.00	0.006	0.02
SrO	910.0	910.0	0.019	0.085	0.085	0.019	0.015	0.015	0.01	0.039	0.063	980.0	980.0	0.092	0.090	0.083	0.084	0.042	0.342	0.063	0.022	0.023	910.0	0.137	0.127	0.089	0.183	0.007	0.126	0.015	0.128	0.231
$Rb_2O$	0.001	pu	pu	0.004	0.004	pu	pu	pu	0.00	0.012	0.003	0.004	0.004	0.004	0.005	0.004	0.005	0.011	0.00	0.005	0.00	0.00	pu	0.00	0.00	0.002	0.00	0.00	pu	pu	0.001	0.00
$As_2O_3$	0.261	0.024	0.268	0.129	0.157	0.250	0.020	0.498	900'0	0.017	0.115	0.144	0.162	0.106	0.	0.189	0.123	0.018	pu	0.135	0.021	0.025	0.515	pu	0.013	pu	0.012	pu	900'0	0.498	0.010	9000
ZnO	0.00	0.027	0.002	0.025	0.026	0.002	0.012	pu	pu	0.038	0.027	0.024	0.028	0.032	0.028	0.024	0.028	0.038	pu	0.029	0.009	0.007	pu	0.004	0.008	0.005	0.010	0.003	0.003	pu	0.003	0.001
CnO	0.010	0.067	pu	0.015	0.010	pu	0.062	pu	pu	0.029	0.012	0.007	0.015	0.009	0.017	0.010	0.011	0.033	pu	0.010	0.004	0.002	0.002	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.228	0.995	0.280	1.355	1.363	0.265	0.937	0.174	0.413	0.612	1.177	1.309	1.369	1.124	1.040	1.283	1.359	0.602	0.314	1.130	1.362	1.360	0.206	0.872	1.034	0.635	1.082	0.267	0.803	0.181	0.799	0.863
MnO	0.317	2.527	0.390	196.0	0.963	0.350	2.523	0.523	pu	0.880	0.564	0.917	0.985	0.751	0.718	0.880	1.009	0.905	pu	1.008	0.924	0.894	0.559	0.023	0.039	0.010	0.030	pu	pu	0.542	0.004	0.001
CaO	14.1	13.0	17.4	23.4	23.0	0.91	12.5	14.3	15.2	16.8	26.5	22.9	23.1	24.5	23.8	21.8	23.6	16.4	0:	22.4	17.2	17.1	15.5	25.5	22.8	10.9	21.4	12.5	23.8	14.8	24.8	15.6
$K_2O$	1.0	0.2	4.0	4.5	4.2	0.3	0.2	0.0	4.0	10.2	4.2	4.3	4.3	5.5	5.3	4.	4.4	6.6	3.3	4.3	0.7	0.7	0.0	9.1	2.1	4.4	2.2	9.0	J.5	0.	J.5	3.5
D	pu	pu	6.0	pu	pu	0.8	pu	pu	pu	9.0	pu	0.2	pu	pu	0.2	0.3	pu	0.5	9.0	9.0	pu	pu	0.2	0.5	0.5	9.0	9.0	pu	9.0	pu	0.5	9.0
SO3	4.	4.0	<u>~</u>	<u></u>	3.5	2.0	9:	0:	<u></u>	0.5	0:	4.	3.2	=:	2.2	1.7	<u>4</u> .	0.8	pu	0.8	1.2	<u></u>	9.1	<u>-</u> .	=	0.5	1.7	9.0	<u>~</u>	<u>4</u> .	<u>-</u> .	0.7
$P_2O_5$	pu	pu	pu	2.3	2.6	pu	pu	pu	pu	5.0	2.5	2.7	2.7	2.4	2.6	3.0	2.4	5.2	6:	4.	pu	pu	pu	pu	=	pu	1.2	pu	pu	pu	pu	pu
$SiO_2$	93.1	83.6	93.9	79.2	76.4	6.98	84.5	87.9	0.101	74.5	74.4	79.0	80.8	80.1	76.8	74.3	80.4	72.3	89.9	74.5	84.5	0.98	95.7	9.98	84.0	89.3	8.18	93.5	83.4	6.06	85.5	99.4
$Al_2O_3$	0.1	2.1	<u></u>	4.2	4.2	=	2.3	0:	4.	2.6	3.5	4.4	4.5	3.2	2.9	3.7	4.4	2.6	9:	4.4	2.4	2.5	1.2	2.6	3.4	<u>~</u>	2.7	2.0	3.0	1.2	3.	2.6
MgO	pu	pu	pu	4.	3.0	pu	pu	pu	pu	8.0	3.2	3.8	3.7	3.6	3.8	2.3	4.2	7.1	5.7	4.4	pu	pu	pu	0.9	4.5	4.3	4.4	pu	4.9	pu	5.7	4.3
Ь	59	09	19	62	63	64	65	99	29	89	69	20	7	72	73	74	75	9/	//	78	79	80	8	82	83	84	82	98	87	88	68	06
<b>X</b>	w02.1	w02.1	w02.1	w02.1	w02. I	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02. I	w02.1	w02.1	w02.1	w02. I	w02.1	w02.1	w02.1	w02. I	w02.1	w02. I	w02.1	w02.1	w02. I	w02.1	w02.1	w02.1	w02.1

$ZrO_2$	0.010	900'0	0.009	0.005	0.010	0.01	0.014	0.014	0.012	0.007	0.003	0.009	0.014	0.013	0.014	0.023	0.013	0.015	0.014	0.012	0.014	0.015	0.009	0.022	0.004	0.023	0.015	0.014	0.014	0.015	0.014	0.023
SrO	0.130	0.196	980.0	0.150	0.125	0.128	0.042	0.04	0.028	0.018	0.018	0.092	0.042	0.030	0.042	0.090	0.132	0.039	0.043	0.029	0.040	0.040	0.043	0.090	0.204	0.092	0.042	0.037	0.042	0.04	0.038	0.091
$Rb_2O$	0.00 ا	0.00	0.002	0.00	0.00	0.00	0.01	0.010	0.015	pu	pu	0.002	0.01	0.015	0.01	0.005	0.00	0.010	0.01	0.015	0.01	0.011	0.004	0.005	0.00	0.004	0.01	0.012	0.012	0.011	0.012	0.005
$As_2O_3$	pu	0.009	pu	0.005	pu	0.005	0.015	0.129	910.0	0.456	0.207	pu	0.009	pu	pu	0.100	0.01	0.049	0.039	0.015	pu	pu	pu	0.	0.010	0.	0.053	0.085	pu	pu	0.064	0.103
ZnO	900'0	0.005	9000	0.003	0.008	0.01	0.037	0.036	0.038	pu	pu	0.003	0.037	0.033	0.036	0.027	0.01	0.031	0.033	0.032	0.035	0.035	0.026	0.027	0.002	0.031	0.037	0.034	0.037	0.036	0.035	0.027
CnO	0.002	pu	pu	pu	0.00	0.00	0.031	0.030	0.008	pu	pu	pu	0.031	0.015	0.025	0.011	0.004	0.022	0.028	0.011	0.028	0.031	0.007	0.005	pu	0.018	0.028	0.029	0.026	0.029	0.029	0.011
$Fe_2O_3$	1.079	0.977	0.649	0.849	1.091	101.1	0.627	999.0	0.516	0.216	0.238	0.622	0.659	0.494	0.607		1.277	0.677	0.631	0.496	0.651	0.645	0.974	1.058	0.521	1.109	0.777	0.679	0.622	0.646	0.617	001.1
MnO	0.023	0.037	pu	910.0	0.033	0.034	0.845	0.713	0.842	0.611	0.374	0.014	0.842	0.849	0.885	0.721	0.139	0.684	0.853	0.857	0.828	0.864	0.061	0.705	pu	0.714	0.651	0.741	0.863	0.851	0.803	0.718
CaO	22.8	24.2	10.4	22.8	23.2	22.7	16.5	13.2	15.3	16.0	15.6	10.5	16.8	15.7	16.4	24.2	24.7	14.4	15.2	15.0	9.91	16.9	25.3	23.8	16.8	25.1	12.1	12.6	9.91	16.5	14.6	24.5
K <sub>2</sub> O	2.1	2.2	4.5	9.	2.1	2.0	0.01	7.5	0.01	0.0	4.0	4.2	l. O	9.6	0:01	5.4	2.3	8.4	0.6	8.6	1.01	10.3	5.3	5.6	2.4	5.6	7.2	7.5	1.0	1.0	8.9	5.6
D	9.4	0.5	9.0	0.5	0.5	0.5	4.0	4.0	0.5	pu	0.7	9.0	0.5	4.0	4.0	pu	9.0	0.5	0.5	0.5	4.0	9.0	pu	0.2	9.4	pu	0.3	0.3	4.0	0.4	9.4	pu
SO3	0.1	<u></u>	9.0	<u></u>	6.0	6.	1.7	8.3	3.0	=:	0.	0.5	2.0	=:	4.0	6.0	2.1	6.3	<u>~</u>	2.0	0.5	0.5	4.	6.0	6.	Ξ:	6.9	7.3	9.0	0.7	2.8	0.
$P_2O_5$	1.1	=	pu	pu	pu	=:	4.9	3.0	4.5	pu	pu	pu	5.0	3.8	4.9	2.5	7.	3.4	3.6	4.0	4.9	5.0	2.1	2.7	pu	2.5	3.0	3.–	5.1	4.8	4.4	2.5
$SiO_2$	80.4	86.2	88.4	84.5	85.7	9.08	73.3	1.08	76.1	7.86	92.9	86.7	72.0	74.6	74.3	80.0	80.5	76.2	82.4	71.7	73.9	75.1	87.8	79.3	90.2	81.4	87.8	81.4	75.4	75.1	74.5	79.0
$Al_2O_3$	2.9	3.0	<u>8</u> .	2.6	3.4	3.0	2.7	3.0	2.5	0:	<u>-</u> .	1.7	2.7	2.4	2.8	2.9	3.5	2.6	2.6	2.3	2.8	2.8	3.4	3.	7.	3.4	3.5	3.	2.6	2.7	2.7	3.
MgO	3.7	5.6	4.3	4.2	4.3	3.6	7.5	4.0	8.6	pu	pu	4.0	9.9	8.2	7.1	3.3	2.9	3.9	4.	7.3	7.4	7.5	3.0	3.5	3.5	4.5	3.8	3.6	8.0	7.5	4.9	3.8
Ь	16	92	93	94	95	96	_	2	$\sim$	4	2	9	_	$\infty$	6	0	=	12	$\underline{\sim}$	4	15	9		<u>&amp;</u>	6	20	21	22	23	24	25	26
>	w02.1	w02.1	w02.1	w02.1	w02.1	w02.1	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2

$ZrO_2$	0.023	0.015	0.032	0.014	0.015	0.005	0.007	0.008	0.005	0.010	0.009	0.015	0.015	0.015	0.009	0.007	0.014	0.01	0.012	0.012	0.012	0.007	0.01	0.014	0.013	0.012	910.0	0.012	0.015	0.012	900'0	0.014
SrO	0.088	0.043	0.064	0.04	0.040	0.232	0.184	0.023	0.011	0.053	0.054	0.040	0.072	0.042	0.023	910.0	0.042	0.046	0.044	0.047	0.029	0.020	0.032	0.04	0.045	0.044	0.046	0.029	0.040	0.043	0.129	0.039
$Rb_2O$	0.005	0.012	0.003	0.01	0.01	0.00	0.00	0.00	0.00	0.022	0.022	0.01	0.003	0.01	0.00	pu	0.01	0.005	0.005	0.005	910.0	pu	910.0	0.007	0.005	0.005	0.003	0.014	0.01	0.004	0.00	0.012
$As_2O_3$	0.100	0.050	0.110	0.010	pu	0.007	pu	0.011	0.018	0.022	0.017	0.010	0.048	0.038	0.014	0.427	0.035	0.020	0.022	0.027	900.0	0.594	0.015	960.0	0.036	0.020	pu	0.047	0.080	0.007	0.010	0.038
ZnO	0.025	0.039	0.022	0.034	0.033	0.002	0.008	0.009	0.00	0.048	0.043	0.032	0.017	0.032	0.010	0.00	0.028	0.025	0.017	0.025	0.032	pu	0.036	0.014	0.020	0.022	0.029	0.033	0.036	0.028	0.004	0.034
CnO	0.014	0.028	0.015	0.032	0.031	pu	pu	0.00	pu	0.002	0.002	0.028	0.004	0.028	0.003	0.00	0.026	0.005	0.005	0.012	0.009	pu	0.009	0.007	0.005	0.012	0.018	0.011	0.034	0.008	pu	0.031
$Fe_2O_3$	1.021	0.740	1.167	0.640	0.635	0.749	1.097	1.376	0.342	0.812	0.729	0.633	0.878	969.0	1.380	0.217	0.652	0.620	919.0	0.673	0.477	0.235	0.518	966.0	0.650	0.619	0.643	0.527	699.0	1.123	0.936	0.625
MnO	0.773	0.724	0.575	0.776	0.771	0.007	0.028	0.882	pu	1.053	0.999	0.864	0.735	0.773	0.849	0.597	0.821	1.072	1.051	0.995	0.912	0.500	0.883	0.918	1.077	1.079	0.654	0.807	0.765	0.292	0.015	0.820
CaO	24.4	13.5	27.2	16.3	9.91	14.0	21.9	17.2	17.1	8.6	10.9	17.0	24.6	12.1	16.7	15.3	16.3	21.6	21.7	22.7	15.2	1.91	15.6	22.8	21.3	21.6	22.4	14.7	15.1	24.2	23.3	0.91
$K_2O$	5.5	8.0	4.0	6.6	0.0	9.1	2.4	0.7	4.0	8.2	9.6	10.2	3.5	7.3	0.7	0.0	9.6	5.7	5.8	5.8	6.6	0.2	6.6	6.3	5.6	5.7	4.7	8.9	9.2	4.8	9.1	9.4
D	pu	4.0	pu	4.0	4.0	9.0	4.0	pu	pu	0.2	pu	4.0	9.0	0.3	pu	pu	4.0	9.0	9.0	9.0	9.0	0.3	0.5	pu	0.4	4.0	9.0	0.5	4.0	4.0	0.4	0.5
$SO_3$	0:1	5.1	2.2	0.8	9.0	0.5	6.0	9.0	<u></u>	46.2	51.8	9.0	2.1	4.3	0.5	0:	3.	9.0	6.0	0.5	0.7	0:	1.7	9.0	2.5	0.7	0.7	5.8	4.0	0.8	2.1	2.5
$P_2O_5$	2.5	3.8	2.4	4.7	4.9	Ξ.	1.2	pu	pu	4.5	5.3	2.0	3.	2.3	pu	pu	4.8	2.7	2.9	3.0	4.0	pu	4.2	2.6	3.3	2.6	3.4	3.9	4.6	3.2	pu	2.0
SiO <sub>2</sub>	6.67	81.0	73.5	71.5	73.3	94.9	8.98	87.2	103.2	32.6	26.9	75.8	74.3	94.3	87.8	95.5	73.7	77.4	78.8	77.1	74.9	99.5	77.5	76.4	77.6	76.5	78.2	68.5	74.4	80.5	84.9	73.1
$Al_2O_3$	3.1	3.	4.	2.7	2.6	2.0	3.3	2.6	3.6	9.0	0.8	2.9	4.8	3.	2.8	Ξ	2.9	6.5	6.7	8.9	2.0	<u></u>	2.8	7.9	6.9	6.2	9.9	2.3	2.7	3.4	3.0	2.9
OgM	3.6	4.9	3.2	6.7	7.4	4.2	5.1	pu	pu	2.8	3.4	7.7	5.4	3.2	pu	pu	7.1	4.0	3.9	4.4	7.7	pu	9.0	5.7	3.6	3.2	3.8	6.4	6.2	2.8	4.7	7.4
Ь	27	28	29	30	3	32	33	34	35	36	37	38	39	40	4	42	43	4	45	46	47	48	49	20	51	52	53	54	_	2	$\sim$	4
>	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.2	w02.3	w02.3	w02.3	w02.3								

$ZrO_2$	0.014	0.011	0.013	0.013	0.013	0.013	0.013	0.011	0.011	0.017	0.012	0.012	0.008	0.012	0.011	0.012	0.008	0.012	0.012	0.020	0.013	0.011	0.012	0.015	0.012	0.011	0.034	0.015	0.01	910.0	0.015	0.014
SrO	0.036	0.030	0.040	0.030	0.049	0.030	0.030	0.030	0.029	0.045	0.030	0.030	0.023	0.030	0.030	0.030	0.021	0.029	0.030	0.048	0.040	0.027	0.031	0.042	0.028	0.029	0.085	0.039	0.029	0.048	0.040	990.0
$Rb_2O$	900'0	0.014	0.012	0.015	9000	910.0	910.0	910.0	0.015	0.004	0.014	0.015	0.00	0.014	0.017	0.015	0.00	0.014	0.014	0.004	0.01	910.0	0.014	0.012	0.015	0.014	0.004	0.010	0.015	0.002	0.012	0.009
$As_2O_3$	0.028	0.021	0.056	0.080	0.044	0.045	0.042	0.052	0.071	pu	0.018	0.048	0.022	pu	0.036	0.047	0.013	0.007	0.075	900'0	0.059	0.035	0.014	0.062	0.046	0.029	0.131	0.080	0.047	090.0	0.015	910.0
ZnO	0.017	0.035	0.032	0.031	0.021	0.036	0.035	0.034	0.033	0.026	0.035	0.035	0.008	0.035	0.037	0.031	0.009	0.033	0.034	0.025	0.034	0.034	0.032	0.036	0.036	0.037	0.028	0.034	0.032	0.020	0.036	0.040
CnO	0.007	900'0	0.029	0.009	900'0	0.004	900'0	0.008	900'0	0.009	0.010	0.013	pu	0.007	0.010	0.009	0.004	0.014	0.012	0.012	0.025	900'0	0.013	0.032	0.012	0.010	0.010	0.029	910.0	0.002	0.028	0.026
$Fe_2O_3$	918.0	0.465	0.635	0.533	0.869	0.520	0.512	0.469	0.488	1.491	0.495	0.509	1.400	0.493	0.464	0.478	1.330	0.484	0.495	1.508	0.682	0.522	0.491	0.622	0.464	0.502	1.346	0.681	0.523	0.924	0.599	0.680
MnO	0.742	0.829	0.756	0.829	0.771	0.907	0.919	0.848	0.851	0.223	0.965	0.820	0.932	0.862	0.921	0.900	0.857	0.885	0.900	0.278	0.788	0.838	0.895	998.0	0.868	0.917	096'0	0.760	0.842	0.693	0.849	1.131
CaO	21.9	15.1	16.0	14.7	20.4	15.2	15.2	14.2	14.6	25.0	15.6	14.9	17.5	15.1	14.5	14.8	16.8	15.3	14.5	23.4	14.0	13.8	15.8	15.7	14.4	15.3	23.5	15.2	14.8	20.5	16.3	18.6
$K_2O$	1.9	9.3	9.4	8.9	0.9	6.6	8.6	9.2	0.6	5.8	9.4	0.6	0.8	9.3	8.6	6.7	0.7	9.4	8.8	5.9	8.4	9.5	9.6	9.5	9.3	9.3	4.4	9.1	8.7	<u>8</u> .	1.0	7.8
D	0.2	0.5	0.5	9.0	4.0	0.5	0.5	0.5	0.5	pu	4.0	0.5	pu	9.0	0.5	0.5	pu	0.5	9.0	pu	9.0	0.5	0.5	0.5	0.5	0.5	pu	0.5	9.0	9.0	0.4	0.5
SO3	1.2	3.4	3.4	5.7	2.8	5.1	4.7	6.9	3.5	<u> </u>	3.7	<u>-</u> .	0.5	2.3	<u>4</u> .	8.9	0.5	2.1	4.6	=	4.2	4.2	3.5	2.0	2.1	1.2	9.1	3.8	4.	0.3	0.	1.2
$P_2O_5$	2.6	4.2	4.9	4.7	2.9	4.4	4.3	4.2	4.0	2.7	4.	4.4	pu	3.9	4.4	4.6	pu	4.	4.4	2.7	4.3	4.	4.2	5.8	4.5	4.5	2.4	5.8	4.4	2.1	5.1	4.3
$SiO_2$	74.5	73.1	73.4	70.7	77.0	72.1	71.2	1.49	73.7	77.5	73.5	70.9	87.7	72.2	77.5	71.5	83.9	75.1	70.5	80.7	75.6	74.5	75.3	70.3	71.0	72.6	9.62	64.7	70.8	87.8	74.6	73.3
$Al_2O_3$	6.7	2.4	2.9	2.8	7.1	2.9	2.2	2.0	2.4	3.9	2.6	2.9	2.8	2.3	2.2	2.5	2.4	2.5	2.9	4.6	3.0	2.5	2.9	2.8	2.1	2.4	4.4	2.7	3.0	5.4	2.8	2.7
MgO	4.4	7.6	7.1	9.9	4.6	7.3	7.2	5.7	7.4	3.2	—. —.	5.9	pu	7.2	7.4	7.7	pu	0.6	6.1	3.7	5.4	9.9	8.4	5.5	7.7	7.0	3.8	4.6	9.9	3.9	7.2	5.9
Ъ	2	9	7	8	6	0	=	12	<u>~</u>	<u>4</u>	15	9	17	<u>∞</u>	6	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34	35	36
>	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3								

$ZrO_2$	0.014	0.012	0.012	0.009	0.012	0.012	0.008	0.014	0.014	0.009	0.014	0.012	0.007	0.036	0.014	0.015	0.012	0.015	0.013	0.008	0.011	0.013	0.017	0.013	0.005	0.013	0.008	0.002	0.010	900'0	0.005	0.008
SrO	0.042	0.030	0.031	900.0	0.030	0.029	0.221	0.039	0.039	0.023	0.040	0.028	0.023	0.064	0.040	0.040	0.029	0.038	0.047	0.024	0.029	0.043	0.061	0.04	0.199	0.109	0.369	0.342	0.137	0.203	0.257	0.148
$Rb_2O$	0.012	0.015	0.015	pu	0.014	0.014	0.00	0.012	0.012	0.00	0.01	0.015	0.00	0.004	0.01	0.004	0.015	0.015	0.003	0.00	0.014	0.003	0.003	0.012	0.00	0.002	0.00	0.00	0.00	0.00	0.00	0.001
$As_2O_3$	0.027	0.036	0.040	pu	0.038	0.029	pu	0.119	0.057	0.026	0.041	0.043	0.020	0.106	0.152	pu	0.041	0.089	900'0	0.022	0.099	0.031	0.021	0.168	pu	pu	0.012	0.009	0.018	900'0	0.011	0.007
ZnO	0.036	0.030	0.035	0.007	0.032	0.031	0.004	0.035	0.031	0.009	0.027	0.035	0.009	0.024	0.027	0.023	0.031	0.030	0.021	0.010	0.033	0.022	0.026	0.034	0.012	0.013	0.004	0.003	0.008	0.005	0.004	0.005
CnO	0.027	0.010	0.008	pu	0.010	900.0	pu	0.032	0.034	0.003	0.033	0.009	0.005	0.014	0.032	0.013	900.0	0.019	900.0	0.001	0.009	0.007	pu	0.026	pu	900'0	pu	pu	pu	pu	pu	0.001
$Fe_2O_3$	0.646	0.501	0.481	0.256	0.502	0.491	0.862	0.569	0.645	1.359	0.601	0.497	1.354	1.153	0.628	1.323	0.486	0.596	0.509	1.461	0.480	1.105	0.602	0.632	1.105	1.124	0.588	0.600	1.022	0.967	0.532	0.876
MnO	0.847	0.804	0.866	pu	0.899	0.901	0.045	0.789	0.810	0.861	0.821	0.758	916.0	0.559	0.772	0.245	0.823	0.789	0.759	0.941	0.767	0.317	0.563	0.772	0.019	0.186	0.015	0.005	0.072	0.011	0.001	0.055
CaO	0.91	14.8	15.0	16.4	15.3	14.5	21.4	15.5	15.2	17.5	15.9	14.9	16.9	27.0	14.6	24.9	14.9	14.2	23.6	16.5	13.4	24.3	25.2	15.8	22.0	25.3	13.4	12.7	22.5	20.4	6.7	22.4
$K_2O$	9.6	9.5	9.2	0.5	9.1	9.4	=	8.9	1.6	0.7	9.5	9.6	0.7	4.	9.8	5.3	6.7	1.0	4.5	0.7	8.	4.	4.	9.8	2.2	2.8	4.4	3.7	2.2	2.3	3.8	Ξ:
Ū	9.0	0.5	0.5	pu	9.0	0.5	0.8	9.0	9.0	pu	0.5	9.0	pu	pu	9.0	pu	0.5	0.7	0.7	pu	0.5	9.0	0.7	0.5	0.5	9.0	0.7	9.0	0.5	9.4	0.3	0.7
SO3	2.3	4.6	5.8	4.	5.8	4.7	9:0	5.8	3.0	0.7	2.2	0.9	9.0	1.2	5.3	1.2	3.9	<u>~</u>	9.0	0.5	7.2	3.4	1.7	7.5	0:	7.	9.0	0.5	J.	6.0	0.8	2.0
$P_2O_5$	4.6	4.4	4.6	pu	3.8	4.	<u></u>	4.5	5.3	pu	5.0	4.6	pu	2.4	4.2	3.2	4.5	7.2	3.3	pu	3.2	3.5	3.9	4.2	=	2.3	2.3	6.	6.	=	pu	1.2
$SiO_2$	74.4	7.1.7	71.8	8.16	72.1	72.2	85.7	67.2	70.5	0.06	70.7	71.4	87.I	77.7	69.3	78.3	73.6	64.2	77.2	83.1	0.99	9.62	74.1	69.4	85.9	80.7	94.3	96.2	80.5	1.98	6.06	78.6
$Al_2O_3$	2.9	2.7	2.6	0.8	2.5	2.7	<u>~</u> .	2.6	2.6	2.9	2.6	2.4	2.4	4.0	2.9	4.0	2.2	2.6	4.2	2.4	2.0	3.4	4.9	2.9	3.	3.2	3.2	3.0	2.7	2.7	2.5	2.9
OgM	6.2	8.2	8.9	pu	9.9	7.5	6.3	6.4	5.9	pu	6.5	8.2	pu	3.4	5.6	2.8	8.3	4.4	4.0	pu	5.4	3.	4.3	0.9	4.3	3.6	9.8	7.9	4.2	4.6	9.9	4.5
Ь	37	38	39	40	4	42	43	4	45	46	47	48	49	20	21	52	53	54	55	26	57	28	29	09	_	2	$\sim$	4	2	9	7	<b>∞</b>
>	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.3	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4						

$ZrO_2$	0.004	0.007	0.009	0.009	9000	0.008	0.009	0.005	0.003	0.004	0.007	0.005	0.007	0.005	0.007	0.046	0.015	0.012	0.013	0.015	0.015	0.013	0.015	0.005	0.015	0.012	0.010	9000	0.014	0.015	0.013	0.015
SrO	0.230	0.002	0.229	0.077	0.050	0.196	0.351	0.171	0.005	0.328	0.228	0.348	0.347	0.346	0.343	0.054	0.04	0.028	0.039	0.059	0.040	0.040	0.040	0.345	0.038	0.030	0.109	0.187	0.040	0.04	0.029	0.040
$Rb_2O$	0.001	0.003	0.00	0.00	0.002	0.00	0.002	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.003	0.012	0.014	0.012	0.002	0.012	0.011	0.012	0.00	0.01	0.015	0.00	0.00	0.012	0.011	0.015	0.011
$As_2O_3$	pu	pu	910.0	pu	pu	0.005	0.034	0.009	0.213	0.019	0.008	0.011	0.008	0.012	0.007	0.043	pu	pu	pu	pu	0.008	0.011	0.013	0.013	0.028	0.007	0.012	0.009	pu	0.026	0.021	0.009
ZnO	0.008	0.110	0.008	0.040	0.003	0.009	0.002	0.005	pu	0.003	0.008	0.002	0.003	0.004	pu	0.025	0.035	0.037	0.032	0.022	0.028	0.032	0.032	0.003	0.036	0.033	0.014	900.0	0.032	0.034	0.034	0.034
CnO	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	0.005	0.002	pu	pu	pu	0.010	0.027	0.011	0.034	0.003	0.031	0.029	0.031	pu	0.024	0.004	0.005	pu	0.026	0.031	0.009	0.026
$Fe_2O_3$	0.949	0.013	1.097	0.643	0.313	960.1	0.648	0.886	0.300	0.412	1.015	0.553	0.591	0.620	0.610	1.102	0.624	0.475	0.614	1.206	0.617	0.620	0.600	0.672	0.605	0.475	0.944	1.314	0.626	0.618	0.500	0.649
MnO	0.042	pu	0.043	pu	0.046	0.033	0.010	0.009	pu	0.010	0.026	0.028	0.008	0.005	0.045	0.484	0.885	0.897	0.789	0.261	0.859	0.823	0.794	910.0	0.833	0.838	0.127	0.020	0.842	0.882	0.815	0.880
$C_{aO}$	21.1	6.4	21.7	20.6	8. —	22.2	<u> </u>	20.0	8.4	13.2	22.1	6:1	6:11	12.0	11.7	23.6	16.9	15.3	16.3	25.6	9.91	15.5	16.3	<u>8</u> .	15.7	14.8	22.3	0.61	16.4	15.9	4.4	16.7
K <sub>2</sub> O	2.3	4.	6:1	0.	5.1	2.2	4.6	2.0	<u></u>	3.0	6:1	3.6	3.5	3.6	3.5	4.5	0.0	8.6	1.01	2.9	0.01	9.6	8.6	3.9	8.6	8.6	3.0	2.6	6.6	6.7	9.3	0.01
D	0.5	0.7	0.5	0.5	0.7	9.0	0.7	9.0	pu	9.0	4.0	9.0	0.5	9.0	0.5	pu	4.0	0.5	4.0	0.7	4.0	4.0	4.0	9.0	4.0	0.5	0.5	0.3	4.0	9.0	0.5	4.0
SO3	1.2	9.0	2.0	0.7	9.0	0.	6.1	6.0	0.3	9.0	0.	0.5	0.3	0.5	4.0	0.7	0.5	<u></u>	4.	6.0	0.5	<u></u>	6.0	9.4	2.2	6.0	2.2	6.0	0.7	<u></u>	4.4	9.0
$P_2O_5$	1.5	pu	<u>8.</u>	pu	pu	=	3.2	=	pu	<u>~</u> .	9:1	1.7	6:1	6:	1.7	2.8	5.1	4.	4.5	2.5	4.9	5.1	4.6	<u>-</u> .	4.6	3.7	2.0	pu	4.7	4.8	4.9	2.0
SiO <sub>2</sub>	78.3	91.1	84.2	89.5	87.1	82.5	73.0	79.0	92.2	92.0	85.5	9.16	87.6	94.6	89.4	81.4	74.7	75.9	0.89	80.5	73.5	73.8	71.2	97.1	69.5	74.6	81.5	85.9	72.5	8.89	71.9	75.3
$Al_2O_3$	3.0	pu	3.8	3.3	Ξ	2.9	4.5	2.0	1.2	2.2	3.6	2.5	2.7	2.8	2.4	3.0	2.9	2.8	2.3	3.3	2.8	2.7	2.5	2.8	2.7	2.2	3.	4.4	2.6	2.3	3.2	2.9
$M_{gO}$	5.2	pu	5.6	pu	2.6	3.9	4.4	3.8	pu	8.9	5.9	6.7	6.7	6.7	5.9	3.2	7.5	8.7	5.7	2.3	7.6	8.9	6.5	6.7	5.6	8.4	3.7	4.4	0.9	5.3	6.9	7.2
Ь	6	0	=	12	<u> </u>	4	15	91		<u>&amp;</u>	61	20	21	22	23	24	25	26	27	28	29	30	$\overline{\mathbb{S}}$	32	33	34	35	36	37	38	39	9
<b>×</b>	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4	w02.4

$ZrO_2$	0.017	0.014	0.015	0.013	0.01	0.014	0.014	0.022	0.012	0.013	0.013	0.012	0.015	0.018	0.012	900'0	0.01	0.013	0.013	0.011	0.012	0.015	0.012	0.033	0.020	0.012	0.012	0.011	0.012	0.012	0.012	0.012
SrO	0.064	0.042	0.042	0.04	0.031	0.04	0.039	0.067	0.028	0.045	0.030	0.029	0.038	0.047	0.027	0.055	0.031	0.030	0.027	0.029	0.029	0.05	0.048	0.062	0.042	0.031	0.030	0.030	0.029	0.045	0.031	0.028
$Rb_2O$	0.002	0.01	0.01	0.01	0.014	0.01	0.01	0.003	910.0	0.004	0.014	0.014	0.01	0.004	0.016	0.004	0.015	0.015	910.0	910.0	910.0	0.004	0.004	0.003	0.003	0.015	0.014	0.014	0.014	0.005	0.015	0.015
$As_2O_3$	pu	0.032	0.039	pu	0.011	0.040	0.026	0.229	0.053	0.011	pu	0.011	0.024	pu	0.007	pu	0.015	0.009	0.028	0.007	0.029	pu	0.028	0.133	pu	0.050	0.021	0.014	0.008	0.019	pu	0.015
ZnO	0.026	0.036	0.035	0.032	0.037	0.039	0.030	0.024	0.036	0.024	0.033	0.037	0.035	0.024	0.034	0.010	0.037	0.032	0.033	0.036	0.031	0.030	0.019	0.025	0.025	0.033	0.034	0.032	0.032	0.023	0.036	0.039
CnO	0.001	0.031	0.034	0.023	0.012	0.031	0.031	0.009	0.010	0.010	600.0	0.012	0.033	0.008	0.012	0.001	0.004	0.014	600.0	900'0	0.004	0.007	0.048	0.012	0.008	0.011	0.012	910.0	0.009	0.002	0.014	0.011
$Fe_2O_3$	0.563	0.663	0.582	0.623	0.453	0.679	0.614	1.132	0.491	1.328	0.481	0.511	0.557	1.385	0.532	0.347	0.483	0.507	0.445	0.479	0.441	1.214	0.639	1.202	1.520	0.503	0.506	0.480	0.487	0.621	0.514	0.520
MnO	0.598	0.865	0.849	0.814	0.844	0.861	0.805	0.705	698.0	0.088	0.902	0.832	0.825	0.390	0.864	0.231	0.946	0.927	0.911	0.839	0.941	0.338	0.901	0.568	0.305	698.0	0.815	0.878	0.804	990.1	0.929	0.839
CaO	24.2	16.5	16.2	16.5	14.8	15.7	16.7	26.8	14.5	25.4	15.3	15.1	15.8	25.3	14.8	12.4	15.5	14.9	14.8	15.1	15.4	24.6	22.8	26.1	25.0	15.4	14.8	15.5	14.7	21.8	15.8	15.1
$K_2O$	3.7	8.6	6.7	8.6	0.6	9.5	1.0	3.7	8.6	5.3	8.6	9.6	8.6	4.9	8.6	5.8	6.6	9.1	6.6	6.6	10.2	5.7	4.8	4.0	4.5	9.4	9.5	8.6	9.6	5.8	6.7	0.01
ט	9.0	4.0	9.0	9.0	0.5	0.5	0.5	pu	0.5	pu	4.0	0.5	9.0	pu	0.5	0.7	4.0	4.0	0.5	0.5	4.0	pu	0.5	0.2	4.0	0.5	0.5	0.5	4.0	0.3	4.0	4.0
SO3	9.0	2.3	6.0	0:	3.8	2.2	0.8	2.8	5.0	2.4	9.0	2.1	0.7	6.0	1.7	0.3	2.0	J.5	3.	1.2	3.3	6.	<u></u>	4.0	0.7	<u></u>	4.0	2.1	1.2	0.3	0.7	<u>∞</u> .
$P_2O_5$	3.6	5.0	5.5	4.6	4.2	5.4	5.1	2.7	4.5	2.6	4.2	3.9	4.4	2.7	3.8	pu	4.0	4.	3.9	4.	4.0	3.4	3.0	3.3	3.6	4.5	4.0	3.9	3.5	2.8	3.8	4.0
SiO <sub>2</sub>	76.4	72.1	73.4	9.69	71.0	73.3	73.8	76.5	73.4	77.8	75.0	74.0	71.5	76.6	74.9	7.16	73.6	77.2	75.3	77.5	76.0	75.1	76.0	74.8	78.8	73.9	75.0	76.3	71.5	78.0	75.1	74.1
$Al_2O_3$	5.0	2.9	2.8	2.2	2.6	3.7	3.	3.8	2.1	4.	2.3	2.4	2.4	3.8	2.3	1.2	2.3	2.6	2.5	2.6	2.2	3.8	l.9	4.0	4.4	2.6	2.6	2.8	6.	6.5	2.4	2.6
MgO	4.4	6.7	7.3	8.9	7.2	5.9	7.3	3.0	9.8	2.2	8.0	7.8	6.7	2.9	7.9	2.9	8.5	8.4	8.5	8.3	9.1	3.2	4.4	<u>~</u> .	3.3	8.0	7.3	8.9	7.5	4.3	8.2	8.5
Ь	14	42	43	4	45	46	47	_	2	$\sim$	4	2	9	_	∞	6	0	=	12	13	4	15	91		8	61	20	21	22	23	24	25
>	w02.4	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5						

$ZrO_2$	0.011	0.012	900.0	0.013	0.007	0.012	0.013	0.021	0.012	900.0	0.012	0.01	0.002	0.012	0.01	0.012	0.013	0.013	0.034	0.013	0.012	0.012	0.012	0.034	0.01	0.013	0.012	0.012	0.009	0.01	0.011	0.011
SrO	0.029	0.032	0.025	0.030	0.053	0.027	0.045	990.0	0.029	0.281	0.028	0.028	0.274	0.029	0.027	0.030	0.038	0.030	0.084	0.039	0.029	0.030	0.028	0.063	0.029	0.029	0.030	0.029	0.021	0.031	0.030	0.029
$Rb_2O$	0.015	0.014	0.017	0.015	0.004	0.015	0.005	0.004	0.014	0.002	910.0	0.017	0.002	0.015	910.0	0.015	0.004	0.015	0.004	0.01	0.015	0.014	910.0	0.003	0.014	910.0	910.0	910.0	910.0	0.015	0.015	0.017
$As_2O_3$	0.031	pu	0.038	0.014	0.013	pu	0.018	0	0.019	pu	0.034	0.055	0.023	900.0	pu	pu	pu	0.015	0.122	0.008	910.0	0.010	0.024	0.110	0.014	0.038	0.008	0.024	0.033	0.007	0.013	0.030
ZnO	0.032	0.035	0.031	0.034	0.007	0.035	0.021	0.030	0.032	0.00	0.033	0.032	0.002	0.035	0.034	0.032	0.020	0.036	0.025	0.030	0.037	0.031	0.032	0.023	0.033	0.033	0.029	0.033	0.028	0.030	0.038	0.038
CnO	0.010	0.008	0.005	0.012	pu	0.011	0.004	900'0	0.011	pu	0.008	0.011	pu	0.010	0.004	0.011	0.011	0.011	0.010	0.026	0.004	0.011	0.005	0.014	0.009	0.008	0.011	0.008	0.015	0.009	0.008	0.011
$Fe_2O_3$	0.474	0.487	0.292	0.477	0.334	0.467	0.686	1.251	0.472	0.750	0.462	0.448	0.760	0.445	0.490	0.505	1.152	0.517	1.365	0.591	0.481	0.521	0.524	1.173	0.484	0.515	0.472	0.542	0.408	0.451	0.511	0.491
MnO	0.850	0.859	900.1	0.959	0.211	0.831	1.053	0.840	0.831	0.035	0.863	0.904	0.045	0.868	0.891	0.927	0.311	0.902	0.912	0.842	0.902	0.904	0.982	0.580	0.831	0.834	0.957	0.880	0.701	0.855	0.903	096.0
CaO	15.1	15.7	13.9	15.3	12.0	15.0	21.6	23.4	15.4	8.9	15.5	14.3	8.8	15.3	15.1	15.6	24.9	15.6	23.3	16.2	14.8	15.6	14.7	27.7	15.4	15.2	15.7	14.9	13.3	15.7	14.9	15.0
$K_2O$	9.5	6.7	8.9	9.5	5.6	6.6	5.7	4.	9.5	4.0	6.6	6.7	4.0	6.7	10.3	6.6	5.0	6.6	4.	8.6	6.7	6.7	6.7	4.2	9.5	9.5	9.6	9.6	 4.	6.7	8.6	6.7
D	9.0	0.5	9.0	9.0	9.0	9.0	9.0	0.2	9.0	0.5	9.0	0.5	0.5	0.5	0.5	0.5	0.3	0.5	pu	0.5	0.5	0.5	0.5	pu	0.5	0.5	9.0	0.5	0.5	9.0	0.5	0.5
SO3	5.4	1.7	8.0	2.6	0.3	0.7	0.5	0.3	9:1	pu	3.5	5.4	pu	0.8	<u>4</u> .	0.7	=:	2.4	9:	0.	3.0	2.0	3.3	0.7	2.8	4.8	6.0	2.3	2.6	<u>4</u> .	2.8	2.8
$P_2O_5$	4.7	4.	3.7	4.0	pu	4.	2.8	2.8	4.0	<u></u>	4.4	4.4	4.	3.9	3.9	4.0	3.3	4.4	2.3	5.3	4.2	3.9	3.9	2.6	4.3	4.3	3.9	4.	4.5	4.	4.3	3.6
$SiO_2$	2.69	75.7	72.3	75.2	6.06	75.6	77.1	75.4	75.3	85.5	73.8	72.9	0.98	74.5	75.8	9.9/	4.18	76.5	77.1	74.9	73.3	74.4	77.2	78.3	75.8	9.59	74.0	74.5	70.3	6.9/	73.9	75.4
$Al_2O_3$	2.1	2.8	6:1	2.4	0.	2.5	6.4	3.8	2.5	1.7	2.3	2.1	1.7	2.5	2.1	2.6	3.5	2.4	3.9	2.6	2.4	2.4	2.4	4.	2.8	1.7	2.6	2.1	=	2.6	2.5	2.4
MgO	7.6	8.9	7.1	7.7	3.3	9.1	4.	3.8	8.2	5.8	8.0	8.0	6.2	7.5	8.2	8.6	3.5	8.8	3.4	7.4	8.	8.4	8.0	4.	8.	5.8	7.6	8.7	6.2	8.4	7.7	7.2
Ь	26	27	28	29	30	3	32	33	34	35	36	37	38	39	9	4	42	43	4	45	46	47	48	49	20	21	52	53	54	55	26	57
<b>*</b>	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5	w02.5									

$ZrO_2$	0.012	0.018	0.015	0.012	0.004	0.015	0.018	0.019	0.019	0.019	0.033	0.014	0.018	0.004	0.019	0.007	0.012	0.020	910.0	0.019	0.012	0.020	0.023	900'0	0.013	0.021	0.032	0.037	0.036	0.020	0.020	0.003
SrO	0.028	0.035	0.050	0.063	0.013	0.065	0.070	990.0	990.0	0.068	690.0	0.061	0.067	0.306	0.068	0.318	990.0	0.067	0.067	0.074	0.064	690.0	990.0	0.306	0.056	0.071	0.071	0.064	0.063	690.0	0.068	0.273
$Rb_2O$	0.015	0.004	0.004	0.002	0.00	0.003	0.003	0.003	0.003	0.003	0.002	0.002	0.003	0.00	0.003	0.002	0.002	0.003	0.003	0.003	0.003	0.003	0.002	0.00	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.001
$As_2O_3$	0.029	0.070	0.027	0.010	0.724	0.018	0.030	pu	pu	900'0	0.021	0.059	0.042	910.0	pu	0.021	0.005	0.023	pu	0.049	0.008	pu	0.009	0.033	pu	pu	0.009	0.012	pu	0.013	0.019	0.012
ZnO	0.028	0.021	0.022	0.053	pu	0.028	0.021	0.047	0.048	0.048	0.026	0.026	0.045	0.013	0.046	0.008	0.042	0.049	0.023	0.022	0.047	0.049	0.048	0.007	0.046	0.042	0.023	0.023	0.024	0.045	0.049	0.004
CnO	0.010	0.004	0.012	0.004	pu	0.002	0.004	0.008	0.009	0.009	0.003	0.007	0.012	pu	0.01	pu	0.012	0.010	0.007	0.002	0.007	0.01	0.010	pu	0.0	0.008	0.009	pu	0.004	0.013	0.010	pu
$Fe_2O_3$	0.440	0.792	1.317	1.362	0.521	0.724	0.772	1.560	1.54	1.574	0.893	0.675	1.630	0.682	1.577	0.936	1.315	1.584	0.749	0.717	1.324	1.623	1.331	0.903	1.60	1.688	0.770	0.773	0.799	1.590	1.610	0.730
MnO	0.891	0.748	0.268	0.144	0.076	0.749	0.929	0.154	0.167	0.190	0.843	0.733	0.141	0.037	0.187	0.051	0.147	0.185	0.692	0.924	0.132	0.131	0.146	0.034	0.086	0.170	0.843	0.800	0.785	0.143	0.180	0.042
CaO	13.7	21.8	25.3	21.3	12.3	23.3	22.4	20.6	20.3	21.3	23.3	23.1	20.7	11.7	21.0	<u> </u>	22.9	20.4	23.9	22.5	23.1	20.3	21.7	10.3	20.1	22.4	24.9	24.9	23.4	20.8	20.9	0.01
K <sub>2</sub> O	9.2	5.1	5.1	4.5	9.0	4.6	3.6	5.8	5.6	5.9	4.4	3.7	5.6	3.5	5.8	4.	5.5	5.5	4.0	3.9	5.6	5.7	5.6	3.5	6.3	6.2	4.7	4.	4.2	5.6	5.6	3.6
ū	9.0	0.3	pu	0.2	pu	9.0	0.5	0.2	pu	0.3	0.5	0.7	9.0	9.0	0.3	0.3	0.2	0.3	0.5	0.5	pu	0.3	0.3	9.0	0.3	0.3	9.0	9.0	9.0	0.3	0.3	4.0
SO3	4.4	5.9	2.9	0.	1.2	2.3	4.7	=	6.0	1.2	2.8	8.9	9.0	0.7	1.2	9.0	<u>~</u>	2.4	0.8	7.4	<u></u>	1.5	<u></u>	<u></u>	6.0	-5.	9.1	2.3	<u></u>	2.7	2.2	4.0
$P_2O_5$	4.2	3.4	3.0	1.7	pu	4.	3.0	2.5	2.3	2.8	3.3	4.0	4.0	<u></u>	2.4	Ξ	2.7	2.7	3.4	3.5	2.6	2.7	2.4	9.	2.8	2.7	3.4	3.8	3.3	2.9	2.7	pu
SiO <sub>2</sub>	74.9	76.2	74.1	69.3	200.7	70.3	69.5	76.3	72.7	79.1	72.8	1.69	73.6	89.2	77.8	86.4	9.08	70.4	72.6	72.0	81.9	76.9	81.9	85.0	79.0	80.3	69.7	72.9	74.0	78.7	9.9/	84.5
$Al_2O_3$	2.0	6.4	4.5	2.6	1.7	3.7	4.5	4.5	3.9	5.2	5.6	3.6	4.7	3.8	4.8	3.9	3.9	4.	4.0	5.0	4.2	4.6	4.6	3.4	5.5	5.8	5.6	5.5	5.7	5.2	5.0	3.7
MgO	8.7	4.5	2.9	pu	pu	3.7	4.3	3.6	3.2	4.7	4.9	4.6	3.8	7.5	4.0	l.9	4.2	2.7	4.5	4.	3.7	3.5	3.9	7.2	3.5	5.	5.0	5.0	5.2	4.5	3.7	4.2
Ь	58	26	09	_	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12	<u> </u>	4	15	91		<u>8</u>	61	20	21	22	23	24	25	26	27	28	29
≯	w02.5	w02.5	w02.5	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6	w02.6

$ZrO_2$	610.0	0.008	0.018	0.003	0.002	0.018	0.018	0.002	0.012	0.005	0.018	900.0	0.019	0.004	0.064	0.013	0.019	0.003	0.062	0.020	0.017	0.014	0.008	0.019	0.019	0.018	0.012	0.018	0.018	0.020	0.017	0.007
SrO	0.067	0.146	0.116	0.343	0.028	0.107	0.106	900.0	0.042	0.002	0.107	0.124	0	0.302	0.09	0.040	0.109	0.018	0.088	0.112	0.112	9000	0.024	0	0.106	0.107	0.151	0.107	0.109	0	0.081	0.280
$Rb_2O$	0.003	0.00	0.002	0.00	pu	0.002	0.002	pu	0.004	0.003	0.002	0.00	0.003	0.00	pu	0.004	0.002	pu	pu	0.002	0.002	pu	0.00	0.003	0.002	0.002	0.00	0.003	0.002	0.002	0.003	0.001
$As_2O_3$	pu	0.008	pu	0.014	0.708	pu	pu	0.009	910.0	pu	pu	0.007	pu	0.010	pu	pu	pu	0.274	pu	pu	pu	0.331	0.020	pu	pu	pu	pu	0.011	pu	pu	0.008	0.009
ZnO	0.055	0.009	0.027	0.004	0.009	0.022	0.024	pu	0.025	0.043	0.022	0.002	0.022	0.003	9000	0.023	0.026	pu	900.0	0.025	0.028	0.00	0.012	0.023	0.020	0.026	0.005	0.022	0.023	0.022	0.027	pu
CnO	600.0	0.004	0.007	pu	pu	0.007	0.004	pu	0.007	0.011	0.005	pu	0.002	pu	0.059	0.014	0.003	pu	0.052	900.0	0.007	pu	pu	0.004	0.004	9000	pu	0.004	0.007	900.0	0.007	pu
$Fe_2O_3$	1.611	0.761	1.646	0.574	0.355	619.1	1.584	0.175	=	0.002	1.560	0.863	1.556	0.644	1.444	1.162	1.644	0.323	1.416	1.654	1.644	0.199	1.500	1.631	1.593	1.619	0.793	1.605	1.568	1.643	1.656	0.559
MnO	0.151	0.055	0.307	0.031	0.311	0.234	0.259	pu	0.151	pu	0.295	pu	0.300	0.012	0.386	0.134	0.309	0.388	0.331	0.356	0.306	pu	0.932	0.280	0.286	0.280	0.030	0.282	0.321	0.285	0.103	0.011
CaO	19.2	23.8	22.3	12.0	14.7	20.8	20.9	15.6	25.4	5.6	21.6	22.2	22.4	0:	8.7	25.3	22.2	17.1	8.3	22.0	22.1	13.6	17.5	20.8	20.9	21.4	19.9	21.3	21.4	21.7	23.1	10.5
$K_2O$	5.3	2.7	4.4	3.6	0.2	4.	4.2	pu	5.2	4.7	4.3	2.1	4.	3.5	0.2	5.4	4.	0.3	0.2	4.4	4.3	pu	0.7	4.	4.	4.	2.1	4.	4.3	4.2	3.8	3.2
D	0.2	0.3	0.5	9.0	pu	0.5	0.5	pu	pu	0.8	9.0	0.3	0.5	9.0	pu	pu	0.5	0.8	pu	9.0	0.5	pu	pu	0.5	9.0	9.0	0.5	0.5	0.5	9.0	9.4	4.0
SO3	1.3	6:	0.7	0.3	6.0	0.7	0.7	1.2	2.8	9.0	0.8	=:	6.0	0.5	0.5	0.8	=	8.0	6.0	0.	6.0	6.0	9.0	0.7	0:	0.8	9.0	9:	6.0	0.7	3.0	4.0
$P_2O_5$	2.0	1.7	3.0	1.7	pu	2.8	2.7	pu	2.7	pu	2.8	pu	3.0	J.5	pu	2.2	3.0	pu	pu	2.7	2.9	pu	pu	2.6	2.8	2.8	pu	3.0	2.6	2.7	2.9	<u></u>
$SiO_2$	65.0	80.3	77.0	1.06	6.16	74.3	73.8	87.5	75.6	0.06	75.4	78.8	78.0	92.1	89.5	77.3	76.8	94.3	2.98	75.5	79.2	89.2	84.9	71.0	76.1	76.9	83.1	74.0	75.1	76.8	79.9	9.88
$Al_2O_3$	3.2	2.0	4.0	<u>~</u>	6.0	3.9	3.5	0.5	3.9	pu	3.9	2.1	4.0	2.5	.3	3.9	4.2	<u>-</u> .	1.2	4.	4.5	0.7	2.4	3.4	3.6	4.2	3.	3.9	3.7	4.0	4.3	2.2
MgO	pu	3.2	4.5	6.1	pu	3.9	3.3	pu	2.3	pu	3.7	3.9	4.6	6.5	pu	pu	3.6	pu	pu	3.4	4.3	pu	pu	3.–	3.5	3.8	4.7	3.4	4.3	3.7	3.–	5.7
Ь	30	_	2	$\sim$	4	2	9	_	&	6	0	=	12	<u>~</u>	4	12	91		<u>&amp;</u>	6	20	21	22	23	24	25	26	27	28	29	30	$\frac{8}{100}$
<b>×</b>	w02.6	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7	w02.7

$ZrO_2$	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.017	0.017	910.0	910.0	0.01	0.012	0.004	0.005	0.019	0.010	0.010	0.010	0.007	900'0	0.018	0.011	0.010	0.005	0.010	0.005	0.012	0.009	0.015
SrO	90000	0.005	0.005	90000	0.005	0.005	900.0	0.005	90000	0.003	0.095	0.108	0.098	0.181	0.188	0.019	0.138	0.106	0.153	0.180	0.112	0.196	0.018	0.109	0.116	0.193	0.056	0.186	0.330	0.185	0.118	0.104
Rb <sub>2</sub> O	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	0.002	0.002	0.002	0.00	0.00	pu	0.00	0.002	0.00	0.00	0.00	0.00	pu	0.002	0.00	0.00	0.003	0.00	0.002	0.00	0.00	0.001
$As_2O_3$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.012	pu	0.011	0.270	0.008	0.008	0.00	0.008	pu	9000	0.497	pu	0.008	pu	pu	9000	0.011	0.009	0.010	900'0
ZnO	0.002	0.00	0.00	0.00	pu	0.00	0.00	0.002	0.003	0.00	0.024	0.027	0.023	0.009	0.010	0.00	0.003	0.026	0.01	0.009	0.009	0.005	pu	0.027	0.010	0.008	900.0	0.007	0.004	900.0	0.010	0.017
CnO	0.004	0.005	0.002	0.002	0.002	0.003	0.007	9000	0.003	pu	0.004	0.004	0.007	0.003	pu	pu	pu	0.005	pu	pu	0.003	pu	0.00	0.003	pu	pu	pu	0.003	pu	0.003	0.00	0.007
$Fe_2O_3$	0.223	0.170	0.212	0.200	0.233	0.227	0.201	0.220	0.214	0.018	1.598	1.455	1.60	1.007	1.072	0.307	0.868	1.612	1.099	1.032	1.08	1.129	0.217	1.604	1.129	1.058	0.354	1.074	166.0	1.052	1.173	1.457
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.177	0.270	0.234	0.091	0.115	0.363	0.031	0.262	0.090	901.0	0.057	0.003	0.541	0.333	0.063	0	0.098	0.077	0.034	0.095	0.073	0.154
CaO	15.4	15.1	15.3	15.4	15.2	14.9	15.1	15.8	16.0	7.2	22.8	21.3	22.7	17.3	18.0	17.0	23.6	21.7	22.1	17.8	25.9	19.2	16.3	22.1	26.2	18.4	9:11	<u>8</u>	0.	18.5	26.3	22.0
K <sub>2</sub> O	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.7	4.	4.	4.	2.7	2.7	0.3	9:1	4.3	2.6	2.7	9.1	2.5	0.	4.3	9.	2.9	5.1	2.8	4.6	2.8	9.1	3.3
Ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	4.0	0.5	4.0	9.0	9.0	0.8	4.0	4.0	4.0	4.0	9.0	0.3	pu	0.5	9.4	9.4	0.7	4.0	9.0	4.0	0.4	0.5
SO3	0.7	0.7	0.8	0.8	0.8	1.5	0.7	0.8	0.8	6.0		0.8	2.0	6.0	6.0	0.7	1.2	0:	1.5	<u></u>	0.	0.7	<u>4</u> .	0.7	9.1	0.	pu	0.	pu	<u></u> 3	<u> </u>	0.8
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.5	2.7	2.9	1.5	<u>4</u> .	pu	pu	2.9	1.5	1.7	pu	<u> </u>	pu	3.0	<u></u>	7.	pu	<u>4</u> .	1.5	1.7	pu	2.3
SiO <sub>2</sub>	90.3	9.68	8.68	0.06	89.3	88.0	0.06	93.2	93.4	102.3	77.8	74.0	76.3	88.2	84.4	95.9	82.2	77.2	80.2	87.0	82.3	88.7	8.76	77.9	9.18	90.3	92.3	87.0	87.3	9.68	84.5	80.8
Al <sub>2</sub> O <sub>3</sub>	0.8	0.7	0.7	9.0	0.7	0.7	0.7	0.7	0.8	9.1	3.9	3.9	3.8	2.6	2.4	=	2.6	4.2	2.5	2.7	3.0	3.4	4.	4.2	2.9	2.8	6.0	2.4	4.2	3.0	3.0	3.4
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	4.2	3.9	3.6	3.6	5.2	4.5	pu	5.0	3.9	3.8	5.1	3.6	4.9	pu	3.6	3.7	4.7	2.7	4.8	7.1	5.2	4.0	3.2
Ь	_	2	$\sim$	4	2	9	_	$\infty$	6	_	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12	13	4	15	91		<u>&amp;</u>	61	20	21	22	23
>	w02.8	w02.8	w02.8	w02.8	w02.8	w02.8	w02.8	w02.8	w02.8	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9

	ω	0	6	0	2	ထ	6	_	4	_	9	9	_	_	9	9	9	9	$\sim$	_	0	_	$\infty$	2	_	4	6	4	4	0	_	0
ZZ	0.00	0.0	0.00	0.0	0.00	0.00	0.019	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.00	0.0	0.00	0.00	0.00	0.00	0.0	0.00	0.0	0.0	0.0	0.0	0.0
SPO	0.019	0.187	0.187	0.187	0.301	0.144	0.110	0.189	0.323	0.008	0.008	0.008	0.009	0.008	0.008	0.009	0.008	0.008	0.002	0.008	0.004	0.009	0.002	0.003	0.009	0.014	0.004	0.002	0.002	0.004	0.002	0.004
$Rb_2O$	0.00	0.00	0.00	0.00	0.00	0.00	0.002	0.00	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	0.001	pu	pu	0.00	pu	pu	0.00	pu	0.00
$As_2O_3$	0.565	0.007	0.010	0.013	0.015	0.008	0.010	pu	0.014	0.090	0.089	0.090	0.080	0.091	0.086	0.082	0.090	0.093	pu	0.086	pu	0.083	pu	pu	0.094	pu	pu	pu	pu	pu	pu	pu
ZnO	pu	0.010	0.008	0.015	0.002	0.00	0.025	0.010	0.002	0.00	pu	0.002	pu	pu	0.00	0.002	0.00	0.00	0.00	pu	pu	pu	pu	pu	pu	pu	0.00	0.00	0.00	0.00	pu	pu
CnO	pu	pu	0.004	0.002	pu	pu	0.005	0.00	pu	pu	pu	0.00	pu	pu	pu	0.002	pu	pu	pu	pu	pu	pu	pu	0.004	pu	pu	pu	0.00	pu	pu	pu	pu
$Fe_2O_3$	0.283	1.082	1.112	1.066	0.796	0.904	1.639	1.066	999.0	0.112	0.137	0.146	0.168	0.135	0.133	0.135	0.152	0.14	690.0	0.144	0.109	0.122	0.090	0.097	0.166	0.102	0.130	0.063	0.08	0.143	0.078	0.138
MnO	0.471	0.120	0.113	0.114	0.002	0.003	0.310	0.113	0.004	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	14.2	18.3	<u>8</u>	18.2	10.9	21.2	21.6	18.2	11.7	16.0	16.2	16.4	15.5	15.9	15.9	15.9	15.5	1.91	9.1	1.91	9.0	16.0	8.9	9.8	17.4	8.	7.6	7.9	7.6	7.6	7.8	7.7
K <sub>2</sub> O	0.7	2.8	2.8	2.9	3.8	2.1	4.2	2.8	3.7	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.0	pu	pu	0.5	pu	0.3	0.5	pu	pu	0.5	pu	9.0
Ū	pu	9.0	4.0	9.0	9.0	0.5	0.5	4.0	0.5	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	9.0	0:	1.2	<u></u>	0:	0.8	<u></u>	0:	0.3	0.7	0.7	0.7	9.0	9.0	0.7	9.0	9.0	0.7	9.4	0.7	0.2	0.7	0.3	0.2	0.7	pu	4.0	0.5	0.5	9.0	9.0	0.5
$P_2O_5$	pu	9:1	1.7	9:1		pu	3.1	<u>1.5</u>	<u>-</u> .	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	.5	9:1	9.1	3	9.1	1.7
SiO <sub>2</sub>	88.2	91.1	87.7	0.06	89.9	87.8	78.5	8.06	8.68	94.6	93.4	93.6	94.1	93.8	93.6	93.5	92.3	94.4	93.6	94.5	90.7	94.5	93.9	94.3	99.3	93.3	33.9	35.8	30.5	38.6	36.2	34.1
$Al_2O_3$	2.8	2.8	2.5	3.0	3.4	3.	4.	2.9	2.3	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.7	pu	pu	<u></u>	pu	<u>4</u> .	pu	pu	pu	pu	pu	pu
MgO	pu	5.5	4.6	5.6	9.9	5.0	3.4	5.0	6.7	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.9	pu	3.5	pu	2.8	3.5	pu	3.7	pu	pu	pu	pu	pu	pu
<u>م</u>	24	25	26	27	28	29	30	3	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	15	9		<u>∞</u>	_	7	$\sim$	4	2	9
>	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w02.9	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	w03	40w	w04	40w	40w	w04	40 <sub>w</sub>

$ZrO_2$	600.0	0.009	0.018	0.008	0.010	0.010	0.009	0.009	0.018	0.019	0.009	0.012	0.013	0.015	0.014	0.012	0.013	0.013	0.013	0.013	0.013	0.014	0.013	0.011	0.012	0.013	0.014	0.012	0.012	0.011	0.012	0.010
SrO	0.004	0.004	0.002	0.004	0.004	0.004	0.005	0.004	0.002	0.003	0.004	0.008	0.008	0.008	0.008	0.009	0.008	0.008	0.008	0.008	0.009	0.008	0.007	0.008	0.002	0.008	0.008	0.008	0.008	0.009	0.008	0.007
Rb <sub>2</sub> O	0.001	0.00	pu	0.00	0.00	0.00	0.00	0.00	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	pu	pu	pu	pu	0.00
As <sub>2</sub> O <sub>3</sub>	pu	pu	pu	pu	pu	pu	pu	pu	900.0	pu	pu	0.088	0.082	0.089	0.090	0.085	0.079	980'0	0.088	0.084	0.087	0.081	0.083	0.088	pu	0.084	0.082	0.084	0.085	980'0	0.093	pu
ZnO	0.001	pu	0.00	pu	0.00	pu	0.00	pu	0.002	0.00	0.00	0.00	pu	0.00	pu	0.003	pu	pu	pu	0.00	pu	0.003	0.00	0.00	pu	pu	0.002	pu	0.00	pu	0.001	pu
CuO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.003	pu	pu	0.001	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.135	0.127	0.08	0.152	0.138	0.175	0.158	0.132	0.084	980.0	0.146	0.126	0.121	0.122	0.128	0.129	0.133	0.139	0.135	0.132	0.133	0.128	0.144	0.122	0.149	0.135	0.122	0.137	0.122	0.125	0.122	0.144
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	7.8	7.6	7.4	7.9	8.0	7.4	8.0	<u>~</u> .	7.8	7.6	<u>~</u> .	14.5	13.4	13.8	13.7	14.2	14.0	13.9	14.0	14.0	14.3	13.8	13.7	14.3	5.5	13.9	14.2	13.9	14.0	14.7	14.5	12.2
K <sub>2</sub> O	4.0	4.0	pu	4.0	0.5	4.0	0.5	0.5	pu	pu	0.5	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.3	pu	pu	pu	pu	pu	pu	0.5
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO	9.0	4.0	9.0	9.0	9.0	4.0	4.0	0.5	6.0	=	0.5	0.7	9.0	0.7	9.0	9.0	9.0	9.0	0.7	0.8	0.7	0.7	0.7	0.7	0.7	9.0	0.7	9.0	0.7	0.7	0.7	0.7
P <sub>2</sub> O <sub>5</sub>	1.5	<u>.</u> 5	<u>~</u>	9.1	<u>8.</u>	9:1	<u>.</u>	<u>.</u>	2.0	2.2	1.7	9.1	6:	2.0	6:	<u>~</u>	1.7	9.1	<u>8</u> .	<u>~</u>	<u>~</u>	1.7	<u>8</u> .	9:1	6:	.5	<u>8</u> .	9.1	9.1	<u></u>	1.7	9.1
SiO <sub>2</sub>	41.8	35.0	34.9	39.8	33.6	32.6	41.5	44.5	30.6	22.2	37.8	42.6	29.1	30.6	34.4	39.5	37.0	38.4	36.4	37.8	36.2	35.0	35.3	44.6	31.6	38.9	35.4	39.8	45.0	52.5	38.8	40.5
Al <sub>2</sub> O <sub>3</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
OgM	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
<u>م</u>	7	∞	6	0	=	12	<u> </u>	4	12	91		8	61	20	21	22	23	24	25	26	27	28	29	30	<u>~</u>	32	33	34	35	36	37	38
>	40w	40 <sub>w</sub>	w04	40w	w04	40 <sub>w</sub>	w04	40w	w04	40 <sub>w</sub>	w04	40 <sub>w</sub>	w04	40 <sub>w</sub>	40 <sub>w</sub>	w04	w04	w04	w04	w04	w04	40w	40w	40 <sub>w</sub>	40 <sub>w</sub>	40w						

$ZrO_2$	0.010	0.014	0.013	0.012	0.01	0.014	0.014	0.013	0.013	0.013	0.013	0.017	0.015	0.013	0.014	0.013	0.01	0.012	0.013	0.013	0.014	0.015	0.014	0.013	0.013	0.013	0.012	0.012	0.012	0.013	0.013	0.012
SrO	0.007	0.008	0.009	0.007	0.003	0.008	0.008	0.008	0.008	0.009	0.002	900'0	0.008	0.009	0.008	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.008	0.008	0.008	0.009	0.008
$Rb_2O$	0.001	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$As_2O_3$	pu	0.090	0.082	0.115	pu	0.091	0.091	0.094	0.091	0.089	pu	pu	0.085	0.093	0.080	0.082	0.088	0.084	0.084	0.088	0.084	980'0	0.090	0.082	0.084	0.089	0.090	0.092	980'0	0.083	0.085	0.084
ZnO	pu	pu	0.002	0.003	pu	0.00	pu	0.00	pu	pu	pu	pu	0.002	pu	pu	pu	0.00	0.002	pu	pu	pu	pu	pu	pu	0.003	0.00	0.00	0.002	0.00	pu	pu	0.001
CnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	0.002
$Fe_2O_3$	0.161	0.129	0.126	0.304	0.147	0.125	0.159	0.121	0.123	0.118	0.074	0.119	0.119	0.143	0.146	0.139	0.120	0.127	0.121	0.148	0.109	0.132	0.140	0.129	0.143	0.140	0.136	0.136	0.135	0.150	0.132	0.130
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	12.0	14.2	14.2	12.2	7.0	14.0	14.2	14.3	14.4	13.9	7.5	5.0	13.5	15.5	13.9	- - -	14.6	14.3	13.9	14.3	14.4	14.0	13.9	14.3	13.9	13.8	- - -	13.9	14.2	13.8	14.5	14.0
$K_2O$	0.5	pu	pu	4.0	0.2	pu	pu	pu	pu	pu	pu	0.2	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
ט	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	0.5	0.7	9.0	0:	0.5	9.0	0.7	0.7	9.0	9.0	0.5	9.0	0.7	0.7	9.0	0.7	0.7	0.7	0.7	0.7	9.0	0.7	9.0	0.7	0.7	9.0	0.7	6.0	0.7	9.0	9.0	9.0
$P_2O_5$	9.1	6:1	<u>1</u> .5	6:1	<u>~</u>	6:1	2.1	<u>8</u> .	9.1	<u>~</u>	9.1	1.7	2.0	1.7	1.7	1.7	<u> </u>	9.1	1.7	1.7	2.0	2.0	1.7	1.7	9.1	1.7	1.5	<u>~</u>	1.5	1.7	8.	7.
SiO <sub>2</sub>	41.3	35.2	37.9	37.4	38.1	31.8	29.7	37.4	42.1	31.6	42.2	36.2	31.3	43.2	36.1	38.0	46.9	43.1	35.0	40.7	32.7	32.4	35.3	40.8	38.8	38.9	40.6	30.8	43.1	33.3	38.4	39.1
$Al_2O_3$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ь	39	40	4	42	43	4	45	46	47	48	_	2	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	15	9	17	<u>∞</u>	6	20	21	22
<b>×</b>	40w	40 <sub>w</sub>	w04	40w	w04	40 <sub>w</sub>	40w	40w	40w	40w	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05

$ZrO_2$	0.013	0.017	0.017	0.013	0.014	0.013	0.015	0.013	0.014	0.013	0.012	0.014	0.012	0.013	0.021	0.020	0.019	0.022	0.019	910.0	0.019	910.0	0.019	0.021	910.0	0.011	0.019	0.020	0.019	0.019	0.020	0.014
SrO	0.008	900.0	900.0	0.008	0.008	0.008	0.009	0.009	0.008	0.009	0.00	0.008	0.008	0.00	0.007	900.0	900.0	900'0	900'0	900'0	0.007	900'0	0.007	900'0	0.007	0.00	0.007	900'0	0.007	900'0	900'0	0.008
$Rb_2O$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	0.002	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	pu	pu	pu	pu
As <sub>2</sub> O <sub>3</sub>	0.080	pu	pu	0.000	0.092	0.088	0.094	0.092	0.087	0.091	pu	0.000	0.086	pu	0.009	0.010	0.008	0.010	900'0	pu	0.034	pu	0.033	0.037	pu	pu	0.033	0.029	0.033	0.032	0.035	0.095
ZnO	0.001	0.00	pu	0.002	0.002	pu	0.002	pu	pu	pu	0.002	pu	pu	0.002	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	pu	pu	0.001	0.00
CnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.003	pu	pu	0.001	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.161	0.	0.119	0.132	0.134	0.132	0.127	0.116	0.149	0.157	0.151	0.135	0.129	0.155	0.112	0.101	0.115	0.118	901.0	0.1	0.128	0.110	0.134	0.110	0.117	0.137	0.110	0.123	0.098	0.117	901.0	0.135
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	1.4	2.0	4.9	14.2	13.9	14.2	14.6	14.5	14.6	14.3	5.7	15.1	<u>4.</u>	5.6	16.4	14.4	15.8	14.8	15.1	5.3	16.8	5.1	15.8	15.1	5.3	5.8	15.0	15.0	15.1	15.2	15.3	13.6
K <sub>2</sub> O	pu	0.2	0.2	pu	pu	pu	pu	pu	pu	pu	0.3	pu	pu	0.3	pu	pu	pu	pu	pu	0.2	pu	0.2	pu	pu	0.2	0.3	pu	pu	pu	pu	pu	pu
ō	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	0.7	0.8	9.0	0.7	0.7	0.7	0.7	9.0	0.8	0.7	9.0	0.7	0.7	0.7	3	1.2	<u> </u>	1.2	<u> </u>	0.8	<u>-</u> .	0.8	<u> </u>	1.2	0.7	9.0	=	<u></u>	1.2	=	<u></u>	0.8
$P_2O_5$	4.	9.	1.7	9.1	<u>~</u>	1.7	2.1	<u>8</u> .	2.0	1.7	6.	2.0	1.7	6:	1.2	<u>7.</u>	0.	9.	=:	1.2	pu	<u>7.</u>	1.2	9.	9.	7.	1.2	<u>4</u> .	1.2	€.	<u>4</u> .	2.1
SiO <sub>2</sub>	43.4	36.9	29.9	44.9	35.3	38.1	34.0	36.5	36.0	36.1	29.2	37.4	39.1	30.5	53.1	40.5	55.9	40.0	1.95	51.6	70.7	45.8	9.99	42.5	46.7	4.8	47.7	51.2	54.3	49.3	52.5	31.6
Al <sub>2</sub> O <sub>3</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ь	23	24	25	26	27	28	29	30	$\frac{1}{2}$	32	33	34	35	36	_	2	$\sim$	4	2	9	7	∞	6	0	=	12	13	4	15	91	1	<u>&amp;</u>
>	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	w05	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w

$ZrO_2$	910.0	0.013	0.013	0.014	0.012	0.015	0.013	0.012	0.01	0.013	0.01	0.014	0.009	0.015	0.012	0.013	0.01	0.011	0.021	0.017	0.020	0.015	910.0	910.0	0.018	0.014	910.0	910.0	0.013	0.01	0.015	0.015
S <sub>O</sub>	0.008	0.008	0.008	0.008	0.008	0.009	0.009	0.008	0.00	0.009	0.007	0.009	0.007	0.008	0.008	0.008	0.00	0.004	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.003	0.002	0.002
$Rb_2O$	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	0.00	pu	0.00	pu	pu	pu	0.002	0.00	pu	pu	pu	pu	pu	pu	pu							
As <sub>2</sub> O <sub>3</sub>	0.084	0.085	0.088	0.087	0.086	0.095	0.091	0.085	pu	0.093	pu	0.092	pu	0.087	980'0	0.087	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
ZuO	0.001	pu	pu	0.00	pu	pu	pu	pu	0.003	0.00	pu	pu	pu	0.003	pu	pu	0.00	pu	pu	pu	0.00	0.00	pu	pu	0.003	pu	pu	0.00	pu	1.105	0.00	pu
CnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.142	0.137	0.129	0.137	0.135	0.144	0.150	0.133	0.143	0.136	0.103	0.143	0.101	0.134	0.129	0.136	0.142	0.137	0.094	0.000	0.087	0.074	0.082	0.080	0.071	0.072	0.088	0.101	0.000	0.021	0.083	0.082
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	13.9	<u>4.</u> 	<u>4.</u>	13.6	14.5	14.8	14.8	14.5	5.7	15.1	6.9	14.3	7.4	14.0	14.6	<u>4.</u> 	5.7	7.9	7.5	8.0	7.9	7.7	7.9	7.8	7.8	7.8	7.9	8.0	— —	9.8	7.6	7.8
K <sub>2</sub> O	pu	pu	pu	pu	pu	pu	pu	pu	0.3	pu	4.0	р	0.5	pu	pu	pu	0.3	0.5	pu	pu	pu	pu	4.0	pu	pu							
ō	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.3	pu	pu
SO	0.7	0.7	0.8	9.0	0.7	0.7	0.7	0.7	9.0	0.7	0.8	0.7	9.0	0.7	0.7	0.7	9.0	0.7	9.0	9.0	9.0	0.7	9.0	9.0	9.0	0.7	9.0	9.0	9.0	0.8	0.5	9.0
P <sub>2</sub> O <sub>5</sub>	2.2	<u>~</u> .	<u>~</u>	<u>8</u> .	<u>~</u> .	2.2	<u>8</u> .	1.5	<u>-</u> .	9:1	<u>8</u> .	6:1	1.5	2.1	7.	2.0	<u>8</u> .	2.1	2.1	1.7	6:1	1.7	1.7	9.1	2.1	<u>8</u> .	<u>8</u> .	6:1	<u>-</u> .	6:1	1.7	9.1
SiO <sub>2</sub>	28.6	36.7	36.6	29.6	38.9	34.4	41.0	43.7	44.6	46.2	33.5	36.9	42.5	31.7	50.3	33.0	37.2	30.5	27.4	36.0	35.2	36.7	37.9	40.1	28.8	37.7	36.4	33.1	48.6	33.8	36.2	40.9
$Al_2O_3$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
۵	61	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34	35	36	37	38	39	4	4	42	43	44	45	46	47	48	49	20
>	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w	90w

$ZrO_2$	0.015	0.014	0.010	0.014	0.013	0.013	0.011	0.013	0.013	0.013	0.010	0.013	0.017	0.013	0.010	0.012	0.012	0.015	910.0	0.012	0.005	0.005	0.004	0.003	900'0	0.008	0.003	0.012	0.007	0.013	0.003	0.003
S <sub>O</sub>	0.002	0.008	0.002	0.009	0.008	0.008	910.0	0.008	0.009	0.008	0.002	0.008	0.002	0.008	0.002	0.008	0.008	0.371	0.007	0.008	0.313	0.003	0.322	0.002	0.314	0.313	0.326	900.0	0.320	0.007	900'0	0.015
$Rb_2O$	pu	pu	0.002	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	pu	0.002	pu	pu	0.00	pu	pu	0.00	0.00	0.00	pu	0.00	0.00	0.00	0.001	0.00	pu	pu	pu
As <sub>2</sub> O <sub>3</sub>	pu	0.089	pu	0.094	0.090	0.091	0.277	960'0	0.085	980'0	pu	0.090	pu	0.084	pu	980.0	0.087	0.020	pu	0.083	0.005	pu	900.0	pu	900.0	0.014	0.009	pu	0.007	pu	0.068	pu
ZnO	0.001	0.00	pu	pu	pu	0.003	pu	0.002	pu	0.003	0.00	pu	0.00	pu	pu	pu	pu	0.002	pu	0.00	0.004	pu	0.005	pu	0.003	0.004	900'0	pu	0.004	pu	pu	pu
CnO	pu	pu	pu	pu	pu	pu	0.004	pu	0.002	pu	pu	pu	pu	pu	pu	pu	pu	0.004	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Fe <sub>2</sub> O <sub>3</sub>	0.088	0.137	0.145	0.116	0.128	0.104	0.197	0.112	0.102	0.107	0.164	0.129	0.093	0.127	0.116	0.142	0.124	0.447	0.127	0.125	0.870	0.081	0.844	0.243	0.864	0.829	0.900	0.105	0.910	0.110	0.215	0.220
MnO	pu	pu	pu	pu	pu	pu	0.370	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	0.013	pu	0.013	pu	0.025	900'0	pu	pu	pu	pu	pu	pu
CaO	8.2	14.8	5.4	14.8	14.3	14.2	13.1	14.7	4.4	<u>4.</u> 	5.5	14.7	—. —.	14.5	5.6	14.2	14.2	10.9	5.2	14.5	9.01	9.0	1.5	9.1	0.	=	8	5.7	3	5.8	16.3	16.7
K <sub>2</sub> O	pu	pu	0.3	pu	pu	pu	pu	pu	pu	pu	0.3	pu	pu	pu	0.3	pu	pu	2.8	0.2	pu	3.8	0.5	4.0	pu	3.8	3.8	4.0	0.2	3.8	0.2	pu	0.0
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.5	pu	pu	9.0	pu	9.0	pu	9.0	9.0	9.0	pu	9.0	pu	pu	pu
SO	0.5	0.7	0.5	0.7	0.7	9.0	6.0	0.7	9.0	6.0	9.0	0.7	9.0	0.7	9.0	9.0	9.0	9.0	0.	0.8	pu	0.3	pu	9.0	pu	pu	pu	0.8	pu	0.8	1.2	0.9
P <sub>2</sub> O <sub>5</sub>	1.7	<u>~</u>	1.7	<u>~</u>	<u>~</u>	<u>~</u>	1.7	9.1	1.7	<u>~</u>	1.7	1.7	1.7	<u>7.</u>	9:	1.7	1.7	2.8	<u>4.</u>	<u>~</u>	<u>~</u>	pu	1.7	pu	<u>8.</u>	1.7	<u>8.</u>	pu	<u>~</u>	pu	pu	pu
SiO <sub>2</sub>	4.14	40.5	38.0	37.0	39.8	37.2	45.3	45.0	40.4	39.8	37.5	42.5	39.7	44.2	39.5	0.14	39.3	40.9	47.1	40.8	94.0	95.5	92.8	92.4	94.5	94.3	9.76	8.16	1.96	91.5	92.1	9.96
Al <sub>2</sub> O <sub>3</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.7	1.2	2.7	9.0	2.6	2.8	2.8	=	2.8	<u></u>	6.0	0.8
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	6.3	3.8	8.9	pu	6.7	6.5	9.9	3.5	l.9	3.5	pu	pu
۵	51	52	53	54	55	26	27	28	26	09	19	62	63	64	65	99	<i>L</i> 9	89	69	70	_	7	$\sim$	4	2	9	7	∞	6	0	=	12
>	90m	90w	90m	90w	90m	90m	90m	90m	90m	90m	90m	90m	90m	90m	90w	90m	90m	90m	90m	90m	w07	w07	w07	w07	w07	w07	w07	w07	w07	w07	w07	w07

$ZrO_2$	910.0	0.00	0.003	900.0	900.0	0.003	0.010	0.010	0.005	0.010	0.01	0.01	0.007	0.004	0.010	0.01	0.01	0.010	0.010	0.01	0.01	0.012	0.010	0.005	0.012	0.010	0.005	0.012	0.005	0.003	900.0	0.002
SrO	0.003	0.009	0.008	90000	0.017	0.002	0.002	0.002	0.004	0.002	0.002	0.002	0.003	0.004	0.002	0.002	0.002	0.002	0.002	0.003	0.002	0.002	0.002	0.004	0.002	0.002	0.004	900.0	0.00	0.01	0.004	900'0
Rb <sub>2</sub> O	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	0.00	pu	0.002	0.00	0.00	0.001
As <sub>2</sub> O <sub>3</sub>	pu	0.259	0.043	pu	0.271	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.007	pu	1.168
ZnO	0.001	pu	0.00	0.002	0.002	pu	0.00	pu	pu	pu	pu	pu	0.00	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	0.00	0.00	pu	pu	pu	0.003	pu	0.002
Ono	pu	pu	pu	pu	0.002	0.002	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$F_2O_3$	0.111	0.209	0.193	0.237	0.205	0.227	0.087	990.0	0.137	0.090	0.073	0.092	0.085	0.144	0.081	960'0	980'0	0.094	0.082	0.089	0.074	0.099	0.088	0.153	0.089	960'0	0.148	0.109	0.152	0.174	0.078	0.335
MnO	pu	pu	pu	pu	0.406	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.427	pu	pu
CaO	9.4	16.2	15.5	15.5	15.3	9.2	8.9	8.5	8.9	8.9	9.0	9.1	9.3	9.1	8.7	9.1	8.8	8.8	8.7	8.9	8.7	9.1	8.9	8.8	8.8	8.9	8.9	5.6	6.4	0.91	8.8	14.5
K,O	0.2	0.0	0.0	0.0	0.0	pu	pu	pu	9.0	pu	pu	pu	0.0	9.0	pu	pu	pu	pu	pu	pu	pu	pu	pu	9.0	pu	pu	0.5	0.2	0.3	0.3	0.5	0.5
Ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	pu	<u>4</u> .	0.8	0.8	6.0	0.3	9.0	6.0	pu	9.0	0.5	0.5	pu	pu	9.0	4.0	0.5	9.0	0.5	4.0	0.5	0.5	0.5	pu	4.0	0.5	0.2	0.8	0.5	0:	pu	6.0
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	94.6	92.2	94.5	9.06	6.86	94.6	6.96	95.8	94.7	0.96	94.2	94.3	95.5	2.96	94.9	94.8	92.3	0.96	95.0	94.5	6.96	9.96	94.1	93.9	94.1	96.2	94.2	93.5	94.2	95.2	93.9	93.2
$Al_2O_3$	0.8	0.8	0.7	0.8	6.0	pu	pu	pu	1.7	pu	pu	pu	pu	9:1	pu	pu	pu	pu	pu	pu	pu	pu	pu	7.	pu	pu	1.5	1.2	2.2	0.8	1.2	6.1
MgO	4.0	pu	pu	pu	pu	pu	3.3	3.0	2.9	3.0	3.2	3.2	<u>~</u> .	3.2	3.0	3.5	3.	3.2	3.4	2.9	3.2	3.5	3.	3.0	3.0	3.7	3.2	3.7	4.3	pu	3.8	pu
Ь	13	4	12	9		<u>&amp;</u>	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	<u>4</u>	15	9		<u>∞</u>	6	20	21	22	23	24	25	26
>	w07	w07	w07	w07	w07	w07	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m	60m

 $\overline{\infty}$ 

$\overline{\text{ZrO}}_{2}$	0.003	0.003	0.012	0.004	900'0	0.002	0.003	0.002	0.00	0.002	0.003	0.010	0.002	0.005	900'0	900'0	0.005	0.005	0.003	0.002	0.002	0.002	0.005	0.002	0.002	0.005	0.005	0.002	0.005	0.002	0.004	900'0
Š	0.003	0.002	900'0	900'0	0.002	910.0	910.0	0.015	910.0	910.0	910.0	900'0	910.0	900'0	0.00	900'0	0.007	0.007	910.0	910.0	910.0	910.0	0.002	910.0	0.017	900'0	0.002	0.017	900'0	0.018	0.362	0.013
$R_2O$	pu	0.00	pu	0.00	0.002	pu	0.00	0.002	0.00	0.00	0.00	pu	pu	pu	pu	0.002	pu	pu	0.00	0.002	pu	pu	pu	0.00	pu							
$As_2O_3$	pu	pu	pu	pu	pu	pu	pu	900.0	0.005	0.005	pu	0.392	pu	pu	pu	pu	pu	pu	pu	0.005	pu	pu	pu	pu	pu	pu	pu	pu	pu	900.0	900'0	0.233
ZnO	1.142	pu	pu	pu	0.002	pu	pu	pu	pu	pu	pu	0.003	pu	0.00	0.00	pu	0.00	0.003	pu	pu	pu	pu	0.001	pu	pu	0.00	0.00	pu	0.00	pu	0.001	pu
9	0.003	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.005	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.001	pu	0.002	pu	pu	pu	pu	pu	pu
$F_2O_3$	0.020	0.080	0.104	0.132	0.155	0.174	0.170	0.173	0.185	0.161	0.180	0.231	0.154	0.192	0.135	0.333	0.198	0.174	0.168	0.166	0.174	0.158	0.153	0.180	0.164	0.206	0.155	0.188	0.360	0.187	0.610	0.219
Ω O	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.019	0.044
Og Og	8.6	9.1	2.8	13.8	9.9	15.6	15.8	15.6	15.7	15.8	15.5	13.8	15.9	13.5	6.4	15.0	13.6	13.6	16.5	15.9	15.8	15.7	l.9	15.4	16.4	13.9	6.3	16.5	14.5	0.91	6.11	12.7
ς 20	0.5	0.2	0.2	9.0	4.0	pu	9.0	0.3	0.3	9.0	9.0	pu	pu	pu	pu	9.4	pu	pu	9.0	4.0	pu	0.3	pu	4.	pu							
Ū	0.5	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	9.0	pu
လွိ	6.0	0.2	0.7	9.0	0.5	0.	<u></u>	=:		0.	0.	<u>-</u> .	0.	0.7	9.0	0.	0.8	0.7	1.2	0.	0.	0.	0.2	=	=	0.7	0.5	1.2	0.8	=:	pu	6.0
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	8.	pu
SiO <sub>2</sub>	94.6	97.6	94.8	97.3	95.1	92.4	94.8	93.7	96.2	97.2	95.8	91.2	96.5	96.2	94.1	7.76	98.1	90.4	6.66	6.76	1.66	6.96	97.6	95.5	99.3	96.2	0.16	99.5	0.96	95.0	95.7	95.3
$A_2O_3$	pu	pu	<u>4</u> .	<u>8</u> .	2.2	pu	0.8	0.7	0.5	0.8	pu	0.5	0.8	6:1	2.1	3.	2.1	<u>8</u> .	6.0	0.7	0.8	0.7	2.0	0.7	0.8	2.0	2.1	6.0	2.8	9.0	3.4	0.5
Q Σ	pu	4.0	3.9	pu	4.4	pu	4.6	pu	pu	pu	pu	pu	pu	pu	4.3	pu	pu	pu	3.8	pu	pu	pu	7.7	pu								
ட	27	28	29	30	3	_	2	$\sim$	4	2	9	_	&	6	0	=	12	<u>~</u>	4	15	9		<u>&amp;</u>	6	20	21	22	23	24	25	26	27
≯	60m	60m	60m	60m	60m	0   	<u>0</u>   ≫	<u>0</u>   ≫	<u>0</u>   ≫	0   	0   	0   	<u>0</u>   ≫	0   	0   	<u>                                     </u>	0   	0 ×														

$ZrO_2$	0.002	900.0	0.002	0.002	0.005	0.002	0.002	0.002	0.005	0.004	0.002	0.003	0.002	0.002	0.003	0.002	0.002	0.004	900.0	0.004	0.002	0.002	0.002	0.002	0.002	0.002	0.00	0.002	0.002	0.002	0.003	0.002
SrO	910.0	0.015	0.017	910.0	0.014	910.0	0.013	0.007	0.350	0.007	0.007	910.0	900'0	0.007	900'0	900'0	910.0	0.351	0.361	0.007	910.0	0.017	0.017	0.017	910.0	910.0	910.0	910.0	0.015	910.0	0.017	0.017
$Rb_2O$	pu	pu	pu	pu	pu	pu	pu	pu	0.00	0.00	pu	pu	pu	pu	pu	pu	pu	0.002	0.00	0.00	pu	pu										
$As_2O_3$	pu	0.221	pu	pu	0.233	pu	0.065	0.009	0.007	900'0	0.008	pu	0.005	pu	pu	pu	pu	900'0	0.0	900.0	pu	pu	pu	pu	0.005	pu	pu	pu	pu	0.005	900'0	9000
ZnO	pu	pu	pu	pu	0.00	pu	pu	0.00	0.00	0.002	0.002	pu	0.002	pu	pu	0.002	pu	pu	pu	pu	pu	0.00	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu
CnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.183	0.228	0.182	0.186	0.188	0.198	0.178	0.264	0.639	0.247	0.260	0.188	0.241	0.174	0.161	0.146	0.152	0.604	0.623	0.286	0.172	0.187	0.180	0.167	0.182	0.150	0.182	0.218	0.202	0.186	0.198	0.167
MnO	pu	0.043	pu	pu	0.025	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	14.9	14.0	14.9	15.3	13.3	14.7	4.	15.5	9.11	15.2	15.0	16.1	15.3	16.4	15.8	15.7	15.5	9.1	8. 	15.9	15.8	15.3	0.91	16.3	15.6	15.1	15.3	0.91	15.9	15.3	0.91	9.91
K <sub>2</sub> O	pu	pu	pu	pu	pu	0.0	0.2	9.0	4.0	9.0	0.5	pu	9.0	0.2	0.2	0.0	pu	4.0	4.0	4.0	pu	0.0	pu	pu	pu	pu						
ū	pu	pu	pu	pu	pu	pu	pu	pu	9.0	pu	pu	pu	pu	pu	pu	pu	pu	9.0	9.0	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3		0.7	1.2	1.2	6.0	=:	6.0	=:	pu	1.5	0.	1.2	=:	<u></u>	1.2	<u></u>	=:	pu	9.0	<u></u>	0.1	1.2	=	Ξ	=	Ξ	1.2	Ξ	=	0:	=	1.2
$P_2O_5$	pu	pu	pu	pu	pu	pu	pu	pu	6:	pu	pu	pu	pu	pu	pu	pu	pu	2.0	6:	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	8.96	95.3	94.1	95.7	9.96	94.4	96.4	98.2	95.2	98.3	96.4	94.8	97.3	98.0	92.8	97.0	95.2	97.0	95.7	99.5	95.5	8.86	96.3	6'86	91.5	6.96	94.0	95.0	95.2	92.7	9.76	96.2
$Al_2O_3$	0.8	0.7	0.7	6.0	9.0	0.7	0.8	6.0	3.5	3.4	9.0	0.7	0.7	0.7	pu	0.7	0.7	3.7	3.4	2.9	9.0	6.0	pu	0.8	0.5	0.8	0.7	0.7	9.0	0.7	0.8	0.7
MgO	pu	pu	pu	pu	pu	pu	pu	pu	7.4	pu	pu	pu	pu	pu	pu	pu	pu	7.9	7.7	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ь	28	29	30	3	32	33	34	35	36	37	38	39	4	4	42	43	44	45	46	47	_	7	$\sim$	4	2	9	_	$\infty$	6	0	=	12
>	0 w	0  %	0   	0	<u>0</u>	0  %	<u>0</u>   ×	<u>0</u>	<u>0</u>	0	<u>0</u>	<u>0</u>	<u>0</u>	0   	0  %	0   %	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u> ×	<u>-</u>	<u>_</u>	<u>_</u>	<u>_</u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u>_</u>	<u> </u>	<u>_</u>	=

2	)2	)2	)3	)2	)2	)2	_	)3	)2	)3	$\sim$	7	)2	)2	4	_	)2	)2	)2	_	)2	)2	_	)2	)2	)2	)3	)2	)2	)2	)2	)2
Zr	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.002
SrO	0.017	0.017	0.009	910.0	0.017	0.017	0.016	0.017	0.013	910.0	0.002	0.002	910.0	910.0	0.007	910.0	910.0	910.0	910.0	910.0	0.015	910.0	0.015	910.0	910.0	910.0	910.0	0.015	910.0	0.00	910.0	0.016
$Rb_2O$	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu							
As <sub>2</sub> O <sub>3</sub>	pu	0.007	099.0	0.007	pu	pu	pu	pu	0.067	pu	pu	pu	0.007	pu	pu	900.0	pu	pu	pu	pu	0.007	pu	0.005	0.005	pu	pu						
ZnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu						
CuO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.191	0.180	0.215	0.173	0.178	0.180	0.157	0.192	0.148	0.175	0.074	0.08	0.167	0.160	0.151	0.163	0.162	0.178	0.171	0.182	0.161	0.164	0.166	0.161	0.174	0.173	0.192	0.164	0.155	0.074	0.169	0.185
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	16.0	16.4	13.8	15.7	15.9	16.5	15.7	15.5	14.8	16.0	8.2	8.6	15.1	15.6	13.0	15.5	15.3	15.7	15.5	15.5	15.3	15.3	15.3	15.3	15.9	15.3	15.7	15.8	15.7	9.2	15.6	15.5
K <sub>2</sub> O	pu	pu	0.5	pu	pu	0.0	pu	pu	0.0	0.0	pu	pu	pu	pu	0.5	pu	0.0	0.1	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.2	pu	pu
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	Γ'.	1.2	0:	=	Ξ:	1.2	0.	Ξ:	0.	=	pu	pu	Ξ.	1.2	0.3	Ξ:	Ξ:	1.2	1.2	0.	0.	6.0	0.	0.	6.0	0:	6.0	0.	0.	0.3	6.0	0.
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	96.5	97.4	1.86	97.0	95.9	98.0	6.96	95.9	8.96	95.5	93.5	94.8	88.4	96.4	89.9	95.1	91.3	94.0	95.4	97.4	93.4	94.3	2.96	94.7	9.76	96.4	95.2	98.3	95.4	94.1	92.6	8.96
$Al_2O_3$	0.7	9.0	6:1	6.0	0.7	0.7	9.0	0.7	0.7	9.0	=	=	pu	6.0	<u>-</u> .	9.0	9.0	pu	0.8	9.0	9.0	0.7	0.7	0.5	9.0	0.8	9.0	0.8	0.8	9.0	9.0	0.7
OgM	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	3.5	4.0	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	4.2	pu	pu
а.	13	4	15	91		<u>&amp;</u>	61	70	21	22	23	24	25	26	27	28	29	30	3	32	33	34	35	36	37	38	39	9	4	42	43	4
≯		<u> </u>	<u>-</u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	_ >	<u> </u>	_ >						

$ZrO_2$	0.005	0.002	0.002	0.00	0.002	0.009	0.008	0.004	0.012	0.012	0.002	0.012	0.005	0.002	0.012	0.005	0.005	0.005	0.005	0.015	0.005	0.005	0.004	0.003	0.002	0.002	0.002	900.0	0.010	900.0	900'0	900'0
S.O	0.008	0.015	0.016	0.016	0.015	0.015	0.014	0.01	0.007	0.007	0.021	900.0	0.007	0.009	900.0	0.008	0.010	0.010	0.013	0.073	0.010	0.010	0.014	0.053	0.016	0.015	0.016	0.008	0.015	0.00	0.015	0.007
$Rb_2O$	0.001	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	0.002	pu	0.00
As <sub>2</sub> O <sub>3</sub>	pu	pu	pu	pu	0	pu	pu	pu	pu	pu	pu	pu	pu	0.048	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.118	901.0	0.121	pu	pu	pu	0.347	pu
ZnO	0.003	pu	pu	pu	0.003	0.004	0.002	0.003	pu	pu	pu	pu	900'0	pu	pu	0.003	0.002	0.002	0.00	0.029	0.00	0.003	900'0	pu	0.002	0.002	0.00	pu	0.002	0.003	pu	0.00
Ono	0.002	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.256	0.192	0.148	0.164	0.156	0.231	0.244	0.188	0.121	0.132	0.147	0.095	0.153	0.212	0.117	0.165	0.187	0.191	0.193	0.539	0.193	0.180	0.133	0.356	0.187	0.189	0.171	0.094	0.351	0.153	0.176	0.101
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	13.8	16.0	1.9	15.2	15.0	17.9	17.3	16.3	5.7	5.7	15.6	5.8	4.	16.2	5.8	4.	15.3	15.6	15.5	19.7	15.9	15.4	15.4	<u>3</u> .	15.3	14.6	15.5	8.4	15.7	6.5	18.3	8.2
K <sub>2</sub> O	9.0	pu	pu	pu	0.2	0.0	pu	0.2	0.2	0.2	0.0	0.2	0.5	pu	0.2	0.5	0.2	0.2	0.2	0.8	0.3	0.2	0.2	0.5	0.3	0.2	0.2	9.0	0.2	4.0	pu	0.5
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.5	pu	pu	pu	0.5	pu							
SO	9.0	1.2	1.2	0:	6.0	0.7	0.7	9.0	0.8	0.8	=:	0.8	9.0	1.2	0.8	0.5	9.0	0.5	0.8	0.3	0.5	9.0	0.5	0.2	6.0	6.0	6.0	0.2	0.3	0.5	0.	pu
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	94.5	97.8	98.0	94.5	92.6	1.68	93.0	6.96	95.0	94.6	96.4	93.3	6'86	95.2	96.5	98.4	95.2	97.5	1.86	8.06	95.9	94.1	9.66	96.5	98.5	97.6	1.66	94.8	98.4	95.8	95.4	94.5
$Al_2O_3$	<u>8.</u>	9.0	0.7	0.7	pu	0.8	0.8	=:	4.	4.	pu	<u></u>	9.	6.0	4.	<u>~</u>	6.0	0.	0.	3.3	=:	6.0	4.	1.2	9.0	pu	9.0	1.7	6.0	2.1	0.	<u>~</u>
OgM	pu	pu	pu	pu	pu	pu	pu	pu	4.2	3.8	pu	3.5	pu	pu	4.3	pu	pu	pu	pu	2.3	pu	pu	pu	pu	pu	pu	pu	4.	pu	4.5	pu	4.
۵	45	46	47	48	_	2	$\sim$	4	2	9	7	∞	6	0	=	12	<u>~</u>	4	15	91		<u>8</u>	6	20	21	22	23	24	25	26	27	28
>		<u>-</u>	<u> </u>	<u>-</u>	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w12	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2	w 2

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ZrO <sub>2</sub>	0.007	0.007	0.004	900'0	0.010	900'0	900'0	0.010	0.008	0.008	0.002	0.005	0.005	0.005	0.003	0.002	0.003	0.005	0.005	0.005	0.005	0.005	0.002	900'0	900'0	0.005	0.005	0.003	900'0	900'0	0.018	0.003
SrO	0.008	0.008	0.007	0.00	910.0	0.00	0.001	0.015	0.008	0.008	910.0	0.009	0.009	0.010	0.013	0.007	0.008	0.009	0.010	0.009	0.009	0.009	0.008	0.009	910.0	0.010	0.009	0.011	0.010	0.009	0.002	0.011
$Rb_2O$	pu	pu	pu	0.002	pu	0.002	0.002	pu	pu	pu	pu	0.00	0.00	0.00	pu	pu	pu	0.00	0.00	0.00	0.00	0.00	pu	0.00	pu	0.00	0.00	pu	0.00	0.00	pu	pu
As <sub>2</sub> O <sub>3</sub>	pu	0.355	pu	pu	pu	0.005	pu	0.161	pu	pu	pu	pu	pu	0.155	pu	0.282	pu	pu	0.009	0.007	pu	pu	0.319									
ZnO	0.003	0.003	pu	0.004	0.002	0.002	0.001	0.001	0.003	0.002	pu	0.005	0.003	0.003	pu	pu	0.001	0.003	0.002	0.002	0.004	0.00	pu	pu	pu	0.00	0.001	0.001	0.002	0.004	0.00	0.003
CuO	0.001	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu									
$Fe_2O_3$	0.315	0.293	0.217	0.153	0.334	0.156	0.171	0.311	0.280	0.333	0.173	0.177	0.176	0.163	0.178	0.146	0.199	0.177	0.183	0.146	0.160	0.172	0.183	0.162	0.229	0.163	0.181	0.165	0.185	0.167	0.058	0.290
MnO	pu	0.031	pu	0.432	pu	pu	0.420	pu	pu	pu	0.264																					
CgO	15.8	15.7	15.5	6.5	15.6	6.5	l.9	15.6	15.4	1.91	13.7	13.0	13.5	12.7	17.5	14.5	15.4	13.3	13.4	13.0	12.7	13.2	15.5	13.2	4.4	12.8	12.8	15.8	13.5	12.9	8.4	17.6
K <sub>2</sub> O	0.3	0.3	0.0	4.0	0.2	4.0	0.3	0.2	0.3	0.3	pu	0.5	0.5	0.5	pu	pu	pu	0.5	9.0	0.5	0.5	9.0	pu	0.5	pu	0.5	0.5	0.3	9.0	0.5	pu	0.2
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu										
SO	9.0	0.7	1.2	0.5	0.2	0.5	0.5	0.3	9.0	0.7	6.0	9.0	9.4	0.5	0.	<u></u>		9.0	0.5	0.2	9.0	9.0	<u></u>	9.0	1.2	0.5	9.0	4.	0.5	9.0	0.3	<u>4</u> .
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu										
SiO <sub>2</sub>	89.3	94.9	95.3	94.8	98.4	93.5	90.2	8.96	92.3	94.4	91.3	95.0	100.7	94.7	91.3	87.1	1.96	266	9.101	91.7	93.9	96.2	0.96	1.66	1.96	95.3	0.96	0.96	8.76	97.8	93.1	6.19
$Al_2O_3$	0.5	9.0	0.8	2.0	6.0	2.1	6:1	6.0	0.7	0.7	pu	1.7	2.0	1.5	0.8	pu	6.0	<u>~</u>	2.1	9.1	9:1	2.0	6.0	<u>~</u>	0.	6:1	<u>~</u> .	0.7	6:1	2.0	<u> </u>	0.8
MgO	pu	pu	pu	4.6	pu	4.	4.	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	3.8	pu
۵	29	30	3	32	33	34	35	36	37	38	_	2	$\sim$	4	2	9	7	∞	6	0	=	12	<u>~</u>	4	15	91		<u>&amp;</u>	6	20	_	7
>	w12	w 2	w12	w 2	<u>×</u>	<u>×</u>	<u>w</u>	<u>~</u>	<u>w</u>	<u>w</u>	<u>×</u>	<u>~</u>	<u>×</u>	<u>~</u>	<u>6</u>   %	6  w																

$ZrO_2$	0.003	0.018	0.002	0.003	0.003	0.002	0.004	0.002	0.003	0.018	0.003	0.019	0.018	0.018	0.018	0.018	0.020	0.005	0.004	0.002	0.003	0.005	0.004	0.003	0.018	0.019	0.018	0.019	0.018	0.018	0.019	0.018
SrO	0.012	0.003	0.012	0.012	0.012	0.008	0.01	0.007	0.01	0.003	0.012	0.002	0.003	0.002	0.002	0.002	0.003	0.010	900'0	0.003	9000	0.007	0.005	900'0	0.003	0.002	0.003	0.003	0.003	0.002	0.002	0.002
$Rb_2O$	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$As_2O_3$	0.319	pu	0.319	0.192	0.189	pu	0.315	pu	0.278	pu	0.185	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
ZnO	0.002	pu	0.003	pu	0.00	pu	0.00	pu	0.002	pu	0.002	pu	pu	0.00	pu	pu	pu	0.002	0.003	0.00	0.002	900'0	0.003	0.001	0.00	pu	pu	pu	pu	0.001	pu	pu
CnO	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	0.003	pu	pu	pu	0.004	0.004	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.261	0.073	0.239	0.288	0.251	0.178	0.258	0.185	0.279	0.053	0.276	0.070	0.072	0.075	0.054	9/0.0	0.083	0.114	0.184	0.075	0.159	0.162	0.194	0.222	0.062	0.078	0.075	0.062	990.0	0.052	0.049	0.064
MnO	0.254	pu	0.281	0.293	0.245	pu	0.250	pu	0.233	pu	0.253	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	17.8	8.3	17.6	18.4	18.6	16.3	17.0	15.9	17.3	8.2	17.8	8.4	8.2	8.4	8.4	8.3	8.3	12.5	15.7	9.0	15.4	15.6	15.3	15.3	— —	8.2	8.4	8.2	8.7	8.4	8.7	— —
$K_2O$	0.2	pu	0.2	0.2	0.2	pu	0.2	pu	0.2	pu	0.2	pu	pu	pu	pu	pu	pu	0.5	pu	pu	pu	0.2	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
D	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO <sub>3</sub>	4.1	0.3	<u>~</u>	<u>4</u> .	<u>4</u> .	1.2	<u>~</u>	6.0	0:	0.2	<u>~</u>	0.3	0.2	0.3	0.2	0.2	0.3	0.8	0.8	0.7	0.7	9.0	0.7	0.7	0.3	0.3	0.3	0.3	9.0	0.3	0.2	0.2
$P_2O_5$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	94.1	93.1	94.4	95.0	95.0	93.1	93.8	6.06	93.2	93.8	95.4	89.5	93.7	93.3	93.0	92.9	92.3	92.5	0.96	6.96	92.1	93.3	92.4	95.3	9.88	91.5	92.8	92.2	95.3	92.1	95.3	91.2
$Al_2O_3$	Ξ	1.2	0:	6.0	1.2	9.0	0:	pu	Ξ	<u>4</u> .	1.2	<u></u>	1.2	<u></u>	1.2	0:	1.2	9.	6.0	pu	0.7	6.0	6.0	0.8	1.2	1.2	1.2	=	<u>4</u> .	1.2	<u></u>	Ξ
OgM	pu	3.8	pu	pu	pu	pu	pu	pu	pu	3.7	pu	3.7	3.9	3.8	3.8	3.8	3.7	pu	pu	2.8	pu	pu	pu	pu	3.3	3.6	3.8	4.0	4.0	3.8	3.5	3.5
Ь	3	4	2	9	7	8	6	0	=	12	<u>~</u>	4	15	9		<u>&amp;</u>	6	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34
>	61w	6  <b>M</b>	6  w	6  <b>M</b>	6  w	<u>6</u>   ×	6  w	<u>6</u>   ×	6  w	6  w	6  w	<u>6</u>   %	6  <b>%</b>	6  <b>M</b>	<u>6</u>   ×	6  w	6  w	6  w	6  w	6  w	6  w	6 ×	<u>6</u>   %	<u>6</u>   %	<u>6</u>   %	<u>6</u>   ×	6  <b>%</b>	<u>6</u>   %	<u>6</u>   %	<u>6</u>   %	<u>6</u>   %	6  w

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$ZrO_2$	0.018	0.019	0.019	0.019	0.019	0.018	0.019	0.019	0.020	0.018	0.018	0.004	0.003	0.003	0.004	0.003	0.018	0.004	0.004	0.006	0.002	0.019	0.017	0.019	0.017	0.003	0.002	0.007	0.007	0.007	0.008	0.007
S.	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.003	0.002	900'0	900.0	0.005	0.005	0.005	0.002	0.005	900.0	0.017	0.011	0.002	0.002	0.002	0.003	0.011	0.012	0.020	0.019	0.019	0.020	0.021
$Rb_2O$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	0.00	0.00	0.001	0.001
As <sub>2</sub> O <sub>3</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.290	0.278	pu	pu	pu	pu	0.286	0.328	0.536	0.571	0.588	0.569	0.594
ZnO	pu	pu	pu	pu	0.002	0.00	0.00	pu	0.00	0.002	pu	0.00	0.00	0.002	0.00	pu	0.00	0.00	pu	9000	pu	pu	pu	pu	pu	0.004	0.004	0.00	0.00	pu	pu	pu
CnO	pu	pu	pu	pu	pu	pu	0.00	pu	0.00	pu	pu	0.00	0.004	pu	0.003	0.003	pu	pu	0.00	0.00	pu	pu	pu	pu	pu	pu						
$Fe_2O_3$	0.073	0.070	0.073	0.061	0.068	0.049	0.057	0.058	0.061	0.067	0.075	0.199	0.194	0.202	0.169	0.201	0.059	0.197	0.191	0.225	0.276	990.0	0.063	0.058	0.070	0.248	0.285	0.329	0.272	0.277	0.264	0.264
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.345	0.272	pu	pu	pu	pu	0.243	0.241	0.421	0.452	0.457	0.480	0.475
CaO	8.4	— —:	8.5	8.0	8.3	8.2	8.0	7.8	8.5	8.4	8.2	15.8	15.6	14.8	15.2	15.5	8.2	15.7	1.91	14.8	17.3	8.2	— —:	8.3	— —:	17.2	17.3	14.5	<u>4.</u> –.	_ 	13.6	14.2
K <sub>2</sub> O	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.2	pu	pu	pu	pu	0.2	0.2	9.0	9.0	0.7	9.0	9.0
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO	0.2	0.3	0.3	0.2	0.2	0.2	pu	0.2	0.2	0.2	0.3	6.0	0.8	0.8	0.8	6.0	0.3	0.7	0.8	6.0	0:	0.3	pu	pu	0.3	0:	1.2	9.0	0.7	0.7	0.7	9.0
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	93.8	91.2	97.6	7.16	6.16	1.06	87.5	84.8	6.68	200.7	88.9	92.7	92.5	88.4	86.2	92.1	87.8	6.16	93.0	94.8	92.8	8.06	9.88	88.3	87.3	92.2	88.4	85.4	85.4	83.7	85.3	84.7
Al <sub>2</sub> O <sub>3</sub>	1.3	0:	1.2	1.2	1.2	<u></u>	=	0:	=	1.2	0:	0.7	0.8	0.5	9.0	0.8	6.0	9.0	9.0	0.8	0:	=	=	1.2	0:	6.0	0.8	2.5	2.5	2.3	2.6	2.4
OgM	3.9	3.7	3.6	3.6	3.3	3.3	3.	2.8	3.5	3.0	3.0	pu	pu	pu	pu	pu	3.0	pu	pu	pu	pu	3.5	3.6	3.2	3.2	pu	pu	pu	pu	pu	pu	pu
۵	35	36	37	38	39	9	4	42	43	4	45	46	47	48	49	20	51	52	53	54	55	26	27	28	29	09	19	62	63	64	65	99
≯	6 w	<u>8</u>	<u>8</u>	<u>6</u>   ×	<u>8</u> ×	<u>8</u>  %	<u>8</u> ×	<u>8</u>	<u>8</u>	<u>8</u>	<u>6</u> ×	6 ×																				

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$ZrO_2$	0.008	0.006	0.006	0.008	0.006	0.006	0.007	0.006	0.007	0.006	0.007	0.005	0.008	0.007	0.006	0.006	0.007	0.006	0.007	0.007	0.006	0.005	0.006	0.006	0.007	0.006	0.007	0.006	0.007	0.006	0.007	0.007
SrO	0.020	0.008	0.008	0.002	0.009	0.008	0.008	0.008	0.008	0.008	0.009	0.010	0.002	0.008	0.008	0.008	0.008	0.009	0.008	0.009	0.008	0.008	0.008	0.008	0.009	0.008	0.008	0.008	0.008	0.008	0.009	0.009
$Rb_2O$	0.00	pu	pu	0.003	pu	pu	pu	pu	pu	pu	pu	0.00	0.003	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
As <sub>2</sub> O <sub>3</sub>	0.590	0.095	0.085	pu	0.090	0.085	0.088	0.087	0.090	0.093	0.092	pu	pu	0.093	0.083	0.090	0.088	0.084	0.090	0.095	980.0	0.088	0.092	0.081	0.089	0.084	980'0	0.088	0.085	0.087	0.087	0.081
ZnO	pu	0.00	pu	0.738	pu	pu	pu	0.00	pu	0.003	pu	pu	0.737	pu	pu	pu	0.002	0.00	0.002	pu	0.00	0.00	0.00	pu	0.00	pu	pu	0.00	0.00	pu	pu	pu
CuO	pu	pu	pu	0.001	pu	pu	pu	pu	0.002	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.259	0.147	0.145	0.020	0.151	0.124	0.119	0.128	0.149	0.140	0.153	0.167	0.033	0.137	0.162	0.131	0.123	0.135	0.142	0.129	0.124	0.126	0.14	0.127	0.134	0.123	0.148	0.135	0.145	0.141	0.140	0.131
MnO	0.494	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	14.3	16.2	15.6	5.9	0.91	15.9	15.0	16.3	1.9	0.91	16.4	13.9	6.2	1.9	15.7	15.8	15.8	0.91	16.3	16.2	15.8	16.2	15.7	15.0	15.9	15.0	15.5	15.5	0.91	15.6	1.9	16.3
K <sub>2</sub> O	9.0	pu	pu	3.9	pu	pu	pu	pu	pu	pu	pu	0.5	4.2	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ū	pu	pu	pu	9.0	pu	pu	pu	pu	pu	pu	pu	pu	0.8	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO	0.7	9.0	9.0	pu	9.0	0.7	9.0	9.0	9.0	9.0	0.7	0.5	pu	9.0	0.7	0.7	0.7	0.7	0.7	0.7	9.0	9.0	9.0	9.0	0.8	9.0	0.7	0.7	0.7	0.8	0.7	9.0
$P_2O_5$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	85.6	97.6	93.5	84.6	92.8	94.7	88.4	93.0	9.76	91.5	0.96	99.3	95.5	95.9	95.1	93.6	95.4	93.6	95.5	94.6	87.1	94.5	94.5	86.2	97.0	90.2	94.0	9.16	95.0	91.2	96.4	92.5
$Al_2O_3$	2.6	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	1.7	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
ОдМ	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
<u>م</u>	29	_	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12	<u> </u>	4	15	91		<u>&amp;</u>	61	_	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12
≯	61w	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w29	w30	w30	w30	w30	w30	w30	w30	w30	w30	w30	w30	w30

$ZrO_2$	900'0	0.007	0.007	0.007	0.010	0.009	0.009	0.009	0.008	0.008	0.009	0.01	0.010	0.010	0.012	0.010	900'0	0.009	0.007	0.01	0.010	0.008	0.010	0.008	0.010	0.010	0.010	0.009	0.010	0.010	0.007	0.012
SrO	0.008	0.008	0.008	0.008	0.015	0.017	910.0	910.0	910.0	0.015	0.017	0.00	0.014	0.003	0.003	0.00	0.007	0.003	0.01	0.009	0.00	0.015	0.003	0.017	0.002	910.0	910.0	0.017	0.017	0.017	910.0	0.014
$Rb_2O$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	pu	0.00	0.00	0.002	pu	0.00	pu	pu	0.002	pu	0.00	pu	0.002	pu	pu	pu	pu	pu	pu	pu
As <sub>2</sub> O <sub>3</sub>	0.087	0.088	0.089	0.085	pu	pu	0.007	900'0	pu	pu	0.005	pu	pu	pu	pu	pu	0.164	pu	0.107	0.015	pu	pu	pu	0.005	pu	pu	pu	900'0	0.005	0.005	0.007	0.245
ZuO	pu	pu	pu	0.002	pu	pu	pu	pu	pu	pu	pu	0.002	pu	0.00	pu	pu	0.005	pu	0.00	0.014	0.001	pu	pu	pu	0.00	0.002	0.00	0.00	pu	pu	pu	0.003
CnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	0.00	pu	pu	0.00	pu	0.001	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.003	pu
$Fe_2O_3$	0.118	0.144	0.139	0.146	0.196	0.157	0.177	0.171	0.191	0.157	0.167	0.137	0.157	0.102	0.113	0.145	0.208	0.082	0.129	0.261	0.137	0.163	0.130	0.158	0.133	0.172	0.177	0.180	0.178	0.204	0.193	0.181
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.061	pu	pu	0.336	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.029
CaO	1.91	16.0	16.4	16.0	13.6	14.3	13.9	14.0	13.8	14.0	1.4	5.4	13.8	7.3	7.0	5.7	13.8	7.5	14.5	14.0	5.5	<u>4</u>	7.3	14.3	5.5	13.5	13.0	13.7	12.9	13.7	13.9	12.1
K <sub>2</sub> O	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.3	pu	0.5	9.0	0.3	0.0	4.0	pu	pu	0.3	pu	0.5	pu	0.3	pu	pu	pu	pu	pu	pu	pu
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	0.7	9.0	0.7	0.7	6.0	6.0	6.0	0:	0.	6.0	6.0	9.0	0.7	0.5	0.5	0.5	0.8	9.0	0.	0.8	0.5	6.0	0.5	0.	0.5	0.	6.0	6.0	6.0	0:		0.7
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	9.1	<u>~</u>	2.0	9.	9.1	-5.	9.1	1.7	2.0	4.	1.7	€.	<u></u>	4.	7.	<u>~</u>	1.2	7.	<u></u>	4.	7.	<u>~</u>	6:	9.	6.	6.	9.1	<u>~</u>
SiO <sub>2</sub>	93.6	95.1	0.96	96.3	34.9	32.9	33.4	40.0	39.6	0.14	36.8	32.1	30.2	40.7	29.7	1.94	46.9	39.0	<u>4</u> .8	34.9	40.6	42.3	46.5	45.7	37.8	35.7	29.4	37.9	28.5	32.6	42.5	37.8
Al <sub>2</sub> O <sub>3</sub>	0.5	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Д.	13	4	15	9	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	15	9		<u>∞</u>	6	20	21	22	23	24	25	26	27	28
>	w30	w30	w30	w30	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w3	w31

$ZrO_2$	0.009	0.010	0.010	0.009	0.010	0.008	0.009	0.008	0.011	0.009	0.008	0.01	0.01	0.009	0.010	0.009	0.008	0.008	0.009	0.008	0.011	0.009	0.008	0.013	0.008	0.008	0.009	0.008	0.009	0.008	0.012	0.011
SrO	910.0	0.017	0.00	0.017	0.017	910.0	910.0	910.0	0.007	0.007	0.002	900'0	0.003	910.0	0.00	0.017	910.0	0.015	910.0	910.0	0.00	0.015	910.0	0.003	0.015	910.0	0.015	0.015	0.015	910.0	0.008	0.007
$Rb_2O$	pu	pu	0.002	pu	pu	pu	pu	pu	0.00	0.00	pu	0.00	0.00	pu	0.002	pu	pu	pu	pu	pu	0.002	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu
As <sub>2</sub> O <sub>3</sub>	0.007	pu	pu	pu	0.005	pu	pu	pu	pu	0.843	pu	pu	pu	pu	pu	900'0	0.007	pu	pu	0.005	pu	0.007	900'0	pu	pu	900'0	pu	900'0	900'0	pu	980'0	980'0
ZnO	0.001	pu	0.002	pu	0.00	pu	pu	pu	0.00	0.003	pu	0.00	0.00	pu	pu	pu	pu	pu	pu	pu	0.002	0.00	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu
CnO	pu	pu	pu	pu	pu	pu	pu	0.002	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$Fe_2O_3$	0.167	0.200	0.147	0.188	0.164	0.184	0.179	0.168	0.131	0.316	0.074	0.187	0.128	0.146	0.140	0.171	0.167	0.170	091.0	0.162	091.0	0.168	0.166	0.129	0.157	0.176	0.162	0.162	0.142	0.158	0.154	0.123
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.013	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	12.9	13.5	5.8	13.5	13.6	13.9	4.4	13.9	12.2	13.1	—. —.	9.	7.1	13.2	5.6	14.2	4.4	13.5	13.6	13.6	5.4	12.6	13.7	6.5	13.8	13.7	13.5	13.4	13.3	13.9	14.2	14.2
K <sub>2</sub> O	pu	pu	4.0	pu	pu	pu	pu	pu	0.5	4.0	0.2	0.5	9.0	pu	0.3	pu	pu	pu	pu	pu	0.3	pu	pu	4.0	pu	pu	pu	pu	pu	pu	pu	pu
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	6.0	6.0	0.5	0.	6.0	6.0	0.	0.	0.5	0.8	0.5	0.5	0.5	0.8	9.0	6.0	0.8	0.8	0.8	0.8	0.5	0.8	0.8	9.0	6.0	0.8	6.0	0.8	0.8	6.0	9.0	0.7
P <sub>2</sub> O <sub>5</sub>	9.1	<u>~</u>	<u>1</u> .5	<u>~</u>	2.1	<u>4</u> .	1.5	1.7	1.5	1.7	1.5	1.7	9:1	<u>~</u>	9:1	1.7	9.1	9.1	1.5	9.1	<u>8</u> .	6:1	<u> </u>	2.1	9.1	<u>4</u> .	1.7	9.1	1.7	1.5	<u>-</u> .	<u>-</u> :
SiO <sub>2</sub>	32.3	30.9	42.2	34.5	29.9	42.8	43.6	39.1	42.6	44.2	38.8	32.8	34.1	30.1	35.6	35.8	41.0	34.1	39.6	35.0	27.5	27.9	4	18.8	40.7	38.5	35.2	34.2	33.2	39.0	39.8	42.8
Al <sub>2</sub> O <sub>3</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
OgM	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
<u>م</u>	29	30	$\frac{3}{2}$	32	33	34	35	36	37	38	39	4	4	42	43	4	45	46	47	48	49	20	5	52	53	54	55	26	57	28	_	2
>	w3l	w31	w31	w31	w31	w3I	w3I	w3	w31	w31	w3	w31	w3	w31	w31	w3	w3	w3I	w3	w3	w3	w31	w3	w3I	w31	w3I	w3	w3	w3	w3	w35	w35

$ZrO_2$	0.012	0.012	0.013	0.012	0.012	0.013	0.012	0.012	0.015	0.012	0.011	0.012	0.011	0.011	0.011	0.012	0.011	0.009	0.011	0.011	0.011	0.011	0.012	0.012	0.013	0.012	0.011	0.013	0.012	0.012	0.012	0.012
SrO	0.008	0.008	0.008	0.008	0.008	0.009	0.008	0.007	0.008	0.009	0.008	0.008	0.008	0.007	0.008	0.008	0.009	0.008	0.008	0.009	0.008	0.009	0.009	0.008	0.008	0.008	0.008	0.009	0.008	0.008	0.008	0.008
$Rb_2O$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
$As_2O_3$	0.092	0.092	980.0	0.085	0.095	0.094	980.0	0.087	0.092	0.085	0.078	0.097	0.088	pu	0.088	0.082	0.095	0.658	0.077	0.085	0.088	0.094	0.091	0.089	0.000	0.000	960'0	0.095	0.000	980.0	0.088	0.090
ZnO	pu	pu	0.003	0.002	pu	pu	0.002	pu	pu	pu	0.002	pu	pu	0.004	0.00	0.00	pu	0.00	0.002	pu	pu	pu	0.003	pu	pu	pu	pu	pu	pu	pu	pu	pu
CnO	0.002	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.003	pu	pu	0.002	pu	pu	pu	pu	pu	pu	pu	0.001	pu	pu	pu	pu	pu
$Fe_2O_3$	0.128	0.125	0.122	0.144	0.133	0.142	0.159	0.128	0.152	0.143	0.136	0.143	0.123	0.137	0.140	0.134	0.146	0.204	0.125	0.131	0.139	0.144	0.138	0.133	0.144	0.132	0.144	0.116	0.135	0.125	0.123	0.139
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
CaO	14.5	<u>4.</u> 	14.2	14.6	14.2	15.1	14.6	14.3	14.2	4.4	<u>4.</u> —.	14.2	14.3	13.5	14.9	13.4	15.6	12.2	14.2	15.3	14.2	15.5	14.7	14.2	14.5	4.4	14.8	15.5	15.0	14.7	14.6	4. 4.
$K_2O$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	4.0	pu	pu	pu	0.5	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	0.7	0.7	0.7	0.7	9.0	0.7	0.7	0.7	0.7	0.8	0.8	0.7	0.7	0.8	0.8	0.7	0.8	6.0	0.7	0.8	0.8	6.0	0.8	0.7	0.8	0.7	6.0	0.7	0.8	0.7	0.7	0.7
$P_2O_5$	1.3	<u>1.5</u>	<u>-</u> .	<u>-</u> .	<u>4</u> .	1.5	3	<u>-</u> .	6:1	<u>-</u> .	1.2	<u></u> 3	<u> </u>	<u>-</u> .	<u></u>	1.5	=:	<u></u> 3	<u></u> 3	<u></u> 3	1.2	1.2	1.2	1.5	<u>4</u> .	1.5	<u>4</u> .	1.5	<u>4</u> .	<u>4</u> .	7.	1.5
$SiO_2$	39.5	39.1	37.8	42.5	4	43.8	44.3	0.14	29.7	45.6	45.0	38.5	44.8	53.3	48.5	36.4	54.3	46.0	41.8	54.1	44.8	54.4	46.8	39.5	45.6	41.5	50.7	44.6	47.3	45.6	43.2	41.9
$Al_2O_3$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ь	~	4	2	9	_	∞	6	0	=	12	<u>~</u>	4	15	91		<u>&amp;</u>	61	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34
<b>*</b>	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35

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$ZrO_2$	0.01	0.0	0.012	0.016	0.013	0.012	0.012	0.0	0.012	0.016	0.012	0.012	0.0	0.03	0.00	0.015	0.03	0.03	0.018	0.036	0.00	0.035	0.03	0.032	0.033	0.00	0.033	0.00	0.03	0.033	0.035	0.00
SrO	0.008	0.004	0.003	0.007	0.008	0.008	0.007	0.008	0.002	900.0	0.008	0.009	0.008	0.087	0.007	900.0	0.087	0.084	0.053	0.086	0.007	0.090	0.086	0.083	0.085	0.007	0.085	0.008	0.089	0.08	0.084	0.007
$Rb_2O$	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.005	pu	pu	0.004	0.005	0.003	0.004	pu	0.005	0.005	0.005	0.004	pu	0.004	pu	0.004	0.004	0.004	pu
$As_2O_3$	0.088	pu	pu	pu	0.087	0.088	0.089	0.094	pu	pu	0.095	0.087	0.094	0.120	0.007	0.034	0.138	0.118	pu	0.123	0.010	0.151	0.144	0.139	0.165	0.009	0.135	0.008	0.126	0.116	0.138	0.009
ZnO	0.001	pu	pu	pu	pu	pu	pu	pu	0.00	pu	0.00	0.004	pu	0.029	pu	pu	0.028	0.028	0.026	0.029	pu	0.030	0.026	0.032	0.028	pu	0.031	pu	0.028	0.027	0.026	0.00
CnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.002	0.008	pu	pu	0.008	0.011	pu	0.008	pu	0.013	0.015	0.012	0.011	pu	0.01	0.00	0.015	0.014	900'0	pu
$Fe_2O_3$	0.124	0.070	0.070	0.102	0.118	0.147	0.130	0.124	0.073	0.107	0.142	0.137	0.143	1.477	0.175	0.116	1.392	1.376	0.567	1.415	0.189	1.474	1.409	1.349	1.365	0.168	1.406	0.187	1.391	1.304	1.328	0.177
MnO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	696.0	pu	pu	0.973	0.904	0.550	0.931	pu	1.034	0.935	0.889	0.949	pu	196.0	pu	996.0	998.0	0.951	pu
CaO	14.3	7.7	6.2	5.1	4.4	4.4	15.1	14.5	1.9	5.3	14.8	14.2	15.0	24.7	9.91	15.6	24.1	23.7	22.5	24.4	16.4	25.2	23.9	22.9	23.2	9.91	23.6	16.4	24.8	23.0	23.4	16.2
K <sub>2</sub> O	pu	4.0	0.0	0.2	pu	pu	pu	pu	0.0	0.2	pu	pu	pu	4.6	pu	pu	4.5	4.5	3.8	4.5	pu	4.7	4.5	4.3	4.4	pu	4.4	pu	4.7	4.3	4.3	pu
ס	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	9.0	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	0.7	9.0	0.5	0.8	0.7	0.7	0.7	0.7	0.5	0.8	0.8	0.7	0.7	9.0	1.2	<u></u>	0.8	0.8	pu	0.5	Ξ:	0.7	6.0	0.7	3.2	=	0.8	=	0.5	0.5	0.7	6.0
$P_2O_5$	1.3	<u>+</u> .	<u>+</u> .	<u></u>	9:1	1.5	<u></u>	<u>-</u> .	.5	9:1	<u>-</u> .	1.5	1.2	2.3	pu	pu	2.3	2.3	3.	2.5	pu	2.4	2.3	2.0	3.0	pu	2.2	pu	2.5	2.2	2.3	pu
SiO <sub>2</sub>	46.0	40.2	43.5	42.3	4	4.8	51.1	44.3	43.8	40.9	47.6	35.3	49.8	84.9	6.96	93.5	84.1	83.3	76.2	85.1	95.8	82.8	84.7	76.5	9.18	95.8	84.7	97.6	85.2	78.2	81.7	92.4
$Al_2O_3$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	4.8	0.7	pu	4.6	4.6	4.2	4.9	9.0	5.0	4.7	3.8	4.7	9.0	4.5	0.5	4.9	3.7	3.9	9.0
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	4.7	pu	pu	4.0	3.8	3.6	4.6	pu	4.6	4.7	2.8	3.9	pu	4.0	pu	4.4	2.6	4.2	pu
Ь	35	36	37	38	39	40	4	42	43	4	45	46	47	_	2	$\sim$	4	2	9	_	$\infty$	6	0	=	12	2	4	15	91		8	61
>	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	w35	1 <del>4</del> w	1 <del>4</del> %	1 <del>4</del> %	₩ 	₩ 	₩ 	1 <del>4</del> w	1 <del>4</del> w	₩ 	1 <del>4</del> %	1 <del>4</del> w	<b>1</b> 4∾	1 <del>4</del> %	1 <del>4</del> %	1 <del>4</del> %	1 <del>4</del> %	₩ 	-    -	14w

$ZrO_2$	0.015	0.002	0.034	0.034	0.002	0.033	0.002	0.036	0.003	0.002	0.003	0.002	0.024	0.002	0.033	0.032	0.034	0.033	0.005	0.034	0.002	0.035	0.013	0.034	0.035	0.002	0.034	0.034	0.033	0.035	0.036	0.002
S <sub>O</sub>	0.043	9000	0.087	0.090	0.007	0.085	0.007	0.088	0.007	0.007	900.0	0.007	0.090	0.007	0.084	0.083	0.085	0.085	0.137	0.087	9000	980.0	0.029	0.083	0.084	0.007	0.087	980.0	0.085	980.0	0.087	0.007
Rb <sub>2</sub> O	0.004	pu	0.005	0.005	pu	0.004	pu	0.004	pu	pu	pu	pu	0.004	pu	0.004	0.004	0.004	0.004	0.00	0.004	pu	0.005	910.0	0.004	0.005	pu	0.004	0.004	0.004	0.005	0.005	pu
As <sub>2</sub> O <sub>3</sub>	0.007	0.007	0.127	0.130	0.008	0.143	0.008	0.135	0.008	0.009	0.011	0.009	0.097	0.009	0.126	0.123	0.120	0.125	pu	0.129	0.007	0.153	0.011	0.119	0.115	0.008	0.140	0.150	0.121	0.116	0.124	0.008
ZnO	0.024	pu	0.026	0.027	pu	0.031	pu	0.030	pu	pu	pu	0.00	0.030	0.00	0.027	0.026	0.026	0.030	0.005	0.027	pu	0.031	0.035	0.027	0.025	pu	0.026	0.029	0.031	0.029	0.028	0.00
CnO	0.011	pu	0.013	0.009	pu	0.009	pu	0.009	pu	pu	pu	pu	0.007	pu	0.011	0.009	0.011	0.010	pu	0.012	pu	0.007	0.005	0.015	0.012	0.00	0.014	0.012	0.011	0.010	0.010	pu
$Fe_2O_3$	1.374	0.200	1.457	1.421	0.174	1.362	0.164	1.367	0.178	0.186	0.176	0.172	1.097	0.174	1.382	1.344	1.357	1.365	0.943	1.347	0.174	1.372	0.504	1.319	1.344	0.168	1.373	1.392	1.419	1.405	1.405	0.205
MnO	0.201	pu	0.919	0.971	pu	0.951	pu	0.890	pu	pu	pu	pu	0.657	pu	0.900	0.895	0.915	0.919	0.012	0.889	pu	0.989	0.865	0.911	0.926	pu	0.986	1.022	0.951	0.981	0.975	pu
CaO	24.1	0.91	23.7	24.5	15.9	24.3	1.91	23.9	16.4	15.7	16.5	16.2	23.5	1.91	24.0	23.8	23.2	23.5	22.0	24.1	15.9	24.5	0.91	23.2	23.7	16.2	23.8	23.3	23.5	23.7	23.3	16.5
K <sub>2</sub> O	4.8	pu	4.5	4.5	pu	4.5	pu	4.2	pu	pu	pu	pu	5.3	pu	4.5	4.4	4.4	4.4	6.1	4.4	pu	4.6	10.4	4.3	4.5	pu	4.6	4.3	4.5	4.5	4.	pu
ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.3	pu	pu	pu	0.5	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	1.3	0:	0.7	0.5	0:	0.7	0.	0.7	0.	=	=:	=	1.2	0:	9.0	9.0	0.8	0.7	9.0	6.0	6.0	0.7	=:	0.	9.0	=	0.8	0.8	9.0	9.0	0.5	0.8
P <sub>2</sub> O <sub>5</sub>	3.4	pu	2.3	2.4	pu	2.3	pu	2.0	pu	pu	pu	pu	2.3	pu	2.4	2.3	2.3	2.2	pu	2.5	pu	2.4	4.2	2.3	2.3	pu	2.2	2.3	2.3	2.3	2.3	pu
SiO <sub>2</sub>	75.0	92.1	83.3	81.7	92.4	83.9	94.2	80.4	95.7	93.6	95.7	95.2	71.3	94.6	83.2	83.9	83.5	84.I	82.8	82.7	93.4	85.6	80.2	82.4	9.08	95.2	82.1	82.6	82.2	81.2	78.9	74.7
$Al_2O_3$	3.4	0.7	4.9	4.2	0.5	4.9	9.0	4.2	9.0	0.5	0.7	0.7	2.1	0.5	4.6	4.6	4.7	4.6	2.5	4.2	9.0	4.6	2.8	4.6	4.3	9.0	4.4	4.	4.6	4.4	3.9	pu
OgM	2.2	pu	3.9	3.9	pu	4.4	pu	3.4	pu	pu	pu	pu	2.3	pu	4.0	3.4	4.	4.3	4.5	3.6	pu	4.4	9.6	3.7	3.9	pu	4.2	3.9	4.4	3.6	3.8	pu
Ь	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34	35	36	37	38	39	9	4	42	43	44	45	46	47	48	49	20	_
≯	14w	₩ 	14w	1 <del>4</del> %	   	1 <del>4</del> %	   	₩ 	₩ 	14×	₩ 	1 <del>4</del> %	₩ 	1 <del>4</del> %	W44	14×	1 <del>4</del> %	1 <del>4</del> %	W44	-    -	W44	₩  -	₩ 	₩  -	₩ 	   	   	w42.1				

| 0.003 | 0.036  | 0.012   | 0.012   | 0.029  | 0.002  | 0.018  | 910.0  | 0.002  | 910.0  | 0.039  | 0.017  
   | 0.014   | 0.027  | 0.018  | 0.029   | 0.004  | 0.003   | 0.014  
   
   | 0.002  | 0.018   | 0.027  | 910.0   
  | 0.003  | 0.014  | 0.028   | 0.014   | 0.002  
   | 0.010   | 0.002  | 0.002  | 0.007   |
|-------|--|---|---|--|--|--|--|--|--|--
--|---|--|--|---|--|---
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--|--|---|--
--|--|--|---|---
--|---|--|--
---|
| 900'0 | 0.063  | 0.04  | 0.04  | 0.08   | 0.007  | 0.056  | 0.059  | 9000   | 900'0  | 0.061  | 0.056  
   | 0.007   | 0.077  | 0.047  | 0.080   | 0.002  | 0.015   | 900.0  
   
   | 0.007  | 090.0   | 0.079  | 0.007   
  | 0.010  | 0.007  | 0.082   | 0.078   | 0.010  
   | 0.101   | 900'0  | 0.007  | 900'0   |
| pu    | 0.004  | 0.004   | 0.004   | 0.003  | pu   | 0.003  | 0.002  | pu   | pu   | 0.004  | 0.003  
   | 0.00  | 0.003  | 0.004  | 0.003   | pu   | pu  | pu   
   
   | pu   | 0.003   | 0.003  | 0.00  
  | pu   | pu   | 0.003   | 0.003   | pu   
   | 0.00  | pu   | pu   | pu  |
| 900'0 | 0.124  | pu  | 0.010   | 0.192  | 0.010  | 900'0  | 0.014  | 900'0  | pu   | 0.115  | pu   
   | 0.020   | 0.114  | 0.020  | 0.114   | pu   | 0.210   | 0.071  
   
   | 0.007  | 0.009   | 0.205  | 0.018   
  | 690.0  | 0.068  | 0.133   | 0.009   | 690'0  
   | 0.029   | pu   | 0.008  | pu  |
| pu    | 0.021  | 0.023   | 0.023   | 0.025  | pu   | 0.020  | 0.023  | pu   | pu   | 0.021  | 0.024  
   | pu  | 0.026  | 0.024  | 0.027   | pu   | pu  | pu   
   
   | pu   | 0.025   | 0.029  | pu  
  | pu   | pu   | 0.027   | 0.024   | pu   
   | 0.008   | 0.00   | pu   | 0.010   |
| pu    | 0.007  | 0.007   | 0.014   | 0.010  | pu   | 0.003  | 0.003  | 0.001  | pu   | 0.010  | pu   
   | 0.002   | 900.0  | 0.013  | 0.010   | pu   | pu  | pu   
   
   | pu   | 0.004   | 900.0  | pu  
  | 0.001  | pu   | 0.008   | 0.008   | pu   
   | 0.005   | pu   | pu   | 0.001   |
| 0.183 | 1.132  | 1.165   | 1.130   | 1.314  | 0.157  | 0.529  | 0.594  | 0.185  | 0.108  | 1.266  | 0.550  
   | 1.959   | 1.378  | 1.479  | 1.422   | 0.140  | 0.155   | 0.116  
   
   | 0.201  | 0.554   | 1.300  | 1.979   
  | 0.164  | 0.099  | 1.488   | 1.434   | 0.152  
   | 1.035   | 0.182  | 0.207  | 0.246   |
| pu    | 0.598  | 0.091   | 0.089   | 0.797  | pu   | 0.641  | 0.537  | pu   | pu   | 0.631  | 0.518  
   | 1.282   | 0.749  | 0.212  | 0.857   | pu   | pu  | pu   
   
   | pu   | 0.588   | 0.774  | 1.442   
  | pu   | pu   | 0.854   | 0.193   | pu   
   | 0.198   | pu   | pu   | pu  |
| 15.8  | 25.8   | 22.7  | 23.9  | 22.8   | 16.0   | 22.7   | 23.9   | 15.9   | 1.9  | 26.4   | 23.0   
   | 8.6   | 22.9   | 22.2   | 24.0  | 8.0  | 14.6  | 16.7   
   
   | 9.91   | 24.7  | 22.0   | 8.8   
  | 16.3   | 0.91   | 24.7  | 22.8  | 15.9   
   | 23.9  | 15.4   | 16.3   | 15.2  |
| pu    | 3.9  | 4.9   | 4.9   | 3.2  | pu   | 3.8  | 3.6  | pu   | pu   | 4.   | 3.8  
   | 0.5   | 3.2  | 5.4  | 3.3   | pu   | pu  | pu   
   
   | pu   | 3.9   | 3.   | 0.5   
  | pu   | pu   | 3.6   | 4.6   | pu   
   | 2.2   | pu   | pu   | 9.0   |
| pu    | pu   | pu  | pu  | 9.0  | pu   | 0.5  | 0.5  | pu   | pu   | pu   | 9.0  
   | pu  | 9.0  | pu   | 0.5   | pu   | pu  | pu   
   
   | pu   | 9.0   | 0.5  | pu  
  | pu   | pu   | 0.3   | 0.3   | pu   
   | 9.4   | pu   | pu   | pu  |
| 0.8   | 2.6  | 9.0   | 9:1   | 0.   | 0:   | pu   | <u>4</u> .   | 0.   |  | 4.0  | pu   
   | 0.3   | pu   | 1.2  | 0.8   | 4.0  | 6.0   | 1.2  
   
   | 0.8  | 1.2   | 0.8  | 0.2   
  | 9.0  | =  | 0.3   | 1.5   | 9.0  
   | 3.7   | 0.8  | 0.8  | 6.0   |
| pu    | 2.3  | 1.7   | 2.0   | 3.   | pu   | 2.5  | 2.7  | pu   | pu   | 1.7  | 2.8  
   | pu  | <u>8</u> .   | 2.2  | 6:1   | pu   | pu  | pu   
   
   | pu   | 3.  | 3.3  | pu  
  | pu   | pu   | 6:1   | 2.6   | pu   
   | 2.0   | pu   | pu   | pu  |
| 74.8  | 9.09   | 65.3  | 9:09  | 58.3   | 77.9   | 61.2   | 52.9   | 74.6   | 79.3   | 54.4   | 63.2   
   | 2.69  | 65.1   | 63.7   | 66.5  | 77.0   | 70.9  | 80.1   
   
   | 78.7   | 62.7  | 59.4   | 74.6  
  | 83.4   | 76.4   | 67.2  | 66.3  | 79.4   
   | 59.8  | 73.0   | 75.5   | 73.3  |
| pu    | 2.3  | 6:  | 2.2   | 2.4  | pu   | 2.7  | 2.3  | pu   | pu   | 2.2  | 2.9  
   | 0.  | 2.4  | 2.6  | 2.5   | 0.7  | pu  | pu   
   
   | pu   | 3.4   | 2.3  | 1.2   
  | pu   | pu   | 2.5   | 2.6   | pu   
   | 9.  | pu   | pu   | pu  |
| pu    | pu   | pu  | pu  | pu   | pu   | pu   | pu   | pu   | pu   | pu   | 2.1  
   | pu  | pu   | pu   | pu  | pu   | pu  | pu   
   
   | pu   | 3.2   | pu   | pu  
  | pu   | pu   | pu  | 2.0   | pu   
   | pu  | pu   | pu   | pu  |
| 2     | $\sim$   | 4   | 2   | 9  | _  | ∞  | 6  | 0  | =  | 12   | <u>n</u>   
   | 4   | 15   | 91   |   | <u>&amp;</u>   | 61  | 20   
   
   | 21   | 22  | 23   | 24  
  | 25   | 26   | 27  | 28  | 29   
   | _   | 7  | $\sim$   | 4   |
| w42.1 | w42.1  | w42.1   | w42.1   | w42.1  | w42.1  | w42.1  | w42.1  | w42.1  | w42.1  | w42.1  | w42.1  
   | w42.1   | w42.1  | w42.1  | w42.1   | w42.1  | w42.1   | w42.1  
   
   | w42.1  | w42.1   | w42.1  | w42.1   
  | w42.1  | w42.1  | w42.1   | w42.1   | w42.1  
   | w42.2   | w42.2  | w42.2  | w42.2   |
|       | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006<br>3 nd 2.3 60.6 2.3 2.6 nd 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006<br>3 nd 2.3 60.6 2.3 2.6 nd 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063<br>4 nd 1.9 65.3 1.7 0.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006<br>3 nd 2.3 60.6 2.3 2.6 nd 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063<br>4 nd 1.9 65.3 1.7 0.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041<br>5 nd 2.2 60.6 2.0 1.6 nd 4.9 23.9 0.089 1.130 0.014 0.023 0.010 0.004 0.041 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.006 3 0.007 0.0 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006<br>3 nd 2.3 60.6 2.3 2.6 nd 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063<br>4 nd 1.9 65.3 1.7 0.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041<br>5 nd 2.2 60.6 2.0 1.6 nd 4.9 23.9 0.089 1.130 0.014 0.023 0.010 0.004 0.041<br>6 nd 2.4 58.3 3.1 1.0 0.4 3.2 22.8 0.797 1.314 0.010 0.025 0.192 0.003 0.081<br>7 nd nd 77.9 nd 1.0 nd nd 16.0 nd 0.157 nd nd 0.010 nd 0.007 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063   4 nd 1.9 65.3 1.7 0.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041   5 nd 2.2 60.6 2.0 1.6 nd 4.9 23.9 0.089 1.130 0.014 0.023 0.010 0.004 0.041   6 nd 2.4 58.3 3.1 1.0 0.4 3.2 22.8 0.797 1.314 0.010 0.025 0.192 0.003 0.081   7 nd nd 77.9 nd 1.0 nd nd 16.0 nd 0.157 nd nd 0.010 nd 0.007   8 nd 2.7 61.2 2.5 nd 0.5 3.8 22.7 0.641 0.529 0.003 0.020 0.006 0.003 0.056 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 3 0.007 0.021 0.124 0.004 0.005 3 nd 0.006 1.132 0.007 0.021 0.124 0.004 0.003 0.004 0.00 | 2 nd nd 74.8 nd 0.08 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 nd 0.006 3 0.007 0.021 0.124 0.004 0.005 | 2 nd nd 748 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 nd 0.006 3 nd 0.005 nd 0.005 nd 0.005 nd 0.005 nd 0.005 nd 0.005 nd 0.004 0.001 nd nd 77.9 nd nd 1.0 nd nd 15.9 nd 0.5 3.8 2.7 0.641 0.529 0.003 0.025 0.192 0.003 0.005 nd 0.007 nd 0.005 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 nd 0.006 3 nd 0.006 nd 0.006 nd 0.006 3 nd 0.005 nd 0.003 nd 0.004 0.004 0.004  0.005 nd 0.23 60.6 2.0 1.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041 0.004 0.041  0.004 0.041 0.004 0.004 0.041 0.004
0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0. | 2 nd nd 74.8 nd 0.8 nd 15.8 nd 0.183 nd 0.006 nd 0.006 nd 0.006 3 3 nd 2.3 60.6 2.3 2.6 nd 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063 4 nd 1.9 65.3 1.7 0.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041 0.041 0.02 | 2 nd nd 748 nd 0.8 nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 3   3 1.0 nd 2.3 60.6 2.3 2.6 nd 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063   4 nd 1.9 65.3 1.7 0.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041   5 nd 2.2 60.6 2.0 1.6 nd 4.9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041   6 nd 2.4 58.3 3.1 1.0 0.4 3.2 22.8 0.797 1.314 0.010 0.025 0.192 0.003 0.081   7 nd nd 77.9 nd 1.0 nd nd 16.0 nd 0.185 0.003 0.020 0.006 0.006 0.005   9 nd 2.3 52.9 2.7 1.4 0.5 3.8 22.7 0.641 0.529 0.003 0.020 0.006 0.006 0.005   10 nd nd 74.6 nd 1.0 nd nd 16.1 nd 0.185 0.001 nd 0.006 nd 0.006   11 nd nd 79.3 nd 1.1 nd nd 16.1 nd 0.108 nd nd 0.006 nd 0.006   12 2.9 63.2 2.8 nd 0.3 3.8 23.0 0.518 0.550 nd 0.002 0.006 0.006   13 2.1 2.9 63.2 2.8 nd 0.3 nd 0.5 8.6 1.282 1.959 0.002 nd 0.000 0.001 0.007   14 nd 1.0 69.7 nd 0.3 nd 0.5 8.6 1.282 1.959 0.002 nd 0.000 0.001 0.007   10 0.001 | 2 nd nd 74.8 nd 0.8 nd nd 15.8 nd 0.183 nd nd 0.006 nd 0.006 3 3 6.06 2.3 2.6 nd 3.9 25.8 0.598 1.132 0.007 0.021 0.124 0.004 0.063 4 4 9 22.7 0.091 1.165 0.007 0.023 nd 0.004 0.041 0.041 0.02 0.003 nd 0.041 0. | 2         nd         nd         15.8         nd         0.183         nd         0.006         nd         0.006           3         2.5         nd         15.8         nd         0.183         nd         nd         0.006         nd         0.006         nd         0.006         nd         0.006         nd         0.006         nd         0.004         0.007         0.001         0.012         0.004 | 2 nd nd 74,8 nd 0,8 nd nd 15,8 nd 0,183 nd nd 0,006 nd 0,006 nd 0,006 3 3 nd 2,3 2,6 nd 3,9 25,8 0,598 1,132 0,007 0,021 0,124 0,004 0,004 0,004 1,9 2,27 0,091 1,165 0,007 0,023 nd 0,004 0,004 0,004 1,0 1,9 65,3 1,7 0,6 nd 4,9 2,27 0,091 1,165 0,007 0,023 nd 0,004 0,004 1,0 1,0 1,2 nd 1,0 1,2 nd 1,0 1,2 nd 1,0 1,2 nd 1,0 nd 1,0 nd 1,1 nd nd 1,1 nd nd 1,1 nd | 2 nd nd 74,8 nd 0,8 nd nd 15,8 nd 0,183 nd nd 0,000 nd 0,0006 nd 0,0006 | 2         nd         nd         15.8         nd         0.183         nd         0.06         nd         0.00         nd         0.00           3         nd         2.3         6.66         2.3         2.6         nd         3.9         25.8         0.598         1.132         0.007         0.021         0.124         0.004         0.004           4         nd         1.9         65.3         1.7         0.6         nd         4.9         2.2         0.099         1.136         0.007         0.021         0.004         0.004           5         nd         2.2         2.2         0.099         1.136         0.007         0.020         0.010         0.004         0.004           6         nd         1.0         0.4         3.2         2.28         0.797         1.34         0.01         0.01         0.023         0.01         0.004         0.041           7         nd         1.0         0.4         3.2         2.2         0.64         0.797         1.34         0.01         0.01         0.01         0.01         0.01         0.001         0.001         0.001         0.001         0.001         0.001         0.001 <td< th=""><th>2         nd         nd         15.8         nd         0.183         nd         0.08         nd         0.08         nd         0.08         nd         0.08         nd         0.09         0.02         0.021         0.124         0.004         0.041           4         nd         2.3         6.6         2.3         2.6         nd         4.9         22.7         0.091         1.165         0.007         0.023         nd         0.004         0.0041           4         nd         2.2         0.091         1.165         0.091         1.165         0.007         0.002         0.004         0.0041           5         nd         2.4         58.3         1.1         1.0         0.4         3.2         2.28         0.797         1.13         0.010         0.004         0.041           7         nd         1.0         nd         4.9         2.2         0.091         0.015         0.004         0.041           8         nd         1.0         nd         1.0         nd         1.0         0.041         0.052         0.020         0.001         0.001         0.001           9         nd         1.0         nd</th><th>2         nd         nd         748         nd         0.8         nd         15.8         nd         15.9         0.04         0.04         0.04         0.04           4         nd         1.2         6.6         2.3         2.6         nd         4.9         2.9         0.991         1.165         0.007         0.023         nd         0.041           5         nd         2.4         6.6         2.2         1.6         nd         4.9         2.9         0.091         1.165         0.007         0.023         0.01         0.041           6         nd         2.4         1.6         nd         1.6         nd         4.9         2.2         0.091         1.165         0.007         0.002         0.004         0.041           7         nd         1.0         nd         1.6         nd         4.9         2.2         0.641         0.529         0.010         0.025         0.010         0.004         0.041           8         nd         1.2</th><th>2         nd         nd         nd         nd         158         nd         0183         nd         000         nd         19         25.8         0.588         1;132         0.007         0.013         0.114         0.004         0.004         0.004           4         nd         12.9         12.0         0.089         1;132         0.007         0.013         0.114         0.004         0.004           5         nd         12.9         12.9         0.299         1;134         0.010         0.003         0.004         0.004           7         nd         10         nd         4.9         22.7         0.644         0.25         0.007         0.010         0.004         0.004           8    
    nd         12         nd         16         nd         16         0.79         13.14         0.010         0.004         0.004           9         nd         12         23         22.9         0.534         0.023         0.010         0.00</th><th>2         nd         nd         748         nd         0.8         nd         158         nd         158         nd         0.183         nd         0.00         nd         0.00         nd         0.00         0.00         nd         0.00         0.0</th><th>2         nd         nd         748         nd         0.8         nd         158         nd         158         nd         0.183         nd         0.00         nd         0.00         nd         0.00         0.00         nd         0.00         0.0</th><th>2         nd         nd         748         nd         0.8         nd         15.8         nd         16.83         nd         0.08         nd         0.09         0.15.0         nd         0.09         0.014         0.007</th><th>2         nd         nd         18         nd         158         nd         183         nd         183         nd         108         nd         158         nd         1132         0.007         0.014         0.005         nd         123         258         0.598         1132         0.007         0.014         0.003         nd         0.004&lt;</th><th>2         nd         148         nd         0.8         nd         158         nd         0.183         nd         0.00</th><th>2         nd         748         nd         0.88         nd         158         nd         0.183         nd         0.007         0.002         nd         0.006         0.007         0.002         nd         0.007         0.002         nd         0.004         0.008         nd         0.007         0.002         nd         0.004         0.008         nd         0.007         0.008         nd         0.008         0.008         0.007         0.001         0.004         <t< th=""><th>2         nd         748         nd         0.8         nd         158         nd         0.83         nd         168         nd         0.89         nd         198         0.00         11.32         0.007         0.001         1.15         0.00         0.004         0.00         0.003         nd         0.00         0.004         0.003         nd         0.00         0.004         1.15         0.004         0.004         0.004         0.003         0.004         0.0</th><th>2         nd         748         nd         0.8         nd         158         nd         0.83         nd         0.00</th><th>2         nd         148         nd         0.8         nd        
158         nd         0.183         nd         0.004         0.005         nd         0.004         0.005           3         nd         123         6.66         2.2         2.6         nd         3.9         2.8         0.098         1.132         0.007         0.013         nd         0.004         0.004           5         nd         2.2         6.66         2.0         1.6         nd         4.9         2.2         0.098         1.13         0.001         0.003         0.004         0.004         0.004           6         nd         2.2         6.6         2.0         1.6         nd         4.9         2.2         0.098         1.13         0.004</th><th>748         nd         0.88         nd         158         nd         0.183         nd         0.00</th></t<></th></td<> | 2         nd         nd         15.8         nd         0.183         nd         0.08         nd         0.08         nd         0.08         nd         0.08         nd         0.09         0.02         0.021         0.124         0.004         0.041           4         nd         2.3         6.6         2.3         2.6         nd         4.9         22.7         0.091         1.165         0.007         0.023         nd         0.004         0.0041           4         nd         2.2         0.091         1.165         0.091         1.165         0.007         0.002         0.004         0.0041           5         nd         2.4         58.3         1.1         1.0         0.4         3.2         2.28         0.797         1.13         0.010         0.004         0.041           7         nd         1.0         nd         4.9         2.2         0.091         0.015         0.004         0.041           8         nd         1.0         nd         1.0         nd         1.0         0.041         0.052         0.020         0.001         0.001         0.001           9         nd         1.0         nd | 2         nd         nd         748         nd         0.8         nd         15.8         nd         15.9         0.04         0.04         0.04         0.04           4         nd         1.2         6.6         2.3         2.6         nd         4.9         2.9         0.991         1.165         0.007         0.023         nd         0.041           5         nd         2.4         6.6         2.2         1.6         nd         4.9         2.9         0.091         1.165         0.007         0.023         0.01         0.041           6         nd         2.4         1.6         nd         1.6         nd         4.9         2.2         0.091         1.165         0.007         0.002         0.004         0.041           7         nd         1.0         nd         1.6         nd         4.9         2.2         0.641         0.529         0.010         0.025         0.010         0.004         0.041           8         nd         1.2 | 2         nd         nd         nd         nd         158         nd         0183         nd         000         nd         19         25.8         0.588         1;132         0.007         0.013         0.114         0.004         0.004         0.004           4         nd         12.9         12.0         0.089         1;132         0.007         0.013         0.114         0.004         0.004           5         nd         12.9         12.9         0.299         1;134         0.010         0.003         0.004         0.004           7         nd         10         nd         4.9         22.7         0.644         0.25         0.007         0.010         0.004         0.004           8         nd         12         nd         16         nd         16         0.79         13.14         0.010         0.004         0.004           9         nd         12         23         22.9         0.534         0.023         0.010         0.00 | 2         nd         nd         748         nd         0.8         nd         158         nd         158         nd         0.183         nd         0.00         nd         0.00         nd         0.00         0.00         nd         0.00         0.0 | 2         nd         nd         748         nd         0.8         nd         158         nd         158         nd         0.183         nd         0.00         nd         0.00         nd         0.00         0.00         nd         0.00         0.0 | 2         nd         nd         748         nd         0.8         nd         15.8         nd         16.83         nd         0.08         nd         0.09         0.15.0         nd         0.09         0.014         0.007 | 2         nd         nd         18         nd         158         nd         183         nd         183         nd         108         nd         158         nd         1132         0.007         0.014         0.005         nd         123         258         0.598         1132         0.007         0.014         0.003         nd         0.004        
0.004         0.004         0.004         0.004         0.004         0.004         0.004         0.004         0.004         0.004         0.004< | 2         nd         148         nd         0.8         nd         158         nd         0.183         nd         0.00 | 2         nd         748         nd         0.88         nd         158         nd         0.183         nd         0.007         0.002         nd         0.006         0.007         0.002         nd         0.007         0.002         nd         0.004         0.008         nd         0.007         0.002         nd         0.004         0.008         nd         0.007         0.008         nd         0.008         0.008         0.007         0.001         0.004 <t< th=""><th>2         nd         748         nd         0.8         nd         158         nd         0.83         nd         168         nd         0.89         nd         198         0.00         11.32         0.007         0.001         1.15         0.00         0.004         0.00         0.003         nd         0.00         0.004         0.003         nd         0.00         0.004         1.15         0.004         0.004         0.004         0.003         0.004         0.0</th><th>2         nd         748         nd         0.8         nd         158         nd         0.83         nd         0.00</th><th>2         nd         148         nd         0.8         nd         158         nd         0.183         nd         0.004         0.005         nd         0.004         0.005           3         nd         123         6.66         2.2         2.6         nd         3.9         2.8         0.098         1.132         0.007         0.013         nd         0.004         0.004           5         nd         2.2         6.66         2.0         1.6         nd         4.9         2.2         0.098         1.13         0.001         0.003         0.004         0.004         0.004           6         nd         2.2         6.6         2.0         1.6         nd         4.9         2.2         0.098         1.13         0.004</th><th>748         nd         0.88         nd         158         nd         0.183         nd         0.00</th></t<> | 2         nd         748         nd         0.8         nd         158         nd         0.83         nd         168         nd         0.89         nd         198         0.00         11.32         0.007         0.001         1.15         0.00         0.004         0.00         0.003         nd         0.00         0.004         0.003         nd         0.00         0.004         1.15         0.004         0.004         0.004         0.003         0.004         0.0 | 2         nd         748         nd         0.8         nd         158         nd         0.83         nd         0.00 | 2         nd         148         nd         0.8         nd         158         nd         0.183         nd         0.004         0.005         nd         0.004         0.005           3         nd         123         6.66         2.2         2.6     
   nd         3.9         2.8         0.098         1.132         0.007         0.013         nd         0.004         0.004           5         nd         2.2         6.66         2.0         1.6         nd         4.9         2.2         0.098         1.13         0.001         0.003         0.004         0.004         0.004           6         nd         2.2         6.6         2.0         1.6         nd         4.9         2.2         0.098         1.13         0.004 | 748         nd         0.88         nd         158         nd         0.183         nd         0.00 |

$ZrO_2$	900'0	0.012	910.0	0.035	0.027	0.007	0.017	0.01	0.002	0.009	900.0	0.002	0.002	0.027	0.015	0.010	0.015	0.029	0.002	0.005	0.036	0.003	0.003	0.015	0.002	0.027	0.002	0.034	0.028	0.014	0.003	0.033
SrO	0.002	0.028	0.046	0.065	0.077	0.052	0.007	0.043	0.007	0.040	0.009	9000	0.007	0.082	0.007	0.085	900.0	0.080	900.0	0.194	0.063	9000	900.0	0.08	0.007	0.080	0.007	0.065	0.079	0.004	0.007	0.064
$Rb_2O$	pu	0.015	0.004	0.004	0.003	0.022	0.00	0.004	pu	0.004	pu	pu	pu	0.004	0.00	0.002	0.00	0.003	pu	0.00	0.004	pu	pu	0.003	pu	0.004	pu	0.004	0.003	0.00	pu	0.004
$As_2O_3$	pu	0.087	0.030	901.0	0.186	0.034	0.019	pu	0.005	pu	0.084	pu	9000	0.123	0.022	pu	0.022	0.193	0.008	901.0	0.118	pu	pu	pu	pu	0.165	0.007	0.14	0.173	pu	0.007	0.110
ZnO	910.0	0.036	0.022	0.025	0.029	0.043	pu	0.023	pu	0.018	pu	pu	pu	0.028	pu	0.003	0.00	0.030	pu	0.005	0.021	pu	pu	0.025	pu	0.026	pu	0.023	0.028	pu	pu	0.023
CnO	0.143	0.009	9000	0.012	0.008	0.013	pu	0.010	pu	0.002	pu	pu	pu	0.007	pu	pu	0.00	0.011	0.002	0.003	0.013	pu	pu	0.007	pu	0.011	pu	0.010	0.015	pu	pu	0.011
$Fe_2O_3$	0.025	0.498	1.277	1.130	1.328	699.0	2.047	1.318	0.174	0.994	0.136	0.170	961.0	1.466	1.962	0.638	1.905	1.373	0.181	0.838	1.129	0.184	0.194	1.449	0.195	1.348	0.192	1.180	1.355	0.157	0.195	1.172
MnO	pu	0.796	0.181	0.568	0.788	0.885	1.399	0.097	pu	0.058	pu	pu	pu	0.802	1.375	pu	1.407	0.791	pu	0.005	0.594	pu	pu	0.180	pu	0.815	pu	0.580	0.835	pu	pu	0.587
CaO	5.6	16.9	23.8	26.3	21.3	20.8	0.6	24.0	15.9	24.2	15.7	16.3	16.4	24.2	8.9	9.01	8.8	22.0	16.5	17.6	26.5	16.0	16.3	23.3	16.2	23.2	15.5	26.1	22.3	8.0	16.3	26.8
$K_2O$	3.2	7.8	5.1	4.0	3.0	8.9	0.5	5.6	pu	4.9	pu	pu	pu	3.6	0.5	4.3	0.5	3.2	pu	2.1	4.	pu	pu	4.6	pu	3.4	pu	4.	3.–	0.7	pu	4.0
D	0.5	0.5	pu	pu	0.5	0.5	pu	pu	pu	pu	pu	pu	pu	0.3	pu	0.5	pu	9.0	pu	0.5	pu	pu	pu	0.3	pu	9.0	pu	pu	0.5	pu	pu	pu
SO3	pu	3.2	3.9	4.0	0.7	31.6	0.3	0.7	6.0	0.7	0.5	6.0	6.0	0.5	0.3	0.3	0.2	0:	6.0	1.2	4.0	0.8	6.0	6.0	6.0	5.1	0.8	2.3	0.9	pu	6.0	9.0
$P_2O_5$	pu	3.7	2.8	2.1	3.6	2.7	pu	2.1	pu	6:	pu	pu	pu	2.1	pu	pu	pu	3.6	pu	3.4	2.2	pu	pu	2.4	pu	2.8	pu	2.2	3.	pu	pu	2.2
$SiO_2$	78.1	49.2	65.2	66.2	56.3	26.5	75.9	71.4	79.1	68.3	78.1	7.97	78.8	69.2	75.9	76.2	75.3	61.7	78.3	63.4	67.8	76.8	80.4	65.5	78.0	8.19	75.4	62.2	8.09	78.7	9.87	65.4
$Al_2O_3$	pu	<u> </u>	2.8	2.6	6:1	9.0	=	2.3	pu	2.7	pu	pu	pu	2.8	<u> </u>	=	0.	2.4	pu	1.5	2.7	pu	pu	2.6	pu	2.5	pu	2.7	2.4	<u>-</u> .	pu	2.7
MgO	pu	2.5	2.1	2.3	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.6	pu	2.2	pu	pu	pu	pu	pu	2.8	pu	pu						
Ь	5	9	_	∞	6	0	=	12	<u>~</u>	4	15	91	17	<u>∞</u>	61	20	21	22	23	24	25	26	27	28	_	2	$\sim$	4	2	9	7	∞
<b>*</b>	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.2	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3

$ZrO_2$	0.002	0.017	0.017	0.002	0.010	0.015	0.019	0.015	0.002	0.027	0.034	0.002	0.003	0.018	0.003	0.019	0.033	0.002	0.012	0.002	0.01	0.013	0.020	0.002	0.005	0.004	0.032	0.027	0.003	0.002	0.008	0.002
SrO	0.007	0.007	0.065	0.007	0.117	0.037	0.058	0.044	9000	0.078	0.060	0.007	0.007	0.054	0.007	0.054	0.064	0.007	0.029	9000	0.039	0.112	0.055	0.007	0.191	0.002	0.063	0.079	0.007	0.007	0.189	0.007
$Rb_2O$	pu	0.00	0.004	pu	0.00	0.005	0.002	0.012	pu	0.003	0.003	pu	pu	0.003	pu	0.003	0.004	pu	0.013	pu	0.004	0.00	0.003	pu	0.00	pu	0.004	0.003	pu	pu	0.00	pu
$As_2O_3$	pu	0.020	0	pu	pu	0.033	0.010	0.008	9000	0.177	0.143	0.005	0.007	pu	0.007	pu	0.149	9000	0.053	pu	pu	0.056	0.015	900'0	0.010	pu	0.167	0.118	pu	900'0	0.053	pu
ZnO	pu	0.00	0.027	pu	0.010	0.019	0.027	0.028	pu	0.025	0.020	pu	pu	0.018	pu	0.021	0.023	pu	0.030	pu	0.019	910.0	0.023	pu	0.003	0.00	0.021	0.029	pu	pu	0.003	0.002
CnO	pu	pu	0.009	pu	0.005	0.013	0.003	0.024	pu	0.007	0.012	pu	pu	pu	pu	0.00	0.009	pu	0.009	pu	0.007	0.003	0.003	pu	pu	pu	0.009	0.009	pu	pu	pu	pu
$Fe_2O_3$	0.165	1.903	1.176	0.172	0.938	0.839	0.613	0.603	0.175	1.288	1.147	0.184	0.198	0.540	0.162	0.578	1.22.1	0.189	0.462	0.199	1.042	0.781	0.598	0.187	0.884	0.126	1.153	1.442	0.193	0.192	0.850	0.195
MnO	pu	1.345	1.009	pu	0.105	0.782	0.593	0.727	pu	0.808	0.547	pu	pu	0.593	pu	0.565	0.594	pu	0.713	pu	0.082	0.746	0.579	pu	0.017	pu	0.563	0.850	pu	pu	0.003	pu
CaO	1.91	8.5	22.5	16.4	21.9	18.7	24.5	16.3	16.9	25.0	25.0	16.2	16.2	22.5	16.7	22.3	25.8	16.4	17.4	16.3	22.7	23.6	22.7	15.8	19.3	8.0	24.2	23.6	16.5	16.0	18.5	15.8
$K_2O$	pu	0.5	4.3	pu	2.3	5.7	3.8	8.5	pu	2.9	3.7	pu	pu	3.8	pu	3.7	3.7	pu	7.1	pu	5.2	2.6	3.6	pu	2.3	pu	3.5	3.7	pu	pu	2.2	pu
D	pu	pu	0.3	pu	0.3	0.2	0.5	9.0	pu	9.0	0.2	pu	pu	0.5	pu	0.5	0.2	pu	9.0	pu	pu	0.3	9.0	pu	0.3	pu	0.2	0.3	pu	pu	0.5	pu
SO3	6.0	0.2	0.3	6.0	=:	4.9	0.3	9.0	6.0	7.4	6.3	6.0	6.0	pu	0.8	pu	5.3	6.0	19.9	6.0	0.5	3	1.7	0.8	0.5	0.2	7.5	0.5	6.0	6.0	7.3	6.0
$P_2O_5$	pu	pu	2.7	pu	pu	2.3	3.0	3.8	pu	3.0	3.	pu	pu	2.7	pu	2.7	2.9	pu	2.6	pu	2.1	2.0	2.8	pu	pu	pu	3.2	<u>∞</u> .	pu	pu	2.4	pu
$SiO_2$	75.7	69.7	65.3	1.08	65.5	62.0	1.19	66.5	77.3	57.2	9.09	76.5	79.5	9.99	7.97	9.59	62.6	9.62	20.0	75.7	71.3	9.59	9.89	74.2	74.9	74.8	55.6	65.0	75.3	75.2	8.99	74.0
$Al_2O_3$	pu	6.0	3.0	0.5	1.5	3.9	3.	6:1	pu	2.6	2.4	pu	pu	3.2	pu	3.3	2.6	pu	9.1	pu	2.4	2.3	3.2	pu	9.1	9.0	2.2	2.4	pu	pu	1.7	pu
MgO	pu	pu	<u>~</u> .	pu	2.2	2.3	2.1	4.9	pu	pu	2.2	pu	pu	2.2	pu	2.0	pu	pu	3.2	pu	pu	pu	2.3	pu	2.7	pu	pu	pu	pu	pu	2.4	pu
Ь	6	0	=	12	<u></u>	<u>+</u>	15	91		<u>8</u>	6	20	_	2	$\sim$	4	2	9	7	∞	6	0	=	12	<u>_3</u>	4	15	9		<u>&amp;</u>	6	20
<b>*</b>	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.3	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4	w42.4

$2^{1}$	0.024	0.01	0.021	0.025	0.024	0.002	0.020	0.003	0.026	0.026	0.023	0.01	0.026	0.025	0.021	0.003	0.01	0.025	0.012	0.023	0.017	0.022	0.008	0.007	0.026	0.024	910.0	0.009	910.0	0.021	0.023	0.012
Š	990'0	0.029	0.049	0.052	0.067	910.0	0.054	0.010	0.051	0.052	0.065	0.114	0.054	0.089	0.065	0.009	0.028	0.053	0.122	0.064	960.0	0.064	0.003	0.012	0.053	990.0	0.076	0.135	0.091	0.050	0.065	0.084
<sub>2</sub> О	0.003	0.015	0.002	0.005	0.004	pu	0.002	0.00	0.005	0.005	0.005	0.00	0.005	0.004	0.003	pu	0.014	0.004	0.00	0.004	0.002	0.004	0.003	pu	0.005	0.004	0.002	0.00	0.002	0.002	0.004	0.002
$As_2O_3$	0.087	0.074	pu	0.118	0.074	pu	900.0	0.407	0.118	0.113	0.073	pu	0.107	0.107	0.062	0.384	0.020	0.109	pu	0.064	pu	0.057	pu	0.250	0.119	0.070	pu	900.0	0.007	pu	0.073	pu
ZnO	0.029	0.035	0.030	0.018	0.028	pu	0.028	0.00	0.021	0.026	0.028	0.012	0.023	0.029	0.030	pu	0.033	0.025	0.012	0.027	0.023	0.030	0.030	0.002	0.025	0.027	0.023	0.01	0.023	0.027	0.031	0.005
9	0.012	0.009	0.00	0.008	0.013	pu	0.003	pu	0.008	0.012	0.012	pu	0.009	0.009	0.010	pu	0.014	0.011	0.004	0.010	0.009	900'0	0.002	0.001	0.007	0.013	0.008	pu	0.005	0.004	0.017	pu
$F_2O_3$	1.082	0.479	1.079	1.230	1.052	0.181	0.956	0.130	1.161	1.243	 	1.182	1.276	1.080	0.988	0.117	0.587	1.227	1.218	1.026	1.614	1.014	0.00	0.246	1.234	1.08	1.617	0.910	1.472	0.939	1.090	0.519
Ω	0.790	0.751	0.568	0.587	0.787	pu	0.536	pu	0.597	0.639	0.746	0.081	909.0	0.749	0.758	pu	0.871	919.0	0.072	0.776	0.187	0.734	pu	0.321	0.599	0.687	0.161	0.179	0.191	0.613	0.721	pu
S	25.1	17.5	23.2	24.2	25.9	17.2	24.0	16.7	24.3	24.6	25.7	22.6	23.8	23.6	24.9	16.5	14.9	23.9	23.0	25.4	22.8	25.6	6.7		24.0	25.5	22.9	23.9	21.9	22.9	24.3	10.7
х О	4.1	7.7	2.2	4.8	4.3	0.0	<u>.</u> 5	0.3	4.9	5.3	4.3	2.1	5.1	5.4	4.2	0.3	9.4	4.8	2.1	4.3	4.	4.4	3.7	pu	5.2	4.2	3.9	2.8	4.	2.1	3.9	8.9
Ū	pu	4.0	0.7	pu	pu	pu	0.7	pu	pu	pu	pu	4.0	pu	pu	pu	pu	0.5	pu	9.0	pu	9.0	pu	6.0	pu	pu	pu	0.3	0.7	4.0	0.7	pu	9.4
Š	0.8	3.0	0.2	0.5	0.7	6.0	0.2	<u></u>	6.0	0.7	0.7	=	0.7	0.8	0.8	4.	3.4	0.8	Ξ	9.0	0.8	9.0	pu	0.8	<u>~</u>	9.0	6.0	9.0	1.2	pu	0.8	9.0
P <sub>2</sub> O <sub>5</sub>	2.5	2.5	2.8	2.5	2.8	pu	2.1	pu	2.6	2.6	2.9	<u></u>	2.8	2.7	3.0	pu	4.2	2.4	4.	2.8	2.9	3.2	pu	pu	2.8	2.9	2.6	<u>∞</u> .	2.6	3.0	2.6	pu
SiO <sub>2</sub>	29.9	68.5	77.2	80.2	79.9	8.86	79.8	92.7	81.7	79.2	81.2	84.7	81.3	81.4	79.0	96.2	70.9	73.8	82.6	80.3	82.9	81.7	95.0	94.2	76.8	78.8	83.3	82.7	80.0	78.4	78.2	85.5
$A_2O_3$	2.8	2.0	5.9	3.5	3.2	0.7	5.1	0.	3.	3.6	3.2	3.5	3.8	3.2	3.0	6.0	2.6	3.	3.3	3.	4.4	3.	pu	0.8	3.4	2.7	4.4	2.1	4.2	4.8	2.8	9:1
Q Σ	3.2	4.8	4.	3.6	3.5	pu	3.7	pu	3.4	4.	3.5	3.4	4.0	4.0	3.3	pu	7.5	2.9	3.4	3.7	4.4	3.9	pu	pu	3.9	3.3	3.5	3.9	3.9	4.0	3.0	3.8
<u>a</u>	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	15	9	17	<u>∞</u>	6	20	21	22	23	24	25	26	27	28	29	30	3	32
≥	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.1	w43.I	w43.1	w43.1	w43.1	w43.1

$\frac{1}{2}$	0.022	0.012	0.018	0.024	0.01	0.007	0.012	0.008	0.023	0.008	0.012	0.002	0.003	0.002	0.002	0.002	0.003	0.002	0.010	0.002	0.002	0.002	0.002	0.011	0.002	900'0	0.002	0.008	0.002	0.011	0.010	0.002
Š	990.0	0.012	0.097	0.092	0.029	0.026	0.027	0.114	0.092	0.176	0.030	0.012	0.012	0.01	0.009	0.009	0.009	0.007	0.014	0.009	0.009	0.009	0.007	910.0	0.012	0.003	0.012	0.002	0.013	0.015	0.012	0.012
<sub>2</sub> О	0.004	pu	0.002	0.004	0.015	910.0	0.017	0.00	0.005	0.00	0.015	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	0.00	pu	0.003	pu	0.00	0.001	pu
$As_2O_3$	0.065	0.408	0.005	901.0	0.007	0.039	910.0	0.021	0.104	900'0	0.030	0.062	0.063	0.073	0.056	0.057	0.058	pu	pu	0.062	0.047	0.049	pu	pu	0.068	pu	0.067	pu	0.070	pu	pu	0.064
ZnO	0.030	0.010	0.026	0.029	0.029	0.028	0.035	0.01	0.029	900'0	0.032	pu	pu	pu	0.00	0.002	pu	pu	0.00	0.00	pu	0.002	pu	pu	pu	2.550	0.00	1.163	pu	pu	0.002	0.00
9	0.015	pu	900'0	0.010	0.009	0.004	0.008	pu	0.010	0.00	0.010	0.040	0.038	0.037	0.047	0.042	0.046	pu	pu	0.037	0.043	0.038	pu	pu	0.04	pu	0.039	pu	0.045	0.001	pu	0.037
$F_2O_3$	1.059	0.190	1.614	1.089	0.463	0.302	0.500	1.002	1.104	960'1	0.537	0.480	0.425	0.431	0.436	0.470	0.408	0.177	0.065	0.427	0.407	0.424	0.190	0.065	0.427	0.025	0.426	0.010	0.469	0.061	0.064	0.432
δ O	0.791	pu	0.179	0.785	0.915	0.942	0.908	0.052	0.721	0.036	0.889	0.079	0.062	990'0	0.109	0.084	0.065	pu	pu	690'0	0.076	0.084	pu	pu	0.031	pu	0.074	pu	0.090	0.012	0.004	0.085
S S	25.5	13.4	22.8	24.5	15.2	15.6	14.9	25.5	24.7	21.2	17.1	15.5	14.8	15.2	14.5	14.4	14.6	18.4	8.5	14.8	13.8	14.2	16.8	9.1	14.9	8.5	15.5	9.9	15.1	9.0	8.7	14.8
K O	4.2	pu	4.0	5.6	6.6	8.7	6.6	1.7	5.5	2.2	9.2	0.2	0.2	0.2	0.	0.2	0.2	pu	0.3	0.2	0.2	0.2	pu	0.3	0.2	0.8	0.2	3.3	0.2	0.3	0.3	0.2
Ō	pu	pu	4.0	pu	0.5	0.5	0.5	0.5	pu	9.0	0.5	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	9.0	pu	pu	pu	pu
Š	0.7	6.0	6.0	9.1	0.8	0.8	<u>8.</u>	3.3	6.0	0.7	4.0	0.8	6.0	0.8	0.8	0.8	0.8	1.2	0.3	0.7	0.8	0.8	0.	0.3	0.8	6.0	6.0	0.8	0.8	0.3	0.3	0.8
P <sub>2</sub> O <sub>5</sub>	2.9	pu	2.8	2.9	3.8	4.4	4.0	9.	2.5	=:	3.7	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	79.3	96.4	85.0	82.7	75.6	74.5	75.9	80.2	77.1	85.7	74.0	94.5	88.4	88.9	90.3	6.06	92.1	99.3	9.88	868	9.06	868	86.5	6'86	4.16	93.7	93.3	94.0	8.06	8.96	94.6	9.06
$A_2O_3$	3.2	0.7	4.7	3.4	2.4	<u>4</u> .	6:1	2.8	2.7	2.9	2.5	0.8	6.0	0.7	0.8	0.7	0.7	6.0	<u></u>	0.8	0.7	0.7	pu	2.0	0.8	pu	6.0	pu	6.0	8.	9.1	<u>-</u> :
Q Σ	3.4	pu	4.9	4.2	8.0	8.4	8.2	2.7	3.4	4.4	8.7	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
ட	33	34	35	36	37	38	39	40	4	42	43	_	2	$\sim$	4	2	9	7	8	6	0	=	12	<u>~</u>	4	15	9		<u>8</u>	6	20	21
≯	w43.1	w43.I	w43.1	w43.I	w43.I	w43.I	w43.I	w43.1	w43.1	w43.I	w43.1	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2	w43.2

$2rO_2$	0.004	0.002	0.003	0.024	0.003	0.025	0.013	0.003	0.003	0.01	0.014	0.004	0.009	0.003	0.003	0.003	0.01	0.003	0.003	0.004	0.011	0.005	0.002	0.01	0.005	0.003	0.005	0.003	0.003	0.005	0.017	0.002
SrO	0.002	0.009	0.009	990.0	0.009	0.05	0.039	0.013	0.009	0.129	0.039	0.002	0.012	0.009	0.010	0.009	910.0	0.009	0.009	0.002	910.0	0.002	0.009	910.0	0.002	0.009	0.002	0.01	0.009	0.002	0.099	0.009
$Rb_2O$	0.004	pu	pu	0.004	pu	0.005	0.011	0.00	pu	0.002	0.012	0.004	0.00	pu	pu	pu	0.00	pu	pu	0.004	0.00	0.003	pu	0.00	0.004	pu	0.004	pu	pu	0.003	0.003	pu
$As_2O_3$	pu	0.052	0.054	0.077	0.053	0.113	0.062	0.076	0.053	pu	0.010	pu	pu	0.058	0.054	0.055	pu	0.057	0.053	pu	900.0	pu	0.056	pu	pu	0.059	pu	0.056	0.046	pu	pu	0.052
ZnO	610.0	0.00	pu	0.027	0.00	0.027	0.029	pu	pu	0.011	0.034	0.020	pu	pu	0.00	pu	pu	pu	pu	0.019	0.001	0.020	pu	pu	0.021	pu	0.019	pu	0.00	0.021	0.025	0.00
CnO	0.029	0.040	0.033	0.011	0.041	0.011	0.031	0.044	0.044	900'0	0.035	pu	pu	0.049	0.048	0.042	pu	0.036	0.040	0.028	pu	pu	0.041	0.002	0.023	0.040	pu	0.047	0.043	pu	0.007	0.051
$Fe_2O_3$	pu	0.450	0.445	1.105	0.429	1.211	0.718	0.455	0.44	1.040	0.573	0.004	0.048	0.432	0.463	0.464	0.065	0.440	0.397	0.003	0.079	pu	0.411	0.059	pu	0.478	pu	0.456	0.435	pu	1.671	0.454
MnO	pu	0.088	0.094	0.752	0.080	0.556	0.704	0.051	0.080	0.093	0.839	pu	0.010	0.062	0.099	0.091	pu	0.075	690'0	pu	0.012	pu	0.083	0.002	pu	0.101	pu	0.103	0.082	pu	0.193	0.104
CaO	5.1	14.5	14.5	25.7	14.5	23.7	14.8	15.9	14.6	23.5	1.91	5.0	8.8	14.8	15.5	14.6	8.7	14.6	14.5	5.1	8.9	4.9	14.3	8.7	4.9	14.9	2.0	1.91	14.6	5.1	23.8	15.0
$K_2O$	3.5	0.2	0.2	4.	0.2	4.7	7.4	0.2	0.2	2.8	6.6	4.2	0.3	0.2	0.2	0.2	0.3	0.2	0.2	3.4	0.3	4.	0.2	0.3	3.2	0.2	4.2	0.2	0.2	4.	4.2	0.2
Ū	0.5	pu	pu	pu	pu	pu	9.0	pu	pu	0.3	9.0	0.7	pu	pu	pu	pu	pu	pu	pu	9.0	pu	0.7	pu	pu	0.5	pu	0.8	pu	pu	0.8	0.3	pu
SO3	4.1	0.7	0.7	0.8	0.8	4.0	9.6	6.0	0.8	0:	0.7	pu	0.3	6.0	6.0	0.8	0.2	0.8	0.8	4.	0.3	pu	0.8	0.3	<u></u>	6.0	pu	Ξ	0.7	pu	1.2	0.8
$P_2O_5$	pu	pu	pu	2.9	pu	2.6	3.7	pu	pu	9:	4.7	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.7	pu
$SiO_2$	1.66	94.7	97.6	83.4	94.0	82.5	76.4	94.8	93.5	89.0	73.7	93.6	94.8	0.16	90.4	7.06	93.2	94.1	92.9	98.8	95.1	102.5	92.9	92.8	93.5	92.6	98.7	99.5	88.7	100.3	78.7	93.1
$Al_2O_3$	pu	6.0	6.0	3.0	0.	3.4	2.3	=	0.8	3.2	2.4	pu	<u> </u>	0.7	0.7	9.0	9:1	0.7	6.0	pu	2.2	pu	6.0	2.7	pu	0.8	pu	0.	0.8	pu	4.0	6.0
OgM	pu	pu	pu	4.0	pu	3.6	4.8	pu	pu	4.0	7.6	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	3.5	pu
Ь	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	12	9		<u>&amp;</u>	6	20	21	22	23	24	25	26	27	28	29	30	_	2
>	w44	44w	44 <sub>w</sub>	44w	44w	44w	44w	44w	44 <sub>w</sub>	44w	44w	w44	44 <sub>w</sub>	44w	44w	44w	44w	44w	44 <sub>w</sub>	44 <sub>w</sub>	44w	44w	44w	w44	44w	44w	₩ 44	w44	44w	44w	w45.1	w45.1

$ZrO_2$	0.002	0.005	0.003	0.013	0.022	0.020	0.014	0.015	0.002	0.012	0.007	0.023	0.025	9000	0.025	0.003	0.012	0.023	910.0	0.010	0.024	0.012	0.022	0.013	0.007	0.022	0.020	900.0	0.025	0.025	0.011	0.013
SrO	0.010	0.236	0.009	0.028	0.064	0.053	0.040	0.040	0.008	0.029	0.180	0.064	0.056	0.167	0.058	0.010	0.031	0.062	0.101	0.028	0.058	0.029	990.0	0.031	0.002	990.0	0.052	0.002	0.058	0.056	0.029	0.038
$Rb_2O$	pu	pu	pu	910.0	0.004	0.002	0.01	0.005	pu	0.015	0.00	0.004	0.005	0.00	0.005	pu	0.015	0.003	0.002	0.015	0.005	910.0	0.004	910.0	0.004	0.003	0.003	0.003	900'0	900'0	0.015	0.011
$As_2O_3$	0.058	0.011	0.055	0.012	0.057	pu	0.024	pu	0.054	0.012	pu	0.076	0.130	0.009	0.128	0.052	0.015	0.070	pu	0.029	0.135	pu	0.064	0.010	pu	0.078	0.120	pu	0.121	0.132	0.009	0.043
ZnO	0.002	0.004	pu	0.031	0.029	0.026	0.036	0.020	pu	0.035	0.008	0.030	0.025	900.0	0.019	0.002	0.041	0.028	0.014	0.031	0.023	0.036	0.031	0.035	0.00	0.030	0.024	0.003	0.027	0.025	0.034	0.032
CnO	0.041	pu	0.046	0.010	0.010	pu	0.035	0.009	0.037	0.009	pu	0.009	0.011	0.00	0.009	0.044	0.008	0.014	pu	0.007	0.012	0.012	0.011	0.010	0.003	0.013	0.007	0.005	0.010	0.014	900'0	0.031
$Fe_2O_3$	0.453	916.0	0.434	0.510	1.028	0.919	0.630	1.374	0.431	0.468	1.037	1.04	1.285	0.900	1.321	0.449	0.502	1.095	1.450	0.492	1.251	0.483	1.070	0.522	0.032	1.095	0.941	0.034	1.309	1.262	0.516	0.615
MnO	0.077	0.007	0.085	0.903	0.736	0.471	0.871	0.117	0.078	0.961	0.044	0.784	0.643	0.024	0.694	0.092	0.867	0.724	0.158	908.0	0.695	0.988	0.729	0.953	pu	0.739	0.712	pu	0.724	669.0	0.855	0.815
CaO	15.0	22.6	14.7	15.3	25.5	23.7	16.3	24.4	14.2	0.91	21.3	24.9	24.1	21.4	24.6	15.3	15.4	24.9	22.3	17.1	24.6	15.2	25.8	15.4	9.9	25.1	23.5	6.4	25.0	24.2	15.3	15.1
$K_2O$	0.2	2.2	0.2	6.6	4.5	9.1	6.6	5.6	0.2	0.01	2.3	4.0	5.2	2.0	5.7	0.2	1.01	4.3	3.3	8.5	5.5	10.4	4.2	<u> </u>	3.9	4.	0.9	3.9	5.7	5.6	6.6	9.2
Ū	pu	9.0	pu	9.0	pu	0.7	9.0	pu	pu	0.5	0.3	pu	pu	0.5	pu	pu	0.5	pu	0.5	0.3	pu	9.0	pu	9.4	0.7	pu	9.4	0.8	pu	pu	9.4	0.5
SO3	0.7	6.0	0.8	<u>.</u> 5	0.8	pu	0.7	0.	0.7	=:	0.7	<u>.</u> 5	0.7	9.0	0.5	0.8	2.2	0.8	pu	2.5	0.7	0.8	9.0	=:	pu	0:	0.7	pu	9.0	9.0	0.7	6.0
$P_2O_5$	pu	9:1	pu	4.2	3.0	2.4	4.9	2.4	pu	4.	0.	2.4	2.7	0:	2.8	pu	4.	3.0	2.4	3.5	2.9	4.	3.0	3.8	pu	2.8	3.0	pu	3.0	2.8	4.0	6.3
$SiO_2$	93.3	8.18	93.0	73.6	74.7	82.1	73.4	7.67	6.68	77.5	85.2	77.7	79.9	85.0	79.4	95.9	77.0	80.5	83.6	73.3	77.9	77.9	8.14	73.3	1.86	82.4	85.0	6.96	82.5	80.2	76.9	8.89
$Al_2O_3$	0.7	2.4	0.8	2.3	3.	5.2	2.8	4.2	0.8	2.5	2.9	<u>~</u> .	3.8	2.6	4.3	9.0	2.4	2.9	3.2	2.9	3.8	2.5	3.0	2.2	pu	3.8	3.0	pu	4.2	4.0	2.4	2.3
MgO	pu	5.6	pu	8.4	3.5	3.2	7.3	2.4	pu	9.0	4.4	2.9	4.5	4.	4.8	pu	8.2	3.6	3.9	6.9	4.	9.3	4.2	7.1	pu	4.2	4.0	pu	5.0	5.0	9.5	5.6
Ь	~	4	2	9	7	$\infty$	6	0	=	12	<u> </u>	4	15	91		<u>&amp;</u>	61	20	21	22	23	24	25	26	27	28	29	30	$\overline{\mathbb{S}}$	32	33	34
>	w45.1	w45.1	w45.1	w45.1	w45.I	w45.1	w45.1	w45.1	w45.I	w45.1	w45.I	w45.1	w45.1	w45.1	w45.1	w45.1	w45.1	w45.1	w45.I	w45.1	w45.1	w45.I	w45.I	w45.1	w45.I	w45.I	w45.1	w45.I	w45.I	w45.I	w45.1	w45.I

7	9	2	_	4	$\sim$	4	$\sim$	7	6	$\sim$	7	$\infty$	$\sim$	$\sim$	7	7	7	$\sim$	$\infty$	7	$\sim$	7	7	2	$\infty$	7	7	$\sim$	7	$\infty$	$\infty$	$\sim$
$ZrO_2$	00'0	0.0	0.02	0.02	0.00	0.02	0.02	0.00	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
S.	0.189	960.0	0.05	0.067	0.010	0.064	990.0	0.009	0.172	0.012	0.092	0.183	0.009	0.012	0.012	0.012	0.012	0.012	0.010	0.012	0.012	0.012	0.012	0.008	0.009	0.013	0.012	0.01	0.01	0.010	0.012	0.012
$Rb_2O$	0.001	0.002	0.003	0.003	pu	0.004	0.004	pu	0.00	pu	0.004	0.00	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.00	pu	pu	pu	pu	pu	pu	pu	pu
As <sub>2</sub> O <sub>3</sub>	pu	0.013	0.085	0.071	090.0	0.068	0.080	0.050	pu	0.070	0.091	0.005	0.059	0.071	0.068	0.068	690.0	0.075	0.058	0.068	0.074	0.075	0.072	pu	0.045	690.0	0.061	0.063	0.067	0.055	0.072	0.068
ZnO	0.004	910.0	0.019	0.029	0.00	0.031	0.031	pu	9000	pu	0.028	0.007	pu	0.00	0.002	0.002	0.002	pu	pu	0.00	pu	pu	pu	0.003	pu	0.00	pu	0.002	0.002	pu	pu	0.00
O <sub>D</sub>	pu	0.005	0.005	0.010	0.04	0.014	0.010	0.04	pu	0.038	0.01	0.00	0.04	0.042	0.045	0.037	0.039	0.044	0.038	0.04	0.038	0.040	0.036	pu	0.036	0.045	0.046	0.039	0.035	0.044	0.040	0.039
Fe <sub>2</sub> O <sub>3</sub>	0.885	1.257	0.860	1.086	0.446	1.107	1.092	0.416	1.442	0.498	1.125	1.098	0.446	0.423	0.468	0.446	0.489	0.456	0.465	0.443	0.411	0.472	0.468	0.184	0.468	0.470	0.462	0.430	0.438	0.44	0.442	0.464
MnO	0.033	0.198	0.677	0.747	0.067	0.767	0.725	0.092	0.030	0.062	0.706	0.043	0.088	0.067	0.093	0.085	0.103	0.088	0.094	980.0	0.104	0.093	690.0	pu	0.046	0.095	0.097	0.059	0.078	0.101	0.058	0.089
CaO	23.0	26.8	24.1	25.5	15.1	25.7	24.9	14.6	18.3	15.5	24.9	22.1	14.7	15.0	15.1	15.0	15.6	15.2	15.2	15.0	14.6	15.3	15.0	13.9	14.6	15.3	15.0	15.3	15.0	14.9	15.2	14.8
K <sub>2</sub> O	2.2	3.0	4.8	4.0	0.2	4.	4.2	0.0	2.6	0.2	5.7	2.3	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.5	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2
ō	9.0	9.0	pu	pu	pu	pu	pu	pu	4.0	pu	pu	9.0	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SO3	6.0	=:	0:	0.7	0.8	0.8	<u>~</u>	0.8	9.0	0.8	0:	0.8	0.8	0:	0.8	0:	0:	0.8	0.8	0.8	0.8	6.0	6.0	0.5	6.0	6.0	6.0	0:	0.8	0.8	0.8	6.0
P <sub>2</sub> O <sub>5</sub>		2.4	2.8	2.7	pu	2.8	2.9	pu	1.5	pu	2.7	1.2	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
SiO <sub>2</sub>	81.5	83.1	85.6	82.6	8.96	83.3	85.4	92.1	1.68	92.8	82.9	88.5	94.1	93.2	93.4	95.1	96.5	92.1	92.6	93.4	7.16	93.2	93.7	95.5	95.1	93.8	93.4	94.3	7.16	88.4	92.3	90.2
Al <sub>2</sub> O <sub>3</sub>	2.5	4.0	<u>.</u>	2.9	0:	3.5	3.7	0.7	3.7	0.8	3.4	3.0	0.7	0:	6.0	0:	Ξ.	6.0	0.7	6.0	6.0	0:	6.0	6.	0.7	0:	6.0	0:	6.0	0.7	6.0	6.0
OgM	4.4	4.2	3.5	3.8	pu	4.2	4.0	pu	4.8	pu	4.0	5.3	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ъ	35	36	37	38	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	<u>4</u>	15	9		<u>∞</u>	6	20	21	22	23	24	25	26	_	7
≯	w45.1	w45.1	w45.I	w45.1	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w45.2	w47.1	w47.1

1	i																															
$ZrO_2$	0.003	0.002	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.003	0.005	0.003	0.002	0.002	0.028	0.019	0.024	0.012	0.026	0.023	0.004	0.015	0.026	0.017	0.026	0.013	0.023	0.007	0.022	0.012	0.002	0.004
SrO	0.012	0.013	0.01	0.01	0.009	0.009	0.012	0.009	0.012	0.009	0.002	0.009	0.009	0.008	0.076	0.109	0.090	0.040	0.052	0.062	0.068	0.073	0.052	0.105	0.053	0.030	0.063	0.201	0.063	0.030	0.009	0.002
$Rb_2O$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.004	pu	pu	pu	0.003	0.002	0.004	0.004	0.005	0.004	0.00	0.003	0.005	0.002	0.005	0.015	0.003	0.00	0.004	0.015	pu	0.004
$As_2O_3$	0.070	690.0	0.068	990.0	0.052	0.055	0.070	0.061	0.064	0.050	pu	0.054	0.051	0.056	0.115	0.007	0.117	pu	0.129	0.050	0.342	0.013	0.113	pu	0.122	0.011	0.054	pu	0.059	0.017	0.062	pu
ZnO	0.002	pu	pu	pu	pu	pu	0.001	pu	0.002	0.00	0.022	0.00	pu	0.00	0.026	0.024	0.030	0.021	0.022	0.028	0.004	0.022	0.024	0.023	0.023	0.033	0.028	0.004	0.028	0.034	0.002	0.021
CnO	0.036	0.038	0.042	0.035	0.042	0.038	0.043	0.044	0.047	0.041	0.028	0.043	0.044	0.033	0.010	0.004	0.011	0.005	0.015	0.009	0.001	0.004	0.007	0.005	0.013	0.014	0.007	pu	0.012	0.008	0.040	0.027
$Fe_2O_3$	0.436	0.451	0.436	0.469	0.405	0.413	0.474	0.420	0.443	0.455	900.0	0.430	0.420	0.431	1.368	1.551	1.062	1.159	1.250	1.094	0.335	1.344	1.198	1.584	1.255	0.452	1.030	0.660	1.050	0.488	0.421	pu
MnO	0.098	0.070	0.072	0.075	0.084	0.088	980.0	0.082	0.105	0.075	pu	0.061	0.084	0.088	0.815	0.330	0.692	0.120	0.591	0.724	0.025	0.163	0.629	0.284	0.588	0.894	0.709	0.031	0.730	0.871	0.123	pu
CaO	14.8	15.9	- - -	14.7	4.	15.0	15.3	14.2	15.0	14.6	2.0	<u>4.</u> —.	14.7	4.4	24.1	22.0	24.4	24.6	24.4	25.8	6:11	24.9	23.8	21.6	24.0	15.6	25.8	22.0	25.6	15.3	4.4	5.1
$K_2O$	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	3.4	0.2	0.2	0.2	3.4	4.3	5.7	4.8	4.8	4.4	3.7	3.9	5.1	4.3	5.1	9.6	4.4	2.4	4.6	6.6	0.2	3.5
D	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.5	pu	pu	pu	9.0	0.5	pu	pu	pu	pu	0.8	0.3	pu	0.5	pu	0.5	pu	4.0	pu	0.5	pu	0.5
SO3	6.0	6.0	1.2	=:	0.7	0.7	6.0	0.8	6.0	6.0	<u>4</u> .	0.8	6.0	0.7	0:	6.0	2.5	0:	0.5	9.0	pu	2.0	9.0	0.8	<u></u>	6.	0.5	0.8	9.0	2.2	6.0	4.
$P_2O_5$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.2	2.9	2.7	2.3	2.8	3.3	pu	2.4	2.5	3.0	2.7	4.3	3.3	=	3.3	4.4	pu	pu
$SiO_2$	216	0.76	89.2	88.4	88.7	92.6	96.2	0.16	93.5	94.1	95.2	93.5	94.4	0.68	77.4	8.18	80.9	83.2	84.7	4.18	92.0	7.7.7	82.6	8	8	77.4	81.7	89.7	81.4	7.97	94.8	97.0
$Al_2O_3$	6.0	0.	0.8	0.7	9.0	6.0	6.0	6.0	=:	0.8	pu	0:	6.0	0.8	3.5	4.8	3.4	3.4	4.0	3.2	=:	3.2	3.5	4.5	4.2	2.5	3.3	3.4	3.2	2.7	6.0	pu
$M_{gO}$	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.9	4.6	4.5	2.7	4.8	3.7	3.6	2.7	4.6	4.8	4.4	6.6	4.	5.6	3.8	9.0	pu	pu
Ь	3	4	2	9	7	<b>∞</b>	6	0	=	12	<u>~</u>	4	12	9	_	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12	<u>~</u>	4	15	9		<u>∞</u>
<b>*</b>	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.1	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2	w47.2

104

0.002 0.005
nd 0.004 0.00
0.020
nd 0.029
5.0 nd 214 0187
3.4 5
1.4 0.5
pu 2.7
98.6

$\frac{2}{2}$	0.002	0.002	0.002	0.003	0.002	0.003	0.003	0.002	0.003	0.069	0.002	0.078	0.002	0.074	0.080	0.003	0.002	0.003	0.074	0.005	0.005	0.004	0.012	0.020	0.076	0.002	0.019	0.003	0.015	0.004	0.002	0.012
Š	0.012	0.011	0.013	0.012	0.012	0.012	0.012	0.013	0.012	0.021	0.012	0.020	0.012	0.021	0.021	0.01	0.012	0.011	0.022	0.011	0.009	0.009	0.030	0.110	0.020	0.012	0.108	0.012	0.055	0.011	0.012	0.029
$\mathbb{R}_2$ O	pu	0.00	pu	0.00	pu	0.00	0.00	pu	pu	pu	pu	0.00	0.00	0.00	0.014	0.002	0.00	pu	0.002	pu	0.003	0.002	0.001	0.017								
$As_2O_3$	0.070	0.074	0.073	990.0	0.067	0.068	0.067	0.073	690.0	900.0	0.068	pu	0.067	pu	pu	0.068	0.067	0.075	pu	pu	pu	pu	0.026	0.010	pu	0.065	pu	0.072	0.009	0.202	990.0	0.018
ZnO	pu	0.00	pu	pu	pu	0.00	pu	pu	pu	pu	0.00	0.003	0.003	0.00	0.002	0.00	0.002	pu	0.00	0.003	pu	0.002	0.032	0.019	0.00	pu	0.026	0.002	0.018	0.013	pu	0.031
9	0.041	0.037	0.038	0.043	0.044	0.038	0.038	0.032	0.042	0.206	0.037	0.200	0.04	0.213	0.207	0.038	0.040	0.039	0.211	pu	pu	pu	0.011	0.001	0.195	0.038	0.007	0.038	0.002	pu	0.043	900'0
$F_{2}O_{3}$	0.447	0.430	0.458	0.460	0.413	0.460	0.448	0.467	0.439	0.055	0.448	0.057	0.466	0.054	0.063	0.463	0.435	0.450	0.049	0.108	0.133	0.120	0.493	1.604	0.043	0.472	1.560	0.502	0.513	1.162	0.444	0.460
δ O	690'0	0.062	0.089	0.072	0.095	0.094	0.067	0.075	0.091	pu	0.087	pu	9/0.0	pu	0.009	0.065	960'0	0.082	pu	pu	pu	pu	0.910	0.267	pu	0.078	0.315	960'0	0.607	1.339	0.097	0.936
S	16.0	14.9	15.6	14.9	14.7	15.5	15.2	15.1	15.4	9.1	15.2	9.4	15.5	9.2	9.1	14.9	14.9	15.2	9.4	13.6	12.0	12.1	15.9	21.5	8.7	14.7	21.3	15.1	23.6	12.3	15.3	14.8
ς Σ	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.2	0.3	0.2	0.3	0.3	0.2	0.2	0.2	0.3	0.5	0.5	0.5	9.2	4.2	0.3	0.2	4.3	0.2	3.9	0.3	0.2	8.6
Ū	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.5	0.4	pu	pu	0.5	pu	0.5	0.3	pu	9.4										
S	0.1	0.	6.0	0:	0.8	0.8	0.8	0.8	0.8	pu	0.8	pu	0.8	pu	pu	0.8	0.8	6.0	pu	9.0	4.0	4.0	3.3	<u></u>	pu	9.0	0.7	0.8	0.	0.5	6.0	2.1
P <sub>2</sub> O <sub>5</sub>	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	3.8	3.0	pu	pu	2.8	pu	3.	pu	pu	3.9										
SiO <sub>2</sub>	6'96	91.2	93.0	91.5	97.6	92.8	93.0	92.9	93.9	97.6	92.8	94.7	92.5	94.0	92.4	93.6	0.16	200.7	94.3	97.6	89.2	80.7	74.2	76.1	80.1	7.7.7	77.4	9.98	75.7	90.5	95.3	71.9
$A_2O_3$	1.2	0.	0.		0.		0.	0.1	0.		0.	1.2	0.	<u>4</u> .	1.2	6.0	0.	6.0	1.2	<u>4</u> .	4.	0.	2.4	3.7	0.8	9.0	4.0	6.0	4.7	2.0	6.0	<u>®</u> .
Qω W	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	8.	4.2	pu	pu	3.9	pu	3.4	pu	pu	7.2										
<u>م</u>	3	4	2	9	7	∞	6	0	=	12	<u>_3</u>	4	15	91		<u>8</u>	6	20	21	_	2	$\sim$	4	2	9	7	∞	6	0	=	12	13
≥	w48.I	w48.I	w48.I	w48.I	w48.I	w48.I	w48.I	w48.I	w48.I	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2										

	_																															
$ZrO_2$	0.012	0.002	0.019	0.022	0.003	0.015	0.002	0.003	0.002	0.003	0.003	0.002	0.002	0.020	0.002	0.020	0.012	0.024	0.021	0.013	0.024	0.003	0.008	0.003	0.002	0.023	0.021	0.025	0.027	0.012	0.024	0.019
SrO	0.029	0.012	0.109	0.062	0.01	0.068	0.012	0.013	0.012	0.01	0.01	0.01	0.012	0.053	0.009	0.065	0.031	990.0	0.093	0.030	0.064	0.009	0.118	0.012	0.007	0.065	0.049	0.068	0.052	0.029	0.048	0.052
$Rb_2O$	0.015	pu	0.002	0.004	pu	0.003	pu	0.002	pu	0.004	0.015	0.004	0.005	0.015	0.004	pu	0.00	pu	pu	0.003	0.003	0.003	0.005	0.014	0.005	0.002						
$As_2O_3$	0.010	690.0	900.0	0.123	690.0	0.008	0.072	0.071	990.0	0.067	0.062	0.072	990.0	pu	0.058	090.0	0.018	0.076	0.104	pu	0.074	0.051	0.005	0.065	0.171	0.082	0.118	0.070	0.107	0.038	0.112	0.007
ZnO	0.039	pu	0.024	0.031	pu	0.023	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.021	pu	0.028	0.038	0.027	0.029	0.036	0.031	0.002	0.011	pu	pu	0.027	0.027	0.030	0.027	0.033	0.022	0.025
CnO	600.0	0.046	0.007	0.010	0.040	0.002	0.045	0.045	0.041	0.039	0.041	0.045	0.037	0.003	0.045	0.013	600.0	0.007	0.007	0.011	0.014	0.048	0.00	0.037	pu	0.013	0.009	0.008	0.014	0.010	600.0	pu
$Fe_2O_3$	0.488	0.423	1.546	1.049	0.467	1.466	0.454	0.455	0.440	0.476	0.400	0.440	0.433	0.956	0.436	010:1	0.452	1.092	090'1	0.492	1.085	0.433	1.147	0.436	0.247	1.090	996.0	1.148	1.202	0.469	1.173	926.0
MnO	0.888	0.087	0.285	0.742	0.105	0.190	0.062	0.082	0.075	690.0	0.064	0.075	0.071	0.538	0.098	0.785	0.888	0.730	0.659	0.903	0.793	0.076	0.022	0.082	pu	0.746	0.668	0.743	0.641	0.818	0.588	0.477
CaO	15.2	15.1	22.0	24.0	15.0	23.8	15.4	15.1	14.6	14.9	14.8	14.4	14.8	23.7	15.1	25.1	15.2	24.1	24.4	15.7	25.0	14.6	22.0	14.6	15.7	24.5	23.1	26.8	23.8	20.1	23.3	22.8
K <sub>2</sub> O	6.7	0.2	4.2	3.8	0.2	4.	0.2	0.2	0.2	0.2	0.2	0.2	0.2	9.1	0.2	4.3	6.6	3.9	5.5	6.6	4.0	0.2	2.2	0.2	pu	4.0	9.9	3.9	5.1	7.9	4.6	1.5
Ū	0.5	pu	0.5	pu	pu	0.3	pu	0.7	pu	pu	4.0	pu	pu	4.0	pu	pu	0.3	pu	pu	pu	0.3	pu	pu	0.3	pu	0.7						
SO3	1.5	0.8	0.7	4.5	6.0	<u>1.5</u>	0.8	6.0	0.8	0.8	0.8	0.7	0.8	pu	0.8	9.0	1.2	1.5	2.0	=:	=:	0.7	<u></u>	0:	0.8	J.5	<u>~</u>	9.0	1.2	6.0	0.5	0.2
$P_2O_5$	4.2	pu	2.9	3.2	pu	2.6	pu	2.0	pu	3.0	3.8	2.4	2.7	4.0	2.5	pu	pu	pu	pu	2.8	3.0	2.6	2.7	<u>~</u> .	2.4	2.2						
$SiO_2$	77.0	92.9	80.3	74.4	92.5	84.6	95.3	92.1	81.9	0.06	97.8	82.8	8.68	8.69	89.5	75.4	72.7	72.6	77.2	73.1	78.4	85.0	74.6	87.3	8.06	78.5	73.0	76.5	9.62	63.7	74.1	72.5
$Al_2O_3$	2.7	0.8	4.5	2.9	6.0	3.8	0:	6.0	9.0	6.0	0.7	pu	0:	3.6	9.0	2.9	2.2	2.2	2.9	2.2	3.0	0.7	2.6	6.0	6.0	2.7	2.0	2.9	3.9	6.	2.7	3.8
OgM	9.5	pu	4.3	3.3	pu	3.6	pu	2.0	pu	3.3	8.4	2.5	3.5	7.7	2.8	pu	2.8	pu	pu	2.5	2.8	3.6	4.5	l.9	3.3	2.7						
Ь	4	15	9		<u>∞</u>	6	20	21	22	23	24	25	26	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	15	9	17	<u>∞</u>	61
>	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w48.2	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49	w49

1.080 0.005 0.031 0.066 0.003 0.064	0.014 0.028 0.070 0.004 0.064	0.003 nd 0.002 0.100	0.032 0.064 0.003 0.063	0.020 nd 0.002 0.096	0.002 0.514 nd 0.020 0.003	nd 0.001 0.123	0.040 0.015 0.024	nd 0.129	nd 0.007	nd 0.008	nd 0.007	0.008	900'0	0.007	0.003	0.007	900'0	0.003	900'0	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.002	900'0	0.003	900'0	900'0
1.080 0.005 0.031 0.066 0.003	0.014 0.028 0.070 0.004	0.003 nd 0.002	0.032 0.064 0.003	0.020 nd 0.002	0.002 0.514 nd	100.0 bn	0.040 0.015	pu	pu	pu	pu																				
990:0 0:003 0:080	0.014 0.028 0.070	0.003 nd	0.032 0.064	0.020 nd	0.002 0.514	pu	0.040					pu	pu	pu	_	₽	$\overline{}$	$\sim$ I	_	_	_	_	$\overline{}$	$\overline{}$	Ъ	Þ	007	ри	.002	pu	pu
1.080 0.005 0.031	0.014 0.028	0.003	0.032	0.020	0.002			pu	pu	pq					0.0	_	ŭ	0.00	2	2	DU	SI.	υ	ŭ		_	0.0		0		
1.080 0.005	0.014					0.012	$\overline{}$				0.009	pu	0.007	0.007	pu	0.007	900.0	pu	0.007	0.007	0.009	0.008	0.009	pu	900'0	0.008	pu	0.005	pu	900'0	0.117
1.080		pu	0.008	90			0.03(	0.003	pu	pu	pu	pu	pu	0.00	2.427	pu	pu	1.162	pu	pu	pu	pu	pu	pu	pu	pu	1.193	0.00	- - - - - -	pu	0.007
	287			0.0	pu	0.00	0.008	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.011
6	<u> </u>	0.677	1.057	1.550	0.316	1.205	0.331	0.852	0.184	0.212	0.184	0.181	0.188	0.193	pu	0.208	0.180	0.007	0.183	0.189	0.224	0.217	0.172	0.206	0.184	0.192	0.010	0.178	0.008	0.166	0.435
0.7	0.760	р	0.726	0.194	0.328	0.068	1.022	0.017	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
24.4	25.1	12.7	24.7	22.0	15.9	23.3	14.5	21.2	18.7	18.4	17.3	18.6	17.2	9.91	8.5	17.6	17.1	9.9	17.6	17.5	17.6	17.3	17.8	18.6	16.9	17.0	6.7	16.5	8.9	16.2	0.01
4.	4.	4.5	4.	3.9	9.4	2.2	9.0	6.	pu	pu	pu	pu	pu	pu	0.8	pu	pu	3.3	pu	pu	pu	pu	pu	pu	pu	pu	3.4	pu	3.4	pu	0.2
pu	pu	9.0	pu	0.4	0.3	9.7	9.0	0.4	pu	pu	pu	pu	pu	pu	pu	pu	pu	9.0	pu	pu	pu	pu	pu	pu	pu	pu	9.0	pu	9.0	pu	pu
0.4	7.	9.0	0.7	6.0	1.2	=	5.1	0.	=	=	0:	1.2	0:	0.	6.0	0.	0:	6.0	=	0.	0.	0.	0.	1.2	6.0	0.	6.0	0.	6.0	0.	pu
2.6	2.6	pu	2.8	2.6	pu	<u></u>	4.2	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
74.2	77.8	6.68	73.3	73.3	89.5	8	68.7	78.5	9.66	99.2	98.2	2.66	95.2	94.6	92.5	99.2	2.96	96.4	99.4	9.86	1.86	97.4	0.66	1.001	1.96	9.96	1.86	92.2	2.96	93.5	2.68
2.7	3.0	9.1	2.3	3.2	1.2	3.2	=	2.1	9.0	0.7	0.8	0.7	9.0	9.0	pu	0.7	9.0	pu	6.0	9.0	0.7	9.0	0.7	0.8	0.8	0.7	pu	0.7	pu	0.7	pu
5.6	3.4	4.	2.6	2.5	pu	3.0	7.7	3.5	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.2
20	21	22	23	24	25	26	27	28	_	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12	_3	4	15	91	17	8	61	20	21	22	_
w49	w49	w49	w49	w49	w49	w49	w49	w49	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w50	w57.01
	20 2.6 2.7 /4.2 2.6 0.4 nd 4.1 24.4 0.719	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 4.5 12.7 nd 0.677	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 26 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.331	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.331 28 3.5 2.1 78.5 nd 1.0 0.4 1.9 21.2 0.017 0.852	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.331 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.331 28 3.5 2.1 78.5 nd 1.0 0.4 19 21.2 0.017 0.852 2 nd 0.7 99.2 nd 1.1 nd nd 18.7 nd 0.184 20 0.212	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.31 28 3.5 2.1 78.5 nd 1.0 0.4 19 21.2 0.017 0.852 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 2.1 nd 0.6 99.8 nd 1.1 nd nd 18.7 nd 0.184 3 nd 0.8 98.2 nd 1.0 nd nd 18.7 nd 0.184 3 nd 0.184 3 nd 0.184 nd 0.212	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.31 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 1 0.8 98.2 nd 1.1 nd nd 18.7 nd 0.184 1 0.8 98.2 nd 1.2 nd 1.2 nd 1.3 nd 0.184 nd 0.181	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.331 28 3.5 2.1 78.5 nd 1.0 0.4 1.9 21.2 0.017 0.852 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 2 nd 0.7 99.2 nd 1.1 nd nd 18.4 nd 0.7 99.2 nd 1.0 nd nd 18.4 nd 0.7 89.2 nd 1.0 nd nd 18.4 nd 0.184 2 1 nd 0.6 95.2 nd 1.0 nd nd 17.3 nd 0.181 2 nd 0.6 95.2 nd 1.0 nd nd 17.3 nd 0.181 2 nd 0.181	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.316 28 3.5 2.1 78.5 nd 1.0 0.4 1.9 21.2 0.017 0.852 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 2 nd 0.7 99.2 nd 1.1 nd nd 18.4 nd 0.212 3 nd 0.8 98.2 nd 1.0 nd nd 18.6 nd 0.181 5 nd 0.6 95.2 nd 1.0 nd nd 17.3 nd 0.181 5 nd 0.6 94.6 nd 1.0 nd nd 16.6 nd 0.193	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.331 28 3.5 2.1 78.5 nd 1.0 0.4 19 21.2 0.017 0.852 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 2 nd 0.7 99.2 nd 1.1 nd nd 18.4 nd 0.7 89.2 nd 1.0 nd nd 18.4 nd 0.181 2 nd 0.6 95.2 nd 1.0 nd nd 18.6 nd 0.188 6 nd 0.6 94.6 nd 1.0 nd nd 16.6 nd 0.193 7 nd 1.0 nd nd 16.6 nd 0.193 7 nd 1.0 nd nd 16.6 nd 0.193 7 nd 0.25 nd 0.9 nd 0.8 85.5 nd 1.0 0.9 nd 0.8 85.5 nd 1.0 nd nd 16.6 nd 0.193	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.316 28 3.5 2.1 78.5 nd 1.0 0.4 1.9 21.2 0.017 0.852 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 1 0.1 0.4 1.3 nd 0.184 1 0.1 0.1 0.4 1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 23 2.6 2.3 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 2.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 28 3.5 2.1 78.5 nd 1.2 0.4 1.9 21.2 0.017 0.852 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 1 0.7 99.2 nd 1.1 nd nd 18.4 nd 0.184 25 nd 0.6 99.5 nd 1.0 nd nd 18.4 nd 0.185 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.185 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.188 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.188 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.188 25 nd 0.6 99.5 nd 0.0 nd nd 17.2 nd 0.188 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.193 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.193 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.193 25 nd 0.6 99.5 nd 1.0 nd nd 18.6 nd 0.193 25 nd 0.6 99.5 nd 1.0 nd nd 17.6 nd 0.208 20.8 nd 0.6 99.5 nd 1.0 nd nd 17.6 nd 0.180 20.8	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 21 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 22 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 24 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 24 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 25 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 25 3.0 3.2 81.1 1.3 1.1 0.4 2.2 23.3 0.068 1.205 27 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.02 0.31 28 3.5 2.1 78.5 nd 1.0 0.4 1.9 21.2 0.017 0.852 1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 2 nd 0.7 99.2 nd 1.0 nd nd 18.4 nd 0.184 2 nd 0.6 95.2 nd 1.0 nd nd 17.3 nd 0.188 6 nd 0.6 95.2 nd 1.0 nd nd 17.2 nd 0.188 6 nd 0.6 95.2 nd 1.0 nd nd 17.6 nd 0.193 7 nd 0.6 95.2 nd 1.0 nd nd 17.6 nd 0.180 8 nd 0.6 95.5 nd 1.0 nd nd 17.6 nd 0.180 8 nd 0.6 95.5 nd 1.0 nd nd 17.6 nd 0.180 9 nd 0.6 95.7 nd 1.0 nd nd 17.6 nd 0.180 9 nd 0.6 95.7 nd 1.0 nd nd 17.6 nd 0.180 1 nd 17.1 nd 17.1 nd 17.1 nd 17.1 nd 17.1 nd 17.	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 2.1 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 2.2 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 2.4 0.72 1.0 0.6 1.0 0.7 2.4 0.72 1.0 0.6 1.0 0.6 4.5 1.2 nd 0.677 2.4 0.72 1.0 0.0 0.1 0.4 1.5 0.2 0.1 0.6 1.0 0.4 2.5 3.2 73.3 2.6 0.9 0.4 3.9 2.0 0.1 0.1 0.5 0.3 1.2 0.3 0.4 1.5 0.3 0.4 1.5 0.3 0.4 1.5 0.3 0.4 1.5 0.3 0.4 1.5 0.3 0.4 1.5 0.3 0.4 1.5 0.3 0.4 1.5 0.3 0.4 1.0 0.3 0.4 1.0 0.3 0.4 1.0 0.1 0.3 0.4 1.0 0.1 0.1 0.1 0.1 0.4 1.0 0.4 1.9 0.1 0.1 0.1 0.1 0.4 1.0 0.4 1.9 0.1 0.1 0.1 0.1 0.1 0.4 1.1 0.4 0.4 1.9 0.1 0.1 0.1 0.1 0.1 0.4 1.1 0.4 0.4 1.9 0.1 0.1 0.1 0.1 0.1 0.1 0.4 1.1 0.4 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 2.5 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 2.3 2.4 1 1.6 89.9 nd 0.6 0.6 4.5 1.2 nd 0.677 2.4 0.726 1.087 2.4 1 2.5 3.2 73.3 2.8 0.7 nd 4.1 24.7 0.726 1.057 2.4 1.2 89.5 nd 1.2 0.3 0.4 3.9 2.2 0.194 1.550 2.2 2.3 0.08 1.2 0.5 2.4 1.3 1.1 0.4 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.2 2.3 0.08 1.2 0.5 2.3 0.08 1.2 0.5 2.3 0.08 1.2 0.5 2.2 0.0 0.4 1.9 0.4 1.9 0.4 1.9 0.1 0.1 0.1 0.4 1.9 0.4 1.9 0.1 0.1 0.1 0.1 0.4 1.9 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 1.081 2.7 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 2.2 4.1 1.6 89.9 nd 0.6 0.6 4.5 12.7 nd 0.677 2.4 0.718 1.0 0.6 4.5 12.7 nd 0.677 2.4 0.728 1.087 2.4 0.73 2.8 0.7 nd 0.677 2.2 3.2 73.3 2.8 0.7 nd 0.677 2.2 3.3 0.068 1.057 2.4 0.7 89.5 nd 1.2 0.4 2.2 2.3 0.068 1.205 2.4 0.7 89.5 nd 1.1 0.4 2.2 2.3 0.068 1.205 2.4 0.7 89.5 nd 1.1 0.4 2.2 2.3 0.068 1.205 2.4 0.0 0.7 89.5 nd 1.1 nd nd 18.7 nd 0.184 1.2 nd 0.18 1.1 nd 0.6 99.5 nd 1.1 nd nd 18.4 nd 0.1 0.0 1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 2.1 3.4 3.0 77.8 2.6 1.5 nd 4.1 25.1 0.760 1.087 2.2 4.1 1.6 89.9 nd 0.6 0.6 4.5 1.2 nd 0.677 2.3 2.6 0.9 0.4 3.9 2.20 0.760 1.087 2.5 3.2 3.2 73.3 2.6 0.9 0.4 3.9 2.20 0.328 0.316 2.5 3.0 3.2 81.1 1.3 1.1 0.4 2.2 2.3 0.068 1.205 2.4 7.7 1.1 68.7 4.2 5.1 0.6 9.0 14.5 1.022 0.331 2.8 3.5 2.1 78.5 nd 1.0 0.4 1.9 21.2 0.017 0.852 1.1 nd 0.6 99.6 nd 1.1 nd nd 18.7 nd 0.184 2.1 nd 0.184 2.1 nd 0.184 nd 0.184 2.1 nd 0.184 nd 0.184 2.1 nd 0.194 2.1 nd 0.	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 1.02	20	20	20  2.6  2.7  742  2.6  0.4  nd  4.1  24.4  0.719  1.080  2.2  4.1  1.6  8.3	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 2.3 3.3 3.8 nd 0.6 0.6 4.5 1.2 7.7 nd 0.677 2.3 2.6 1.3 nd 4.1 25.1 0.760 1.087 2.4 1.16 8.9 nd 0.6 0.6 4.5 1.2 7.3 nd 0.677 2.5 3.2 73.3 2.6 0.9 0.4 3.9 22.0 0.194 1.550 2.5 nd 1.2 89.5 nd 1.2 0.3 0.4 15.9 0.328 0.316 2.2 3.3 1.1 0.4 2.2 2.3 0.068 1.205 2.3 1.1 0.8 7.7 1.1 6.8 7 4.2 5.1 0.6 9.0 14.5 10.22 0.331 1.1 0.4 2.2 2.3 0.068 1.205 2.3 nd 0.6 99.6 nd 1.1 nd nd 1.8 nd 0.1 1.3 nd 0.1	20	20 2.6 2.7 74.2 2.6 0.4 nd 4.1 24.4 0.719 1.080 2.5 2.7 74.2 2.6 0.4 nd 4.1 24.7 0.750 1.080 2.3 3.1 3.2 2.6 0.5 nd 4.1 24.7 0.750 1.087 2.4 1.1 6.8 9.9 nd 0.6 0.6 4.5 1.2 0.0 0.194 1.550 2.4 2.5 3.2 73.3 2.6 0.9 0.4 3.9 2.20 0.194 1.550 2.5 3.2 3.2 73.3 2.6 0.9 0.4 3.9 2.20 0.194 1.550 2.5 3.2 3.2 73.3 2.6 0.9 0.4 3.9 2.20 0.194 1.550 2.5 3.0 3.1 81.1 1.3 1.1 0.4 2.2 2.3 3.3 0.068 1.205 2.5 3.2 1.1 68.7 nd 1.2 0.4 1.9 21.2 0.017 0.832 1.1 0.6 9.9 1.9 1.1 0.4 1.9 21.2 0.017 0.832 1.1 0.8 9.9 nd 1.0 nd nd 1.1 nd nd 1.8 nd 0.184 nd 0.184 nd 0.184 nd 0.184 nd 0.184 nd 0.194 nd 0.19 9.9 nd 0.0 9.9 nd 0.0 nd 1.0 nd nd 1.2 nd 0.184 nd 0.198 nd 0.19 9.9 nd 0.0 9.9 nd 0.0 0.0 nd 1.1 nd 0.0 9.9 nd 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	1.080 1.087 0.677 1.057 1.057 1.550 0.316 0.331 0.184 0.188 0.193 0.188 0.193 0.188 0.193 0.183 0.183 0.183 0.183 0.193 0.183 0.193 0.193 0.193 0.192 0.192 0.192 0.192 0.192

$ZrO_2$	0.010	0.008	0.007	0.008	600.0	0.007	0.007	0.007	600.0	900.0	0.003	0.007	0.007	0.003	9000	600.0	600.0	600.0	600.0	0.002	0.002	0.010	600.0	0.007	0.005	0.007	0.007	0.007	600.0	0.007	0.008	0.007
SrO	0.115	0.166	900'0	0.170	0.113	0.169	0.008	0.005	0.169	0.171	0.010	900'0	900'0	0.007	0.169	0.007	0.167	0.170	0.114	0.007	0.009	0.114	0.166	900.0	0.010	900'0	0.174	900'0	0.169	0.162	0.171	0.008
$Rb_2O$	0.001	0.00	pu	0.00	0.00	0.00	pu	pu	0.00	0.00	0.00	pu	pu	pu	0.00	pu	0.00	0.00	0.00	pu	pu	0.00	0.00	pu	0.00	pu	0.00	pu	0.00	0.00	0.001	pu
$As_2O_3$	pu	pu	0.116	9000	pu	0.007	pu	0.122	0.009	pu	910.0	0.115	0.114	0.188	0.009	0.050	9000	910.0	pu	pu	0.047	pu	0.010	0.110	pu	0.110	0.005	0.116	pu	0.044	pu	pu
ZnO	0.038	0.005	0.005	9000	0.021	0.004	0.003	9000	9000	0.008	0.003	0.007	9000	pu	9000	pu	0.008	0.009	0.022	0.002	pu	0.035	0.009	0.009	0.00	0.005	0.004	0.005	0.005	0.005	0.009	0.002
CnO	pu	pu	0.010	pu	pu	pu	pu	0.011	0.00	pu	pu	0.014	0.011	pu	pu	9000	0.00	pu	pu	pu	pu	pu	0.002	0.011	pu	0.008	0.003	0.009	pu	0.002	pu	pu
$Fe_2O_3$	0.808	1.158	0.449	1.367	0.783	1.207	0.318	0.425	1.162	1.152	0.246	0.412	0.420	0.185	1.169	0.116	1.424	1.419	0.845	0.156	0.182	0.803	1.388	0.427	0.236	0.413	1.189	0.392	1.124	1.089	1.391	0.340
MnO	0.007	0.018	pu	0.029	900'0	0.028	pu	pu	0.036	0.032	0.024	pu	pu	pu	0.011	pu	0.04	0.042	pu	0.104	pu	0.014	0.038	pu	pu	pu	0.023	pu	0.034	0.020	0.040	pu
CaO	9.61	21.2	6.6	17.5	18.9	21.4	0.91	0.0	21.4	21.3	16.3	6.6	6.7	15.6	21.5	14.8	17.6	18.2	19.0	15.0	15.9	19.2	17.4	0.0		6.6	22.3	10.2	21.9	20.1	  -  -	16.0
$K_2O$	1.7	6:1	0.	2.5	9.1	2.0	0.3	0.2	2.0	2.0	0.3	0.	0.2	pu	6:1	pu	2.5	2.5	9.1	pu	0.0	9.1	2.5	0.2	0.5	0.2	2.1	0.2	2.1	<u>~</u>	2.6	0.3
D	0.4	4.0	pu	0.4	0.4	0.5	pu	pu	0.5	0.5	pu	pu	pu	pu	0.5	pu	4.0	0.4	4.0	pu	pu	4.0	4.0	pu	pu	pu	0.5	pu	0.5	0.5	0.5	pu
$SO_3$	0.3	0.8	pu	0.4	0.3	0.8	9.0	pu	0.7	0.8	=	pu	pu	<u>-</u> .	.5	6.0	9.0	0.4	0.3	=	0:	0.5	9.0	pu	0.5	pu	6.0	pu	0.	5.1	0.4	0.7
$P_2O_5$	pu	pu	pu	<u>-</u> .	pu	pu	pu	pu	0.	=:	pu	pu	pu	pu	<u>4</u> .	pu	1.5	1.7	pu	pu	pu	pu	1.5	pu	pu	pu	=:	pu	<u> </u>	1.7	<u>+</u> .	pu
$SiO_2$	87.3	85.2	88.9	87.2	88.9	87.2	91.5	90.4	86.9	8.98	95.2	92.0	0.88	94.9	8.98	92.8	1.98	88.9	8.16	98.6	296	8.16	87.7	92.4	99.3	92.7	89.5	92.5	88.2	82.2	6.68	93.9
$Al_2O_3$	3.5	3.0	pu	3.9	3.8	3.4	9.0	0.5	3.4	3.7	0.8	pu	pu	6.0	3.8	pu	3.6	4.	4.0	9.0	0.8	3.8	4.2	9.0	2.0	0.5	3.4	0.7	3.7	3.4	3.9	0.5
MgO	3.5	3.7	2.2	4.7	3.	4.8	pu	2.2	4.4	4.6	pu	2.9	2.2	pu	4.7	pu	4.	4.6	4.	pu	pu	3.8	4.9	2.6	pu	2.8	4.5	2.3	4.4	4.5	2.0	pu
Ь	2	$\sim$	4	2	9	_	∞	6	0	=	12	<u>~</u>	4	15	9	17	<u>∞</u>	61	20	21	22	23	24	_	7	$\sim$	4	2	9	_	<b>∞</b>	6
<b>X</b>	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.01	w57.02	w57.02	w57.02	w57.02	w57.02	w57.02	w57.02	w57.02	w57.02

0.011	0.038	0.010	0.015	0.012	900'0	0.007	0.011	0.037	0.022	0.038	0.022	900'0	0.023	0.007	0.012	0.007	0.014	0.017	0.014	0.008	0.027	0.008	0.008	900.0	0.011	0.009	0.009	0.004	0.007	0.002	0.009
0.111	0.047	0.130	0.044	0.043	0.070	0.243	0.112	0.049	0.091	0.049	0.051	0.187	0.086	900.0	0.047	0.005	0.042	0.045	0.050	0.322	0.064	0.008	0.168	0.168	900.0	0.173	0.01	0.003	900'0	0.041	0.165
0.00	0.003	0.00	0.004	0.004	0.004	0.002	0.00	0.003	0.004	0.004	0.002	0.00	0.004	pu	0.003	pu	0.005	0.004	0.003	0.00	0.004	pu	0.00	0.00	pu	0.00	pu	pu	pu	pu	0.001
0.007	0.105	pu	0.014	pu	pu	9000	0.014	0.129	0.119	0.121	0.081	0.008	0.103	0.119	0.021	0.113	0.024	0.012	0.018	0.007	0.103	pu	pu	pu	0.011	pu	pu	0.485	0.113	0.013	pu
0.013	0.026	9000	0.025	0.020	0.009	0.004	0.008	0.033	0.025	0.035	0.018	9000	0.025	0.007	0.022	0.005	0.027	0.028	0.023	0.00	0.042	0.002	0.003	0.009	pu	9000	pu	pu	0.004	pu	0.005
0.008	0.011	0.00	0.013	9000	0.003	pu	0.005	0.013	0.013	0.013	0.010	pu	0.009	0.015	0.010	9000	0.002	0.01	0.009	pu	0.013	pu	0.002	0.00	pu	pu	pu	pu	900'0	pu	0.001
1.039	1.0.1	1.045	1.377	1.168	0.337	0.503	1.112	1.147	1.107	1.157	0.756	1.074	1.032	0.460	0.511	0.416	1.187	0.732	0.516	0.624	1.426	0.298	1.150	1.305	0.082	1.484	0.168	0.099	0.407	0.317	1.158
0.055	0.512	0.119	0.124	0.094	0.200	0.007	0.035	0.682	0.733	0.684	0.445	0.029	0.678	pu	0.581	pu	0.287	0.604	0.588	pu	0.804	pu	0.024	0.059	pu	0.040	pu	pu	pu	pu	0.028
24.4	23.1	23.9	23.9	23.6	12.5	6.7	26.2	24.7	24.9	24.8	23.2	19.3	23.5	8.6	23.0	6.7	24.1	22.1	23.7	1.5	22.4	1.91	21.2	22.8	15.3	17.9	15.3	8.7	6.6	14.6	21.3
9.1	4.8	2.4	5.2	4.8	6.5	3.7	1.7	5.2	5.6	5.1	3.6	2.3	5.2	0.2	3.8	0.2	5.1	4.6	3.8	3.5	5.6	0.3	6.1	2.0	pu	2.6	0.0	pu	0.0	0.5	2.0
9.0	pu	0.3	pu	pu	0.7	0.3	9.0	pu	pu	pu	pu	9.0	pu	pu	9.0	pu	pu	9.0	9.0	9.0	pu	pu	0.5	4.0	pu	0.5	pu	pu	pu	0.5	0.5
2.2	3.6	4.	2.1	9.0	0.3	-5.	2.0	0.8	2.1	6.0	<u>~</u> .	6.0	2.0	pu	2.0	pu	7.	9.1	1.7	pu	3.	0.7	0.8	9.0	€.	0.3	0.5	9.4	pu	9.4	0.1
1.5	3.7	<u></u>	2.9	2.4	pu	<u></u>	9.	3.5	2.6	3.6	2.4	<u></u>	2.5	pu	3.8	pu	3.2	3.6	3.5	2.0	3.3	pu	Ξ:	0:	pu	4.	pu	pu	pu	pu	0.1
83.1	82.9	85.2	78.6	85.2	94.4	94.3	1.98	80.7	79.2	79.1	79.9	82.7	74.1	93.6	80.2	6.06	83.8	77.3	79.8	95.7	77.5	95.7	88.4	88°.I	94.3	90.2	9.96	90.5	61.7	97.4	88.3
3.2	3.0	3.2	3.9	3.4	0.	2.6	4.0	2.6	3.3	2.8	9:1	2.6	2.4	1.5	5.1	pu	3.9	6.2	4.9	2.8	3.9	6.0	3.5	4.0	pu	3.9	0.7	pu	9.0	=:	3.6
4.2	3.	2.0	2.8	2.6	3.3	9.7	4.6	3.9	4.	3.2	2.1	4.8	3.0	2.2	3.8	2.7	3.7	3.9	3.6	7.3	4.0	pu	4.4	5.2	pu	5.0	pu	pu	2.5	pu	3.8
_	2	$\sim$	4	2	9	_	∞	_	2	$\sim$	4	2	9	7	_	2	$\sim$	4	2	9	7	_	2	$\sim$	4	2	9	7	_	7	M
w57.03	w57.03	w57.03	w57.03	w57.03	w57.03	w57.03	w57.03	w57.04	w57.04	w57.04	w57.04	w57.04	w57.04	w57.04	w57.05	w57.05	w57.05	w57.05	w57.05	w57.05	w57.05	w57.06	w57.06	w57.06	w57.06	w57.06	w57.06	w57.06	w57.07	w57.07	w57.07
	3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2 3.1 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.1111 2 3.1 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2 3.1 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 4 2.8 3.9 78.6 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2 3.1 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.016 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 4 2.8 3.9 78.6 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 2.8 2.6 3.4 85.2 2.4 0.6 nd 4.8 23.6 0.094 1.168 0.006 0.020 nd 0.004 0.043	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.011 0.026 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 4 2.8 3.9 78.6 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 5 2.6 3.4 85.2 2.4 0.6 nd 4.8 23.6 0.094 1.168 0.006 0.020 nd 0.004 0.043 6 3.3 1.0 94.4 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.070	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2 3.1 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.016 0.026 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 4 2.8 3.9 78.6 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 2 3.4 85.2 2.4 0.6 nd 4.8 23.6 0.094 1.168 0.006 0.020 nd 0.004 0.043 6 3.3 1.0 94.4 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.070 0.070 7.6 2.6 94.3 1.3 1.5 0.3 3.7 9.7 0.002 0.503 nd 0.004 0.006 0.020 0.243	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.1111 2 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 0.130 2 5.0 3.4 85.2 2.4 0.6 nd 4.8 23.6 0.094 1.168 0.006 0.020 nd 0.004 0.004 0.004 0.004 0.007 0.3 3.3 1.0 94.4 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.006 0.020 0.243 1.3 1.5 0.3 3.7 9.7 0.002 0.503 nd 0.004 0.006 0.002 0.243 8 4.6 4.0 86.1 1.6 2.0 0.4 1.7 26.2 0.035 1.112 0.005 0.005 0.014 0.001 0.112	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 0.044 0.3 2.4 0.6 nd 4.8 23.6 0.094 1.168 0.006 0.025 0.014 0.004 0.043 0.043 3.3 1.0 94.4 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.070 7 7.6 2.6 94.3 1.3 1.5 0.3 3.7 9.7 0.002 0.503 nd 0.004 0.006 0.002 0.243 8 6.0 86.1 1.6 2.0 0.4 1.7 26.2 0.035 1.112 0.005 0.008 0.014 0.001 0.112 8 4.6 4.0 86.1 1.6 2.0 0.4 1.7 26.2 0.035 1.147 0.013 0.033 0.039 0.014 0.001 0.112	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24,4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2 2 3.1 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 0.130 2.4 2.8 3.9 78.6 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 0.0 nd 4.8 23.6 0.094 1.168 0.006 0.020 nd 0.004 0.043 0.070 0.3 1.0 94.4 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.070 0.243 0.2 0.4 1.5 0.3 3.7 0.03 0.005 0.003 0.004 0.006 0.002 0.243 0.0 0.0 0.4 1.7 26.2 0.035 1.112 0.005 0.008 0.014 0.001 0.112 0.112 0.005 0.03 0.14 0.0 0.1 0.112 0.113 0.3 0.2 0.3 0.14 0.0 0.1 0.113 0.13 0.2 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24,4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2.3 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3.5 2.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 0.044 2.8 3.9 78.6 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 0.044 2.8 3.4 85.2 2.4 0.6 nd 4.8 23.6 0.094 1.168 0.006 0.020 nd 0.004 0.004 0.004 0.007 0.3 3.3 1.0 94.4 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.007 0.004 0.007 0.004 0.004 0.007 0.004 0.004 0.007 0.004 0.007 0.004 0.007 0.000 0.0	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2.3 3.1 8.2 8.2 1.3 1.4 0.3 2.4 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3.2 8.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 0.044 2.8 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 0.04 2.8 3.4 85.2 2.4 0.6 nd 4.8 23.6 0.094 1.168 0.006 0.020 nd 0.004 0.004 0.045 0.005 0.009 nd 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.007 0.00 0.33 1.0 0.004 0.004 0.007 0.00 0.33 1.1 0.004 0.004 0.000 0.004 0.0	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2.3 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2.3 3.0 82.9 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3.5 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 0.044 2.8 2.9 2.1 nd 5.2 23.9 0.124 1.377 0.013 0.025 0.014 0.004 0.044 0.044 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.004 0.005 0.003 0.004 0.004 0.004 0.005 0.33 1.0 94.4 nd 0.3 0.7 6.5 12.5 0.200 0.337 0.003 0.009 nd 0.004 0.005 0.005 0.00	1 4.2 3.2 8.3.1 1.5 2.2 0.4 1.6 24.4 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2.3 3.9 8.29 3.7 3.6 nd 4.8 23.1 0.512 1.011 0.011 0.026 0.105 0.003 0.047 3.5 5.0 3.2 85.2 1.3 1.4 0.3 2.4 23.9 0.119 1.045 0.001 0.006 nd 0.001 0.130 0.44 2.8 3.9 78.6 2.9 2.1 nd 5.2 2.3 0.124 1.377 0.013 0.025 0.014 0.004 0.044 0.03 0.04 0.03 0.037 0.033 0.009 nd 0.004 0.044 0.03 0.04 0.03 0.033 0.033 0.009 nd 0.004 0.004 0.004 0.004 0.03 0.03 0.03	1         4.2         3.2         83.1         1.5         2.2         0.4         1.6         24.4         0.055         1.039         0.008         0.013         0.007         0.001         0.111           3         3.1         3.0         82.9         3.7         3.6         nd         4.8         23.1         0.512         1.011         0.011         0.026         0.105         0.003         0.047           4         2.8         3.2         85.2         1.3         1.4         0.3         2.4         23.9         0.119         1.045         0.001         0.006         nd         0.001         0.004         0.014         0.001         0.004	1 4.2 3.2 83.1 1.5 2.2 0.4 1.6 24, 0.055 1.039 0.008 0.013 0.007 0.001 0.111 2.2 3.1 83.2 83.2 83.2 83.2 83.2 83.2 83.2 83.2	1         4,2         3,2         8,31         1,5         2,2         0,4         1,6         24,4         0,055         1,039         0,008         0,013         0,007         0,001         0,111           3,1         3,0         82,9         3,7         3,6         nd         4,8         23,1         0,512         1,011         0,011         0,016         0,005         0,005         0,004         0,044           4         2,8         3,9         7,86         2,9         2,1         nd         2,3         0,124         1,137         0,013         0,005         nd         0,004         0,044           5         3,2         3,4         8,5,2         2,4         0,6         nd         1,18         0,003         0,044         0,004         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044         0,004         0,044	1         4.2         3.2         83.1         1.5         2.2         0.4         1.6         24.4         0.055         1.039         0.008         0.013         0.007         0.001         0.011         0.011         0.012         0.013         0.004         0.011         0.011         0.011         0.005         0.013         0.004         0.013         0.004         0.013         0.004         0.013         0.004         0.004         0.014         0.004         0.013         0.004	1         4.2         3.2         83.1         1.5         2.2         0.4         1.6         244         0.055         1.039         0.008         0.013         0.007         0.001         0.011           3         3.0         82.9         3.7         3.6         nd         4.8         23.1         0.512         1.011         0.011         0.016         0.005         0.105         0.003         0.044           4         2.8         3.9         7.86         2.9         1.1         1.045         0.001         0.006         0.002         0.003         0.044           5         2.6         3.4         85.2         2.4         0.6         1.2         0.044         1.8         0.04         1.18         0.004	1         4,2         3,2         8,31         1,5         2,2         0,4         1,6         24,4         0,055         1,039         0,008         0,013         0,007         0,001         0,011         0,111         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,011         0,002         0,003         0,004	1         42         32         83.1         1.5         22         0.4         1.6         244         0.055         1.039         0.008         0.013         0.007         0.010         0.011           3         3.1         3.0         82.9         3.7         3.6         nd         4.8         23.1         0.512         1.011         0.011         0.026         0.105         0.003         0.047           4         2.6         3.9         3.7         3.6         1.4         0.3         2.4         2.8         0.119         1.049         0.004 <td< th=""><th>  1</th><th>  1</th><th>1         42         32         831         1.5         22         0.4         1.6         244         0.055         1.039         0.008         0.013         0.007         0.001         0.013         0.005         0.01         0.010         0.004         0.01         0.0</th><th>  1</th><th>  1</th><th>  1</th><th>  1</th><th>42         32         831         15         22         04         16         244         0055         1039         0008         0013         0009</th><th>1 4.2 3.2 83.1 1.5 2.2 0.4 3 3.0 82.9 3.7 3.6 nd 3 5.0 3.2 85.2 1.3 1.4 0.3 4 2.8 3.9 78.6 2.9 2.1 nd 5 2.6 3.4 85.2 2.4 0.6 nd 6 3.3 1.0 94.4 nd 0.3 0.7 7 6 2.6 94.3 1.3 1.5 0.3 8 4.6 4.0 86.1 1.6 2.0 0.4 1 3.3 79.2 2.6 2.1 nd 3 3.2 2.8 79.1 3.6 0.9 nd 4 2.1 1.6 79.9 2.4 3.1 nd 7 2.2 1.5 93.6 nd nd nd 7 2.2 1.5 93.6 nd nd 8 3.3 3.7 3.9 83.8 3.2 1.5 nd 8 3.4 8.5 180.2 3.8 0.0 6 7.3 2.8 95.7 0.0 nd 0.9 95.7 nd 0.0 0.0 0.0 7 4.4 3.5 88.4 1.1 0.8 0.5 8 5.0 3.9 90.2 1.4 0.3 0.5 6 nd 0.7 96.6 nd 0.6 7 nd nd 94.3 nd nd 0.7 96.6 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 96.6 nd 0.7 0.6 0.7 nd 0.7 96.6 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 0.6 0.4 nd 0.7 0.6 0.4 nd 0.7 0.6 0.4 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 0.6 0.7 nd 0.8 0.7 nd 0.9 95.7 nd 0.9 95.7 nd 0.9 95.7 nd 0.9 95.7 nd 0.9 0.9 0.9 nd 0</th></td<>	1	1	1         42         32         831         1.5         22         0.4         1.6         244         0.055         1.039         0.008         0.013         0.007         0.001         0.013         0.005         0.01         0.010         0.004         0.01         0.0	1	1	1	1	42         32         831         15         22         04         16         244         0055         1039         0008         0013         0009	1 4.2 3.2 83.1 1.5 2.2 0.4 3 3.0 82.9 3.7 3.6 nd 3 5.0 3.2 85.2 1.3 1.4 0.3 4 2.8 3.9 78.6 2.9 2.1 nd 5 2.6 3.4 85.2 2.4 0.6 nd 6 3.3 1.0 94.4 nd 0.3 0.7 7 6 2.6 94.3 1.3 1.5 0.3 8 4.6 4.0 86.1 1.6 2.0 0.4 1 3.3 79.2 2.6 2.1 nd 3 3.2 2.8 79.1 3.6 0.9 nd 4 2.1 1.6 79.9 2.4 3.1 nd 7 2.2 1.5 93.6 nd nd nd 7 2.2 1.5 93.6 nd nd 8 3.3 3.7 3.9 83.8 3.2 1.5 nd 8 3.4 8.5 180.2 3.8 0.0 6 7.3 2.8 95.7 0.0 nd 0.9 95.7 nd 0.0 0.0 0.0 7 4.4 3.5 88.4 1.1 0.8 0.5 8 5.0 3.9 90.2 1.4 0.3 0.5 6 nd 0.7 96.6 nd 0.6 7 nd nd 94.3 nd nd 0.7 96.6 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 96.6 nd 0.7 0.6 0.7 nd 0.7 96.6 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 0.6 0.4 nd 0.7 0.6 0.4 nd 0.7 0.6 0.4 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 0.6 0.7 nd 0.8 0.5 nd 0.7 0.6 0.7 nd 0.8 0.7 nd 0.9 95.7 nd 0.9 95.7 nd 0.9 95.7 nd 0.9 95.7 nd 0.9 0.9 0.9 nd 0

$ZrO_2$	0.034	0.003	0.008	0.032	0.002	0.003	0.008	0.002	0.008	0.007	0.004	0.007	0.004	900'0	0.005	0.005	0.008	0.013	0.009	0.017	0.007	0.034	0.004	0.035	0.003	0.035	0.010	0.005	0.007	0.024	0.033	0.037
S.	190.0	900'0	0.166	0.061	0.013	0.015	0.164	0.008	900.0	900.0	0.009	0.173	0.009	900.0	0.007	0.008	0.026	0.068	0.044	0.023	0.025	0.063	0.007	0.062	0.003	0.063	0.137	0.132	0.210	990.0	0.063	0.064
$Rb_2O$	0.004	pu	0.00	0.003	pu	pu	0.00	pu	pu	pu	0.00	0.00	0.00	pu	0.00	pu	910.0	0.009	0.004	0.011	910.0	0.003	0.00	0.003	0.00	0.003	0.00	0.00	0.00	0.003	0.003	0.003
$As_2O_3$	0.183	pu	pu	0.130	0.819	0.307	pu	pu	0.120	0.116	pu	0.010	pu	0.115	pu	pu	910.0	pu	pu	0.013	0.025	0.105	0.652	0.102	0.064	0.108	pu	pu	0.010	0.135	0.107	0.134
ZnO	0.021	0.002	0.00	0.022	0.004	pu	0.005	pu	0.007	900.0	pu	0.002	pu	900.0	0.003	0.003	0.033	0.039	0.019	0.029	0.031	0.020	pu	0.021	pu	0.023	900.0	0.004	0.012	0.026	0.025	0.023
CuO	0.012	pu	0.003	0.008	pu	pu	0.002	pu	0.012	0.009	pu	0.00	pu	0.009	pu	0.00	0.008	0.025	0.009	0.012	0.013	0.007	0.001	0.010	pu	0.019	pu	0.003	pu	0.010	0.008	0.018
$Fe_2O_3$	1.126	0.147	1.109	1.135	0.235	0.078	1.145	0.156	0.455	0.446	0.118	I. 18	0.098	0.434	0.195	0.902	0.330	0.700	1.124	0.657	0.297	1.212	0.298	8	0.090	1.132	1.148	0.929	1.072	1.357	1.193	1.331
MnO	0.575	pu	0.046	0.527	0.352	pu	0.014	pu	pu	pu	pu	0.014	pu	pu	pu	1.014	0.995	1.217	0.042	0.640	966.0	0.569	0.012	0.588	pu	0.583	0.025	0.010	0.094	0.593	0.541	0.562
CaO	24.7	15.1	21.1	25.9	12.5	17.1	20.7	15.7	10.2	8.6	7.9	21.2	8.0	6.7	13.3	0.0	14.9	19.0	26.2	14.0	14.6	27.3	14.0	26.8	8.2	27.2	23.0	23.2	18.6	22.2	27.1	24.0
K <sub>2</sub> O	3.7	0.2	6:1	3.9	0.2	pu	6:1	pu	0.2	0.2	0.2	2.0	0.2	0.	0.5	0.2	9.5	- 8.	5.5	6.7	8.8	4.	0.5	4.0	0.2	4.2	1.7	1.7	3.7	2.9	4.	4.2
ס	0.3	pu	4.0	pu	pu	pu	0.5	pu	pu	pu	pu	0.4	pu	pu	pu	pu	9.0	4.0	pu	9.0	0.5	pu	pu	pu	pu	pu	0.3	9.0	0.5	9.0	pu	0.3
SO3	6.1	1.2	0.8	2.0	0.8	6.0	6.0	6.0	pu	pu	9.0	1.2	0.7	pu	4.0	pu	4.5	0.	9.0	0.7	0.7	1.2	0.8	6.0	0.2	0.8	0.7	1.2	0.	6.0	0.	6.7
$P_2O_5$	4.2	pu	1.2	2.7	pu	pu	1.2	pu	pu	pu	pu	=	pu	pu	pu	pu	4.9	4.7	2.1	4.	4.6	2.7	pu	2.6	pu	2.7	=:	pu	2.1	4.	2.6	3.7
SiO <sub>2</sub>	69.5	94.9	86.5	75.1	96.3	93.1	85.3	95.3	93.6	94.6	93.9	88.3	8.16	9.88	98.3	92.4	75.6	75.7	82.5	78.3	74.2	80.9	95.3	9.08	96.5	81.5	84.7	87.0	87.2	78.5	9.77	77.4
$Al_2O_3$	3.5	9.0	3.6	3.6	0:	0.7	3.2	9.0	0.7	1.2	9.0	3.5	0.8	pu	2.1	pu	<u>~</u>	2.9	4.4	2.7	<u>~</u>	4.5	2.0	4.	€.	4.5	3.2	3.0	3.0	2.8	4.2	4.
OgM	3.0	pu	4.6	3.7	pu	pu	4.	pu	2.4	2.5	3.8	4.7	3.8	2.2	pu	2.5	6.7	7.1	2.1	J.6	8.8	3.7	pu	3.9	4.6	3.4	5.4	5.1	5.7	2.5	4.0	2.6
۵	4	2	9	7	$\infty$	6	_	2	$\sim$	4	2	9		$\infty$		2	$\sim$	4	2	9	7	_	2	$\sim$	4	2	9	7	_	7	$\sim$	4
≯	w57.07	w57.07	w57.07	w57.07	w57.07	w57.07	w57.08	w57.08	w57.08	w57.08	w57.08	w57.08	w57.08	w57.08	w57.09	w57.09	w57.09	w57.09	w57.09	w57.09	w57.09	w57.10	w57.11	w57.11	w57.11	w57.11						

$ZrO_2$	0.024	0.022	0.036	0.003	0.007	0.008	0.034	0.030	0.007	0.040	0.005	0.037	0.017	0.040	0.038	0.004	0.038	0.007	0.038	0.015	0.036	0.002	0.014	0.015	0.007	0.005	0.009	0.008	900'0	0.009	0.007	0.003
SrO	0.064	0.088	0.052	0.009	900.0	0.164	0.060	0.052	0.216	0.05	0.007	0.059	0.044	0.050	0.05	0.003	0.05	900.0	0.057	0.089	0.059	900.0	0.047	0.043	0.027	0.012	0.168	0.172	0.012	0.163	0.165	900'0
$Rb_2O$	0.003	0.005	0.003	0.00	pu	0.00	0.004	0.003	0.00	0.004	0.00	0.003	0.004	0.003	0.003	pu	0.003	pu	0.004	0.003	0.004	pu	0.003	0.005	0.017	pu	0.00	0.00	0.001	0.001	0.00	pu
$As_2O_3$	0.110	0.169	0.184	0.613	0.117	pu	0.173	0.113	pu	0.135	pu	0.074	0.039	0.121	0.129	pu	0.148	0.113	0.055	0.013	0.097	0.124	0.013	pu	0.019	pu	0.012	pu	pu	pu	0.008	pu
ZnO	0.025	0.029	0.030	0.00	0.008	0.003	0.019	0.027	0.00	0.035	0.002	0.033	0.018	0.034	0.038	pu	0.037	0.007	0.027	0.023	0.032	pu	0.025	0.026	0.030	0.004	0.008	900.0	pu	0.007	0.005	pu
CnO	0.005	0.009	0.011	pu	0.007	0.007	910.0	0.010	0.007	0.012	pu	0.009	900'0	0.013	0.012	pu	0.012	0.008	0.011	0.003	0.010	pu	0.013	0.010	0.014	pu	pu	pu	pu	pu	0.001	pu
$Fe_2O_3$	1.354	1.021	0.898	0.424	0.473	1.155	1.115	1.046	0.512	1.140	0.230		1.342	1.112	1.153	0.002	1.176	0.463	1.139	1.557	1.197	0.164	0.513	1.351	0.326	0.229	1.372	1.459	0.156	1.394	1.125	0.157
MnO	0.627	0.690	0.579	pu	pu	0.029	0.560	0.729	0.004	0.682	pu	0.551	0.306	0.653	0.690	0.085	0.582	pu	0.624	0.118	0.569	pu	0.660	0.159	0.938	pu	0.035	0.052	pu	0.048	0.012	pu
CaO	22.7	22.2	22.2	13.5	I  -	21.1	25.3	23.1	13.8	25.1	4.4	23.1	23.9	24.9	25.0	9.3	25.4	10.2	23.0	22.7	23.9	15.5	24.5	26.2	14.7	15.6	17.6	17.8	13.5	17.6	21.0	16.4
$K_2O$	2.9	5.3	4.4	0.5	0.2	2.0	3.7	4.	1.7	5.1	0.5	5.4	4.3	5.1	5.2	0.2	4.7	0.	5.3	4.0	5.5	pu	3.9	6.1	9.2	0.2	2.5	2.6	0.5	2.6	6.1	pu
D	9.0	0.3	0.3	pu	pu	0.3	0.3	9.0	0.2	pu	0.2	pu	0.2	0.3	0.2	pu	9.0	pu	9.0	pu	4.0	0.5	pu	0.5	0.5	pu						
SO3	6.5	9:1	9:1	6.0	pu	6.0	9.3	1.01	9.0	9:1	0.8	2.1	=:	0:	6.0	4.0	3.5	pu	1.2	6:1	3.5	1.2	<u>4</u> .	0:	4.5	0.3	0.3	0.5	0.3	0.4	0.7	9:1
$P_2O_5$	3.8	4.4	5.5	pu	pu	1.2	4.0	4.6	pu	3.6	pu	3.3	3.	3.6	3.7	pu	3.6	pu	3.3	3.0	3.6	pu	3.6	2.7	4.5	pu	<u>4</u> .	<u>4</u> .	pu	<u>+</u> .	pu	pu
$SiO_2$	78.3	76.0	71.4	95.1	93.2	88.3	8.69	74.0	93.7	81.9	9.96	84.3	74.4	9.18	87.8	95.5	75.8	92.9	80.9	82.4	76.8	97.3	77.5	8	73.7	97.8	87.3	88.8	1.86	90.5	83.7	94.7
$Al_2O_3$	3.6	3.	2.0	2.0	pu	3.8	4.4	2.6	<u>~</u>	2.6	2.0	3.4	3.4	2.6	3.0	0.5	2.6	9.0	2.5	4.5	3.2	0.8	4.7	4.4	<u></u>	0.8	3.7	4.2	2.0	4.3	2.9	9.0
OgM	3.4	<u>~</u> .	pu	pu	2.6	4.6	3.6	3.0	4.4	4.0	pu	3.4	2.3	3.7	4.	3.5	3.7	2.2	2.7	3.6	4.	pu	3.6	2.8	8.9	pu	4.8	4.5	pu	4.7	3.9	pu
Ь	5	9	7	&	6	0	=	12	_	2	$\sim$	4	2	9	_	&	_	2	$\sim$	4	2	9	7	8	6	_	2	$\sim$	4	2	9	_
>	w57.11	w57.11	w57.11	w57.11	w57.11	w57.11	w57.11	w57.11	w57.12	w57.12	w57.12	w57.12	w57.12	w57.12	w57.12	w57.12	w57.13	w57.13	w57.13	w57.14	w57.14	w57.14	w57.14	w57.14	w57.14	w57.15						

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ZrO <sub>2</sub>	0.007	0.007	0.003	0.008	900.0	900.0	0.015	0.033	0.009	0.034	0.015	0.007	0.033	900.0	0.004	0.003	0.034	0.031	900.0	900.0	0.007	0.038	0.032	0.017	0.031	0.007	0.033	0.005	0.005	0.036	900'0	0.035
SrO	0.168	0.167	900'0	0.169	0.005	0.233	0.042	0.068	0.125	0.062	0.055	0.128	0.064	0.129	0.002	0.015	0.063	0.065	900'0	900'0	900'0	0.063	0.062	0.115	0.062	900'0	0.062	0.008	0.008	0.061	0.008	0.063
$Rb_2O$	0.001	0.00	pu	0.00	pu	0.00	0.003	0.004	0.00	0.003	0.003	0.00	0.003	0.00	pu	pu	0.003	0.003	pu	pu	pu	0.004	0.003	0.002	0.003	pu	0.004	pu	pu	0.003	pu	0.003
As <sub>2</sub> O <sub>3</sub>	900'0	0.011	pu	900'0	pu	0.007	0.052	0.119	pu	0.102	0.019	0.007	0.115	0.021	0.504	0.429	0.109	0.119	0.108	0.120	0.107	0.098	0.108	0.014	0.137	0.109	0.122	pu	pu	0.122	pu	0.116
ZnO	0.007	900'0	pu	900'0	0.007	0.008	0.025	0.024	0.01	0.017	0.023	0.010	0.021	0.004	pu	pu	0.023	0.022	900'0	0.008	900.0	0.021	0.025	0.023	0.019	0.008	0.024	0.002	0.003	0.017	0.003	0.022
CnO	pu	0.002	pu	0.002	pu	0.001	0.108	0.012	pu	0.011	0.002	0.004	0.017	pu	pu	pu	0.014	0.011	0.005	0.009	0.015	0.014	0.014	0.007	0.009	0.008	0.011	pu	0.003	0.009	pu	0.009
$Fe_2O_3$	1.164	1.124	0.156	1.139	0.187	1.058	0.612	1.152	0.736		0.552	1.307	1.179	0.914	0.101	0.125	1.199	1.087	0.433	0.404	0.436	1.306	1.170	1.571	1.026	0.416	1.109	0.912	0.870	1.132	0.900	1.173
MnO	0.038	0.013	pu	0.031	pu	0.039	0.453	0.585	0.093	0.539	0.638	0.101	0.586	0.031	pu	0.067	0.539	0.550	0.004	pu	pu	0.569	0.595	0.218	0.530	pu	0.605	1.005	0.988	0.512	1.024	0.585
CaO	21.3	21.3	14.9	21.6	15.4	21.2	25.0	28.5	24.5	26.8	22.8	24.7	27.9	22.4	9.1	13.3	26.6	26.7	9.3	8.6	9.5	24.0	27.4	23.7	27.8	9.4	26.8	6.6	9.6	26.2	9.6	26.6
K <sub>2</sub> O	2.0	2.0	pu	2.0	0.3	2.2	4.4	4.3	2.0	3.9	3.7	<u>~</u>	4.	9.1	pu	pu	3.9	4.2	0.0	0.2	0.2	4.	4.2	3.5	4.0	0.2	4.0	0.2	0.2	3.8	0.2	4.
ū	9.0	9.0	pu	9.0	pu	0.5	9.0	pu	0.5	pu	9.0	0.5	pu	9.0	pu	9.0	pu															
SO3	0.7	<u></u>	9:1	6.0	6.0	6.0	0.8	0.8	6.0	0.8	2.1	3.0	0.5	3.8	0.3	0.7	7.	2.0	pu	pu	pu	4.0	9.0	1.7	9:	pu	3.7	pu	pu	2.2	pu	2.0
P <sub>2</sub> O <sub>5</sub>	Ξ.	<u></u>	pu	pu	pu	5.	3.9	2.7	4.	2.6	3.4	<u>.</u> 5	2.6	1.2	pu	pu	2.4	2.9	pu	pu	pu	2.4	2.8	3.0	2.2	pu	3.2	pu	pu	2.4	pu	2.8
SiO <sub>2</sub>	9.98	86.5	93.0	86.4	91.2	85.6	81.5	BO.I	84.I	79.2	76.7	85.5	78.6	80.8	95.3	1.06	78.1	76.4	85.3	92.4	87.4	83.3	9.08	76.2	73.5	1.68	9.62	61.7	87.0	9.08	89.7	78.4
Al <sub>2</sub> O <sub>3</sub>	3.3	3.8	9.0	3.5	0.7	3.4	8.9	4.5	2.2	4.2	4.4	3.5	4.3	2.8	pu	pu	4.2	4.	pu	9.0	0.5	4.3	4.6	3.9	3.8	pu	4.7	pu	0.5	4.0	9.0	4.5
OgM	3.9	4.0	pu	4.6	pu	5.8	3.5	3.8	2.7	3.6	<u></u>	3.7	3.9	4.5	2.1	pu	3.4	4.0	2.1	2.6	2.2	4.0	4.6	4.0	2.5	2.4	4.0	2.3	2.0	2.5	2.3	3.8
۵	2	$\sim$	4	2	9	7	_	2	$\sim$	4	2	9	_	$\infty$	6	0	=	_	2	$\sim$	4	2	9	_	&	6	_	2	$\sim$	4	2	9
≯	w57.15	w57.15	w57.15	w57.15	w57.15	w57.15	w57.16	w57.16	w57.16	w57.16	w57.16	w57.16	w57.16	w57.16	w57.16	w57.16	w57.16	w57.17	w57.18	w57.18	w57.18	w57.18	w57.18	w57.18								

$ZrO_2$	0.005	0.008	900.0	0.015	0.002	900.0	0.009	900.0	0.005	0.007	0.013	0.014	0.007	0.040	0.003	0.004	0.024	0.023	0.022	0.018	0.023	0.003	0.002	0.023	0.005	0.003	0.022	0.018	0.017	900.0	0.009	0.005
SrO	0.007	0.168	0.020	0.099	0.014	900'0	0.166	0.167	0.015	900'0	0.047	0.048	900'0	0.063	0.003	910.0	0.065	0.064	0.065	0.053	0.067	0.012	0.009	0.063	0.014	900'0	0.067	0.054	0.067	0.013	0.195	0.340
$Rb_2O$	pu	0.00	pu	0.00	pu	pu	0.00	0.00	pu	pu	0.004	0.003	pu	0.003	0.00	pu	0.003	0.003	0.003	0.003	0.003	0.00	pu	0.003	0.00	0.00	0.003	0.003	0.003	0.00	0.00	0.001
$As_2O_3$	pu	9000	pu	pu	0.810	0.122	0.008	pu	0.237	0.105	0.013	0.022	0.113	0.119	0.065	0.014	0.222	0.223	0.214	0.064	0.218	0.236	pu	0.216	0.235	1.169	0.225	0.010	pu	0.233	0.007	0.009
ZnO	0.002	0.012	0.002	910.0	0.002	0.008	0.008	0.007	0.00	9000	0.021	0.022	0.007	0.022	pu	0.012	0.027	0.027	0.029	0.021	0.026	0.015	pu	0.027	0.021	0.002	0.021	0.022	0.031	0.020	9000	0.003
CnO	0.002	pu	pu	0.00	pu	0.014	pu	pu	pu	0.011	9000	0.012	0.011	0.013	pu	090.0	0.009	0.007	0.010	0.003	0.009	0.002	pu	900'0	0.005	pu	0.007	0.002	9000	0.004	pu	pu
$Fe_2O_3$	0.887	414.1	0.169	1.429	0.227	0.424	1.400	1.175	0.313	0.418	1.323	0.484	0.419	1.240	0.082	0.963	1.192	1.146	1.157	0.516	1.158	1.248	0.187	6  .	1.257	0.490	1.167	0.594	0.568	1.280	0.943	0.533
MnO	0.985	0.044	pu	0.151	0.312	pu	0.046	0.028	0.256	pu	0.268	099.0	pu	0.678	pu	2.213	0.673	0.728	0.698	0.545	0.738	1.400	pu	0.714	1.375	pu	0.656	0.530	0.645	1.438	0.014	0.004
CaO	9.6	<u>8</u>	15.4	21.7	12.5	0.01	17.5	21.4	4.4	9.5	25.7	24.7	9.5	27.8	8.2	12.6	26.8	26.4	26.1	20.9	27.1	1.7	14.9	26.6	12.2	13.0	26.3	22.7	24.3	12.3	19.8	0.1
$K_2O$	0.2	2.6	pu	3.3	0.2	0.0	2.5	2.0	pu	0.0	4.9	3.9	0.0	4.2	0.2	0.0	3.7	3.5	3.4	3.6	3.6	0.2	pu	3.6	0.3	9.0	3.5	3.9	3.7	0.3	2.1	3.9
D	pu	0.5	pu	0.5	pu	pu	0.5	4.0	pu	pu	pu	9.0	pu	pu	pu	pu	pu	pu	pu	9.0	pu	0.2	pu	pu	pu	pu	pu	0.5	0.5	0.2	0.3	0.5
SO3	pu	9.0	0.8	0.3	6.0	pu	4.0	0.7	0.7	pu	2.9	9:1	pu	6:	pu	9.0	6.0	=:	0.5	4.8	9.0	4.0	6.0	0.8	9.0	9.0	0.7	9.0	9.0	9.0	4.0	pu
$P_2O_5$	pu	<u>4</u> .	pu	2.3	pu	pu	4.	<u> </u>	pu	pu	3.	3.3	pu	2.8	pu	pu	2.0	2.1	1.7	3.	6:1	pu	pu	8.	pu	pu	<u>8</u> .	2.7	3.	pu	pu	<u>-</u> .
SiO <sub>2</sub>	89.3	88.8	94.2	9.18	8.96	92.4	88.4	87.6	97.1	91.4	78.8	77.4	6.68	78.2	94.2	75.4	66.3	65.5	62.2	62.3	65.8	72.2	77.4	65.7	71.4	8	66.3	9.79	67.2	76.0	6.69	73.8
$Al_2O_3$	9.0	3.8	9.0	3.0	Ξ	0.5	3.9	4.0	6.0	0.8	4.9	4.7	0.5	4.9	4.	1.2	2.7	2.2	2.2	 	2.2	1.2	pu	2.3	1.2	<u>4</u> .	2.3	3.2	3.5	<u>4</u> .	<u>~</u>	1.5
OgM	2.0	5.2	pu	3.3	pu	2.4	4.9	4.5	pu	2.5	3.3	3.8	2.6	3.7	4.2	pu	pu	2.4	pu	pu	2.1	pu	pu	2.3	pu	pu	pu	pu	2.7	pu	2.4	3.4
Ь	7	_	7	$\sim$	4	2	9	_	_	7	$\sim$	4	2	9	_	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	15	_	2
<b>*</b>	w57.18	w57.19	w57.19	w57.19	w57.19	w57.19	w57.19	w57.19	w57.20	99M	99M	99M	99M	99M	99M	99M	99M	99M	99M	99M	99M	99M	99M	99M	79m	79m						

$ZrO_2$	910.0	0.014	0.008	0.003	0.005	0.004	0.024	0.024	900'0	0.009	0.007	0.005	0.008	0.002	0.005	0.005	0.002	0.003	0.005	0.002	900'0	0.004	0.002	0.005	900.0	0.005	0.012	0.012	0.023	0.023	0.02	0.002
SrO	0.051	0.1	0.205	0.007	0.012	0.012	990.0	690.0	0.296	0.170	0.132	0.353	0.149	0.007	900.0	0.182	0.004	0.007	0.014	0.004	900.0	0.002	0.007	0.273	0.002	0.002	0.030	0.031	0.067	0.068	0.065	0.009
$Rb_2O$	0.004	0.007	0.00	pu	0.00	0.007	0.003	0.003	0.00	0.00	0.00	0.002	0.00	pu	0.00	0.00	pu	pu	pu	pu	0.00	pu	pu	0.00	pu	pu	0.015	0.015	0.003	0.003	0.002	pu
$As_2O_3$	0.007	0.049	0.015	910.0	0.196	0.135	0.134	0.137	0.009	0.009	pu	0.007	0.007	0.224	pu	0.037	pu	0.017	0.458	pu	pu	0.341	910.0	0.007	0.440	0.443	0.011	0.020	0.164	0.147	0.143	pu
ZnO	0.026	0.013	0.003	pu	0.014	0.015	0.027	0.026	0.002	0.007	0.004	0.003	0.005	0.00	0.00	900.0	0.005	pu	0.00	0.004	0.002	0.007	pu	900'0	0.002	pu	0.039	0.034	0.025	0.028	0.031	0.001
CnO	0.014	0.007	pu	pu	pu	0.00	0.011	0.003	pu	0.007	0.002	pu	0.00	pu	0.007	pu	pu	pu	pu	pu	pu	pu	pu	pu	910.0	0.022	0.011	0.012	900'0	0.012	0.002	pu
$Fe_2O_3$	1.311	1.381	1.008	0.165	1.144	1.282	1.300	1.413	0.904	1.350	0.982	0.563	0.852	0.268	0.191	0.872	0.232	0.142	0.138	0.233	0.196	0.070	0.174	0.570	0.021	0.017	0.479	0.538	1.289	1.317	1.039	0.195
MnO	0.255	0.156	0.017	pu	1.230	1.374	0.635	0.658	0.027	0.019	0.004	pu	0.018	0.039	pu	0.014	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	0.895	0.889	0.667	0.663	0.661	pu
CaO	23.5	23.7	20.7	15.3	<u> </u>	12.2	24.5	24.3	<u> </u>	21.9	21.9	11.5	21.3	14.9	13.8	18.9	16.9	15.1	0.91	9.91	13.4	8.2	14.9	6.7	6.3	6.3	15.0	15.2	22.1	24.7	24.3	15.1
$K_2O$	4.8	3.2	2.3	pu	0.3	0.3	3.3	3.4	3.4	6.	2.0	4.0	<u>~</u>	pu	9.0	2.0	0.0	pu	pu	0.0	9.0	pu	pu	3.5	2.5	2.5	9.6	9.3	3.0	3.4	2.9	pu
D	pu	9.0	0.3	pu	0.2	0.2	0.3	0.3	9.0	9.0	0.3	9.0	0.3	pu	pu	0.5	pu	pu	pu	pu	pu	pu	pu	0.3	9.0	0.7	4.0	4.0	4.0	9.0	9.0	pu
SO3	8.0	7.3	0.8	6.0	4.0	9.0	9.0	0.7	0.3	0.7	=:	pu	9.1	0.8	0.5	5.1	9.0	6.0	0.5	0.7	4.0	0.2	6.0	0.5	pu	pu	6.0	<u>1.5</u>	4.	0.	pu	6.0
$P_2O_5$	2.3	3.2	0.	pu	pu	pu	2.1	2.1	pu	pu	pu	9.1	pu	pu	pu	6:1	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	3.4	3.0	2.1	2.1	2.1	pu
$SiO_2$	62.4	63.3	75.1	79.2	77.0	77.3	0.69	69.3	77.3	9.69	73.0	77.7	71.0	9.08	80.7	0.69	77.6	78.8	80.2	75.4	80.7	76.3	78.6	76.5	78.2	75.3	64.5	1.49	68.2	2.99	65.0	9.9/
$Al_2O_3$	2.1	2.5	2.0	pu	0.	<u></u>	2.6	2.4	2.6	2.2	2.3	1.7	1.7	pu	<u></u>	<u>.</u> 5	pu	pu	0.5	pu	<u></u>	pu	pu	9.	pu	pu	<u>.</u> 5	<u>8.</u>	2.4	2.3	2.1	pu
OgM	pu	2.4	3.4	pu	pu	pu	pu	pu	4.	2.3	3.4	4.2	3.3	pu	pu	2.7	pu	pu	pu	pu	pu	pu	pu	4.5	pu	pu	4.9	3.8	pu	2.0	pu	pu
Ь	3	4	2	9	7	∞	6	0	=	12	<u> </u>	4	_	2	$\sim$	4	2	9	7	∞	6	0	=	12	_	2	$\sim$	4	2	9	7	<b>∞</b>
>	79M	79m	79m	79m	79m	79m	79m	79m	79m	79m	79m	79m	89M	%9w	%9w	89w	%9w	89M	89M	%9w	%9w	%9w	89M	89M	l.69w	I.69w	l.69w	l.69w	l.69w	l.69w	I.69w	N.69.1

690'0	0.065 0.023				0.024	0.024	0.009	0.010	0.01	0.019	0.031	0.010	.005	:005	900:	.005	013	.005	.013	.025	.023	.024	.025	.024	.023	9.014	0.012	0.040	0.011	900'(	0.022
	0.065	690	_								_	$\cup$	O	0	0	0	0	0	0	0	0	0	O	O	O	O	0	$\cup$	$\cup$	0	$\cup$
$\sim$		0	90.0	0.322	990.0	0.064	0.003	0.002	0.045	0.057	090.0	0.058	0.015	0.013	0.002	0.013	0.093	0.013	0.048	990.0	0.067	0.068	0.065	690.0	0.067	0.055	0.030	0.052	0.029	0.002	690'0
0.00	0.003	0.003	0.003	0.00	0.003	0.003	0.00	0.00	0.004	0.003	0.004	0.009	pu	pu	pu	pu	0.002	pu	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.004	910.0	0.003	0.015	pu	0.002
0.163	0.127	0.138	0.141	0.009	0.146	0.133	pu	pu	pu	0.049	0.100	0.075	0.313	0.236	0.005	0.239	pu	0.241	pu	0.133	0.158	0.138	0.157	0.141	0.132	pu	0.015	0.133	0.010	0.447	0.147
0.025	0.026	0.028	0.029	0.00	0.033	0.027	0.170	0.168	0.027	0.024	0.020	0.040	0.003	0.002	0.014	0.004	0.002	0.003	0.024	0.028	0.029	0.028	0.029	0.030	0.024	0.025	0.030	0.034	0.037	0.00	0.031
0.008	0.002	0.010	600.0	pu	0.004	0.013	pu	pu	0.015	0.003	0.010	0.007	pu	0.002	0.130	0.005	pu	0.00	0.011	0.008	0.004	0.007	0.003	0.009	0.008	0.010	0.004	0.014	0.011	0.024	900'0
1.340	1.260	1.237	1.300	0.684	1.270	1.289	0.038	0.01	1.345	0.602	1.1	0.639	961.0	0.180	0.023	0.169	0.527	0.205	1.239	1.245	1.317	1.335	1.258	1.304	1.257	1.328	0.502	1.197	0.514	0.015	1.095
0.680	919.0	0.675	0.709	0.022	0.694	0.636	pu	pu	0.098	999.0	0.537	1.091	0.117	0.055	pu	0.068	pu	0.083	0.189	0.661	0.668	0.659	0.684	0.721	0.704	0.157	0.928	0.640	0.894	pu	0.610
24.3	23.8	25.0	23.4	0.	24.8	23.5	6.3	6.3	23.9	9.61	26.0	14.9	12.7	12.9	5.9	12.5	9.01	12.6	22.6	23.6	22.7	23.8	24.3	24.3	24.2	26.3	15.4	23.7	15.1	6.1	24.6
3.4	3.2	3.6	3.2	3.7	3.6	3.3	2.8	2.8	5.3	3.8	4.0	8.8	pu	pu	3.3	pu	7.1	pu	5.3	3.3	3.0	3.–	3.0	3.3	3.4	6.4	9.5	5.0	9.3	2.4	2.9
9.0	0.3	0.3	0.3	0.5	4.0	0.3	9.0	0.5	pu	0.5	pu	4.0	pu	pu	9.0	pu	0.5	pu	pu	0.3	0.3	0.3	0.3	0.3	0.3	pu	0.4	pu	0.4	9.0	9.4
2.8	0.3	4.0	6.0	pu	2.1	1.5	=	0.8	0:	9.0	0.8	0.	0.3	0.5	0.2	9.0	0.4	9.0	0.8	6.0	2.2	<u></u>	9.1	9.0	0.5	0.8	=	0.8	1.2	pu	pu
2.2	2.1	2.2	2.1	1.2	2.5	2.0	pu	pu	2.2	2.2	6:1	3.6	pu	pu	pu	pu	pu	pu	<u>8</u> .	2.2	2.0	2.0	6:1	2.1	2.0	2.0	2.8	2.8	3.2	pu	2.2
1.89	68.0	70.0	68.3	74.9	9.79	64.0	80.2	78.9	8.69	70.3	63.2	59.3	82.5	9.62	1.08	80.3	76.0	82.2	6.69	9.69	67.8	68.3	64.0	70.6	70.9	66.4	6.99	67.2	4.19	77.1	65.8
2.5	2.1	2.7	2.4	9.	2.8	2.1	pu	pu	2.5	3.9	2.3	<u>4</u> .	pu	pu	pu	pu	1.2	pu	3.2	2.4	2.5	2.7	2.5	2.5	2.2	3.4	6.1	<u>4</u> .	7.	pu	2.2
pu	pu	2.0	pu	3.7	2.0	pu	pu	pu	pu	2.2	2.2	2.7	pu	pu	pu	pu	3.0	pu	2.1	2.1	pu	2.1	2.2	2.5	pu	2.2	3.7	pu	4.	pu	2.1
6	0	=	12	<u>1</u> 3	4	15	9		<u>&amp;</u>	6	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34	35	_	2	Υ	4	2
	2.5 68.1 2.2 2.8 0.4 3.4	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 2.0 2.7 70.0 2.2 0.4 0.3 3.6	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 2.0 2.7 70.0 2.2 0.4 0.3 3.6 nd 2.4 68.3 2.1 0.9 0.3 3.2	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 2.7 70.0 2.2 0.4 0.3 3.6 nd 2.4 68.3 2.1 0.9 0.3 3.2 3.7 1.6 74.9 1.2 nd 0.5 3.7	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 0.4 0.3 3.2 0.3 3.2 0.4 0.3 3.2 0.4 0.3 3.2 0.4 0.3 3.2 0.4 0.3 3.2 0.4 0.3 3.2 0.4 0.5 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.4 0.3 3.2 0.4 0.3 3.2 0.4 0.3 3.2 0.4 0.3 3.2 0.3 3.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 2.2 0.4 0.3 3.2 3.2 nd 2.4 68.3 2.1 0.9 0.3 3.2 3.2 nd 2.8 67.6 2.5 2.1 0.4 3.6 nd nd 80.2 nd 1.1 0.6 2.8	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 2.2 0.4 0.3 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 0.3 3.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 2.7 70.0 2.2 0.4 0.3 3.2 3.2 nd 2.4 68.3 2.1 0.9 0.3 3.2 3.2 3.7 1.6 74.9 1.2 nd 0.5 3.7 2.0 2.8 67.6 2.5 2.1 0.4 3.6 nd nd 80.2 nd 1.1 0.6 2.8 nd 0.8 0.5 2.8 nd 0.8 0.5 2.8 nd 2.5 69.8 2.2 1.0 nd 5.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 2.2 0.4 0.3 3.2 3.2 0.4 0.3 3.2 0.3 3.2 0.4 68.3 2.1 0.9 0.3 3.2 3.2 0.2 0.4 0.3 3.2 3.2 0.2 0.4 0.3 3.2 0.2 0.4 0.5 0.3 3.2 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 2.2 0.4 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 0.3 3.2 0.3 0.3 3.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 2.7 70.0 2.2 0.4 0.3 3.2 3.2 nd 2.4 68.3 2.1 0.9 0.3 3.2 3.2 3.7 1.6 74.9 1.2 nd 0.5 3.7 2.0 2.8 67.6 2.5 2.1 0.4 3.6 nd nd 80.2 nd 1.1 0.6 2.8 nd 78.9 nd 0.8 0.5 2.8 nd 2.5 69.8 2.2 1.0 nd 5.3 2.2 2.2 3.9 70.3 2.2 0.6 0.5 3.8 2.7 1.4 59.3 3.6 1.0 0.4 8.8	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 0.3 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.4 0.5 0.3 3.2 0.4 0.4 0.5 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.2 2.7 70.0 2.1 0.3 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 3.2 nd 0.5 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.4 0.4 0.5 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 nd 2.2 7.0 2.2 0.4 0.3 3.2 3.2 nd 2.4 68.3 2.1 0.9 0.3 3.2 3.2 nd 2.8 67.6 2.5 2.1 0.4 3.6 3.7 nd 2.1 64.0 2.0 1.5 0.3 3.3 nd nd 78.9 nd 0.8 0.5 2.8 nd 0.8 0.5 2.8 2.2 2.3 69.8 2.2 1.0 nd 5.3 2.2 2.3 63.2 2.3 63.2 1.0 nd 5.3 3.8 2.2 2.3 63.2 1.0 nd 5.3 3.8 2.2 2.3 63.2 1.0 nd 5.3 3.8 2.2 1.0 nd 5.3 3.8 2.2 1.0 nd 5.3 3.8 nd nd 78.5 nd 0.3 nd nd nd 79.6 nd 0.3 nd nd nd 79.6 nd 0.5 0.6 0.5 3.3 nd nd nd 79.6 nd 0.5 0.6 0.5 3.3 nd nd nd 79.6 nd 0.2 0.6 0.5 3.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 0.3 3.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.0 68.0 2.1 0.3 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 3.2 0.3 3.2 3.2 3.2 0.3 3.2 3.2 3.2 0.3 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.2 0.4 0.3 3.2 0.2 0.4 0.3 3.2 0.2 0.4 0.3 0.3 3.2 0.2 0.4 0.3 0.3 0.3 0.4 0.4 0.2 0.2 0.4 0.2 0.4 0.3 0.4 0.4 0.2 0.4 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.5 0.4 0.4 0.5 0.4 0.5 0.4 0.4 0.5 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.5 0.4 0.4 0.5 0.4 0.5 0.4 0.	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 3.2 3.2 0.3 3.2 3.2 3.2 0.3 3.2 3.2 3.2 0.3 3.2 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.2 0.4 68.3 2.1 0.9 0.3 3.2 0.2 0.4 0.5 3.7 0.2 2.8 67.6 2.5 2.1 0.4 3.6 0.3 0.3 0.3 0.3 0.4 0.4 0.2 0.2 0.5 0.3 0.3 0.3 0.4 0.3 0.3 0.3 0.4 0.3 0.3 0.4 0.4 0.3 0.4 0.4 0.3 0.4 0.4 0.3 0.4 0.4 0.3 0.4 0.4 0.3 0.4 0.4 0.3 0.4 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.5 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	nd 2.5 68.1 2.2 2.8 0.4 3.4  nd 2.1 68.0 2.1 0.3 0.3 3.2  2.0 2.7 70.0 2.2 0.4 0.3 3.2  3.7 1.6 74.9 1.2 nd 0.5 3.7  2.0 2.8 67.6 2.5 2.1 0.4 3.6  nd 2.1 64.0 2.0 1.5 0.3 3.3  nd nd 80.2 nd 1.1 0.6 2.8  nd nd 82.2 nd 0.8 0.5 2.8  nd nd 82.5 nd 0.3 nd nd nd nd 82.5 nd 0.3 nd nd nd 82.1 nd 0.5 nd nd 2.1 3.2 69.9 1.8 0.8 nd 5.3	nd 2.5 68.1 2.2 2.8 0,4 3.4 1.2 1.0 1.2 1.0 1.3 1.2 1.0 1.3 1.0 1.3 1.2 1.0 1.3 1.2 1.0 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.0 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.4 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	nd 2.5 68.1 2.2 2.8 0.4 3.4  nd 2.1 68.0 2.1 0.3 0.3 3.2  2.0 2.7 70.0 2.2 0.4 0.3 3.2  3.7 1.6 74.9 1.2 nd 0.5 3.7  2.0 2.8 67.6 2.5 2.1 0.4 3.6  nd nd 80.2 nd 1.1 0.6 2.8  nd nd 78.9 nd 0.8 0.5 2.8  nd nd 78.9 nd 0.8 0.5 2.8  nd nd 82.5 nd 0.3 3.8  nd nd 82.5 nd 0.3 3.8  nd nd 80.1 nd 0.6 nd nd nd nd 80.3 nd 0.6 nd nd 2.1 2.6 0.6 0.5 3.3  nd nd 80.1 nd 0.4 0.5 nd nd nd 80.3 nd 0.6 nd nd 2.1 2.6 0.6 0.5 3.3  2.1 2.4 69.6 2.2 0.9 0.3 3.3  nd nd 82.2 nd 0.6 nd 0.5 nd nd nd 82.1 nd 0.6 nd 0.5 nd nd 0.6	nd 2.5 68.1 2.2 2.8 0.4 3.4  nd 2.1 68.0 2.1 0.3 0.3 3.2  2.0 2.7 70.0 2.2 0.4 0.3 3.2  3.7 1.6 74.9 1.2 nd 0.5 3.7  2.0 2.8 67.6 2.5 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0.5 3.7   2.0 2.8 67.6 2.5 2.1 0.4 3.6   3.7 1.6 74.9 1.2 nd 0.5 3.7   2.0 2.8 67.6 2.5 2.1 0.4 3.6   1.1 0.6 2.8   1.2 3.9 70.3 2.2 0.6 0.5 2.8   1.2 2.3 63.2 1.9 0.8 nd 4.0   2.7 1.4 59.3 3.6 1.0 0.4 8.8   1.4 59.3 3.6 1.0 0.4 0.5 nd nd   1.4 59.3 3.6 1.0 0.4 0.5   1.5 1.4 59.3 1.6 0.6 0.5 3.3   1.6 1.4 59.3 1.6 0.6 0.5 3.3   1.7 1.4 59.3 1.6 0.6 0.5 1.0   1.8 0.8 1.1 0.4 0.5   1.9 0.8 1.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	nd 25 68.1 2.2 2.8 0.4 3.4 nd 2.1 68.0 2.1 0.3 0.3 3.2 2.0 2.7 70.0 2.2 0.4 0.3 3.2 3.2 nd 2.4 68.3 2.1 0.9 0.3 3.2 3.2 2.0 2.8 67.6 2.5 2.1 0.4 3.6 2.2 nd 2.1 64.0 2.0 1.5 0.3 3.3 nd nd 80.2 nd 0.8 0.5 2.8 nd 0.8 nd 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.3 0.4 0.5 0.3 0.4 0.5 0.3 0.4 0.5 0.3 0.4 0.5 0.3 0.4 0.5 0.3 0.4 0.5 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.4 0.5 0.3 0.3 0.4 0.5 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 25 68.1 2.2 2.8 0.4 3.4 nd 2.0 2.1 68.0 2.1 0.3 0.3 3.2 2.0 0.4 0.3 3.2 0.2 2.0 0.4 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.2 0.3 3.3 0.3 3.3 0.3 3.3 0.3 0.3 3.3 0.3 0	nd 25 68.1 22 2.8 0.4 3.4 nd 2.5 68.0 2.1 0.3 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 2.0 0.4 0.3 3.2 3.2 0.4 0.3 3.2 3.2 0.4 0.3 3.2 3.2 0.2 0.4 0.3 3.2 3.2 0.2 0.4 0.3 3.2 3.2 0.2 0.4 0.3 3.2 0.2 0.4 0.3 3.2 0.2 0.4 0.3 3.2 0.2 0.4 0.3 3.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.5 68.0 2.1 0.3 0.3 3.2 2.0 2.2 0.4 0.3 3.5 3.2 2.0 2.2 0.4 0.3 3.2 3.2 2.0 2.8 0.4 0.3 3.2 3.2 2.0 2.8 6.7.6 2.5 2.1 0.4 0.3 3.5 3.2 2.0 2.8 6.7.6 2.5 2.1 0.4 3.6 3.3 3.3 nd nd 80.2 nd 1.1 0.6 2.8 3.3 3.3 2.2 0.6 0.5 3.8 2.2 1.0 nd 5.3 3.3 2.2 2.3 6.9.8 2.2 1.0 nd 5.3 3.8 nd nd 82.5 nd 0.3 nd nd 82.5 nd 0.5 nd nd nd 80.1 nd 0.0 0.4 0.5 nd nd nd 80.1 nd 0.0 0.4 0.5 nd nd nd 80.2 nd 0.6 nd nd nd 80.2 nd 0.6 nd nd 2.1 2.6 0.9 1.8 0.8 nd 5.3 3.0 2.1 2.4 69.6 2.2 0.9 0.3 3.3 2.1 2.4 69.6 2.2 0.9 0.3 3.3 2.1 2.7 68.3 2.0 1.3 0.3 3.1 2.2 2.5 64.0 1.9 1.6 0.3 3.3 3.0 2.5 2.5 64.0 1.9 1.6 0.3 3.3 3.4 66.4 2.0 0.8 nd 6.4 3.3 nd 1.4 67.2 2.8 0.8 nd 6.4 5.0 1.1 0.4 9.5 0.3 3.3 1.4 67.2 2.8 0.8 nd 6.5 0.3 3.3 1.4 67.2 2.8 0.8 nd 6.5 0.5 0.3 3.3 1.4 6.5 0.2 2.8 0.8 nd 6.5 0.5 0.3 3.3 1.4 6.5 0.2 2.8 0.8 nd 6.5 0.5 0.3 3.3 1.4 6.5 0.3 3.3 1.4 6.5 0.2 2.8 0.8 nd 6.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 3.3 1.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 2.8 0.4 0.4 6.5 0.3 3.3 1.4 6.5 0.3 2.2 0.3 3.3 1.4 6.5 0.3 3.	nd 2.5 68.1 2.2 2.8 0.4 3.4 nd 2.5 68.0 2.1 0.3 0.3 3.2 2.2 0.4 0.3 3.2 3.2 2.2 0.4 0.3 3.2 3.2 0.4 0.3 3.2 3.2 0.4 0.3 3.2 3.2 0.4 0.3 3.2 3.2 0.4 0.3 3.2 0.3 3.2 0.2 0.4 0.3 3.2 0.3 3.2 0.2 0.2 0.4 0.3 3.2 0.3 3.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	2.5 68.1 2.2 2.8 0.4 2.1 68.0 2.1 0.3 0.3 2.7 70.0 2.2 0.4 0.3 2.4 68.3 2.1 0.9 0.3 1.6 74.9 1.2 nd 0.5 2.8 67.6 2.5 2.1 0.4 2.1 64.0 2.0 1.5 0.3 1.4 64.0 2.0 1.5 0.3 1.4 59.3 2.2 0.6 0.5 1.3 63.2 1.9 0.8 nd 1.4 59.3 3.6 1.0 nd 1.4 59.3 3.6 1.0 nd 1.4 59.3 3.6 1.0 nd 1.5 76.0 nd 0.5 nd 1.2 76.0 nd 0.6 nd 2.5 67.8 2.0 2.2 0.3 2.5 64.0 1.9 1.6 0.3 2.5 64.0 1.9 1.6 0.3 2.5 64.0 1.9 1.6 0.3 2.5 70.6 2.1 0.6 1.9 66.9 2.8 1.1 0.4 1.9 66.9 2.8 1.1 0.4 1.1 67.2 2.8 0.8 1.1 0.4 1.2 66.4 3.2 1.2 0.8 1.1 0.4 1.2 66.4 3.2 1.2 0.8 1.1 0.4 1.2 66.9 2.8 1.1 0.4 1.1 0.7 1 nd 0.6

$ZrO_2$	0.025	0.024	0.013	0.024	0.020	0.003	0.023	0.009	0.002	0.023	0.023	0.022	900.0	0.005	0.024	0.022	0.014	0.013	0.023	0.014	0.005	900.0	900.0	0.017	0.008	900.0	900.0	900.0	910.0	0.003	0.012	0.040
SrO	990'0	0.068	0.039	0.071	0.067	0.018	990.0	0.002	0.007	0.068	0.064	0.067	0.002	0.002	0.070	0.050	0.052	980.0	990.0	0.085	0.014	0.002	910.0	0.089	0.143	0.002	0.321	0.322	0.098	0.015	0.030	0.068
$Rb_2O$	0.003	0.003	0.004	0.002	0.002	pu	0.003	0.00	pu	0.003	0.003	0.003	pu	pu	0.003	0.002	0.003	0.002	0.003	0.002	pu	pu	0.00	0.002	0.00	pu	0.00	0.00	0.002	pu	0.015	0.004
$As_2O_3$	0.138	0.148	pu	0.143	0.204	0.008	0.128	pu	0.007	0.228	0.130	0.145	0.443	pu	0.169	pu	pu	pu	0.169	pu	0.201	0.437	0.337	pu	0.010	pu	0.008	0.007	pu	0.418	0.011	0.077
ZnO	0.028	0.028	0.022	0.025	0.027	0.00	0.028	0.173	0.002	0.026	0.026	0.025	pu	0.012	0.027	0.030	0.022	0.002	0.032	0.002	pu	0.002	0.003	0.024	0.007	0.013	0.00	pu	0.022	0.00	0.032	0.039
CnO	0.011	0.008	0.007	0.005	0.007	pu	0.008	0.003	pu	0.010	0.007	0.005	0.023	pu	0.005	0.002	0.015	pu	0.011	pu	pu	0.020	pu	900.0	pu	pu	pu	pu	0.002	pu	0.012	0.014
$Fe_2O_3$	1.289	1.302	1.224	1.178	1.077	0.201	1.309	0.046	0.203	1.346	1.252	1.222	0.025	0.008	1.076	1.078	1.340	0.491	1.242	0.501	0.169	0.009	0.250	1.607	0.942	0.014	0.497	0.540	1.584	0.145	0.531	1.151
MnO	0.664	0.649	0.126	0.659	0.619	pu	0.679	pu	pu	0.640	0.662	0.640	pu	pu	0.687	0.546	0.200	pu	0.677	pu	0.075	pu	910.0	0.123	0.100	pu	0.013	0.012	0.244	0.077	0.875	1.376
CaO	23.9	23.7	24.1	25.5	22.9	1.91	24.1	6.4	16.7	22.0	23.2	23.3	6.3	5.6	25.5	22.6	23.5	9.01	21.9	11.2	12.9	6.2	15.1	22.5	22.2	5.8	1.01	10.7	19.3	13.0	14.7	20.6
K <sub>2</sub> O	3.5	3.2	4.8	3.0	2.8	0.0	3.3	2.7	pu	<u>~</u> .	3.2	3.4	2.4	2.7	3.0	2.0	4.5	8.9	2.9	7.0	pu	2.5	0.8	4.	6:	2.6	3.3	3.5	3.8	pu	9.2	5.4
ū	0.3	0.3	pu	0.5	9.0	pu	0.33	9.0	pu	0.3	0.3	0.3	9.0	6.0	4.0	9.0	pu	0.5	0.3	0.3	pu	0.7	pu	9.4	9.0	0:	9.0	0.5	9.0	pu	9.4	pu
SO3	1.3	<u>~</u>	0:	9.0	3.2	<u>4</u> .	0.5	0.8	1.2	9.0	0.5	<u></u>	pu	pu	1.7	0.3	<u></u>	0.5	2.7	0.3	9.0	pu	2.9	6.0	<u></u>	pu	0.3	0.2	0.8	0.7	<u></u>	9.0
$P_2O_5$	2.2	2.3	2.1	2.7	2.1	pu	6.	pu	pu	2.2	6.	2.2	pu	pu	2.4	2.5	2.2	pu	1.7	pu	pu	pu	pu	2.1	pu	pu	<u></u>	<u>.</u> 5	2.1	pu	2.9	2.0
$SiO_2$	0.89	6.79	2.99	69.5	63.7	79.4	1.69	78.5	79.5	59.9	9.29	9.99	77.7	80.7	65.8	1.99	1.89	72.0	74.2	72.7	78.0	78.8	76.0	1.69	71.5	82.8	76.2	80.3	6.19	79.3	0.99	53.2
$Al_2O_3$	2.7	2.5	2.4	2.6	2.1	pu	2.4	pu	pu	2.0	2.0	2.5	pu	pu	2.4	3.9	2.6	<u> </u>	2.4	0.	pu	pu	0.7	2.8	<u>8</u> .	pu	=:	<u>-</u> .	2.1	pu	9.1	<u></u>
MgO	2.1	2.2	pu	pu	pu	pu	2.4	pu	pu	pu	pu	pu	pu	pu	pu	2.4	pu	2.5	pu	3.0	pu	pu	pu	2.4	2.0	pu	3.5	4.0	pu	pu	3.4	pu
Ъ	9	_	$\infty$	6	0	=	12	$\underline{\sim}$	4	12	9		<u>&amp;</u>	6	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34	35	_	2
<b>×</b>	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.2	w69.3	w69.3

$ZrO_2$	0.005	0.036	0.023	0.022	0.023	0.002	0.024	900.0	0.005	0.024	0.025	0.022	900.0	0.022	900.0	0.023	900.0	0.005	0.023	0.018	0.004	900'0	0.007	0.005	900.0	900.0	0.008	900.0	0.023	900.0	0.022	0.026
SrO	0.002	0.048	0.069	990.0	0.067	0.007	0.067	0.002	0.002	990.0	990.0	690.0	0.002	0.069	0.002	0.067	0.002	0.212	0.065	0.045	0.325	0.002	0.212	0.015	0.002	0.215	0.204	0.002	990.0	0.002	0.067	0.068
$Rb_2O$	pu	0.003	0.002	0.003	0.003	pu	0.003	pu	pu	0.002	0.003	0.002	pu	0.002	pu	0.003	pu	0.00	0.003	0.004	0.00	pu	0.00	pu	pu	0.00	0.00	pu	0.003	pu	0.003	0.003
$As_2O_3$	0.442	0.130	0.170	0.140	0.153	0.038	0.172	0.632	pu	0.158	0.162	0.244	pu	0.152	pu	0.158	pu	0.018	0.174	0.014	0.012	0.618	900'0	0.353	0.639	pu	pu	900'0	0.144	pu	0.124	0.168
ZnO	pu	0.032	0.027	0.032	0.029	0.00	0.028	0.014	0.013	0.027	0.027	0.025	0.013	0.025	0.010	0.029	0.012	0.003	0.030	0.024	0.005	0.013	0.003	pu	910.0	0.007	0.013	0.015	0.025	0.012	0.028	0.022
CnO	0.027	910.0	0.011	0.008	0.007	0.003	0.009	pu	0.135	0.003	0.010	0.007	0.137	pu	0.139	0.007	0.133	pu	0.008	0.014	pu	pu	pu	0.00	pu	pu	0.00	0.144	0.012	0.136	0.004	0.009
$Fe_2O_3$	910.0	1.150	1.117	1.277	1.211	0.168	1.294	0.025	0.01	1.294	1.288	8	0.028	1.074	0.01	1.279	0.027	1.054	1.262	1.396	0.995	0.012	0   .	0.209	0.013	1.083	1.125	0.009	1.306	0.022	1.224	1.334
MnO	pu	0.663	0.710	0.644	0.641	pu	0.642	pu	pu	0.634	0.615	0.633	pu	0.692	pu	0.650	pu	0.035	0.617	0.305	0.024	pu	pu	pu	pu	0.055	0.074	pu	0.672	pu	0.708	999.0
CaO	0.9	24.0	24.3	23.8	23.3	15.7	23.8	5.8	0.9	22.1	23.1	23.0	5.7	24.7	5.7	23.1	5.9	20.3	22.8	24.3	<u> </u>	5.7	6.61	14.9	5.7	20.7	·   ·	5.8	24.2	5.6	23.8	23.7
$K_2O$	2.3	4.9	3.0	3.2	3.4	pu	3.3	2.9	3.3	3.0	3.0	2.8	3.	3.0	3.3	3.2	3.3	2.3	3.	4.9	3.9	3.0	2.2	pu	3.0	2.4	2.9	3.3	3.4	3.2	3.4	3.3
D	9.0	pu	9.0	9.0	4.0	pu	0.3	0.8	9.0	0.3	0.3	0.4	0.5	4.0	0.5	0.3	9.0	0.3	0.3	pu	4.0	0.8	0.3	pu	0.8	0.3	0.5	0.5	0.3	0.5	0.3	0.4
SO3	pu	0.5	6:1	<u> </u>	3.	0.8	2.3	pu	pu	4.0	2.0	9.0	0.2	0.	0.5	2.4	0.3	2.8	2.6	9.1	0.2	pu	0.7	0.7	pu	0.	0.2	0.3	0.7	0.4	0.3	2.5
$P_2O_5$	pu	2.8	2.3	2.2	2.5	pu	2.0	pu	pu	<u>~</u>	<u>~</u>	6.1	pu	2.2	pu	2.2	pu	<u></u>	6.1	2.4	1.2	pu	pu	pu	pu	=	1.7	pu	2.1	pu	2.1	2.2
$SiO_2$	75.5	8.99	64.4	69.3	65.1	76.2	69.4	79.0	81.5	67.4	69.2	65.2	78.3	64.0	79.5	69.2	81.0	71.9	1.49	67.5	76.0	75.2	70.0	78.2	79.7	72.0	6.79	82.5	6.89	78.0	8.89	68.5
$Al_2O_3$	pu	9:1	2.3	2.4	2.4	pu	2.7	pu	pu	2.4	2.1	2.4	pu	2.0	pu	2.5	pu	2.1	2.1	3.3	2.4	pu	6:1	pu	pu	2.1	6:1	pu	2.5	pu	2.5	2.4
MgO	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.8	pu	pu	3.9	pu	2.4	pu	pu	3.4	2.9	pu	pu	pu	2.2	pu
Ь	3	4	2	9	7	∞	6	0	=	12	<u> </u>	4	12	91		<u>8</u>	6	20	21	22	23	24	25	26	27	28	29	30	3	32	33	34
>	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3	w69.3

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رد	2	4	5	$\infty$	2	7	9	Ñ	7	9	$\infty$	7	7	7	$\sim$	$\sim$	4	$\sim$	$\infty$	7		4	7	7	$\infty$	4	4	$\sim$	2	4	7	_
ZrQ	0.02	0.02	0.00	0.03	0.0	0.04	0.00	0.00	0.02	0.00	0.02	0.00	0.02	0.00	0.02	0.02	0.00	0.02	0.02	0.00	0.00	0.02	0.00	0.02	0.02	0.00	0.00	0.02	0.02	0.00	0.022	0.0
SO	0.068	0.068	0.002	0.051	0.029	990.0	0.003	0.002	990.0	0.01	0.065	0.008	990.0	0.018	0.065	0.064	0.008	0.068	0.067	0.007	0.014	0.069	0.007	0.067	0.067	0.016	0.01	0.064	990.0	910.0	0.067	0.005
$Rb_2O$	0.002	0.002	pu	0.003	0.015	0.004	pu	pu	0.002	pu	0.002	pu	0.003	pu	0.003	0.003	0.00	0.003	0.003	pu	pu	0.003	pu	0.003	0.003	pu	pu	0.003	0.003	pu	0.003	pu
As <sub>2</sub> O <sub>3</sub>	0.131	0.123	pu	0.121	910.0	0.083	pu	pu	0.163	pu	0.134	0.110	0.178	0.062	0.130	0.148	0.087	0.146	0.135	0.008	0.011	0.144	pu	0.138	0.136	0.007	0.196	0.133	0.157	900'0	0.136	pu
ZnO	0.024	0.030	0.015	0.032	0.035	0.033	0.012	0.012	0.023	900.0	0.027	0.00	0.027	0.00	0.028	0.031	pu	0.028	0.023	pu	0.004	0.025	pu	0.027	0.026	0.003	pu	0.026	0.025	0.007	0.025	9000
Ono	900'0	0.011	0.130	0.013	0.011	0.013	0.171	0.156	0.009	pu	0.011	pu	0.007	pu	900'0	0.004	pu	900.0	0.007	pu	pu	0.005	pu	0.011	0.009	pu	pu	0.012	0.009	pu	0.013	pu
$Fe_2O_3$	1.327	1.294	0.024	1.155	0.526	1.194	0.023	0.012	1.297	0.143	1.232	0.202	1.297	0.181	1.238	1.280	0.193	1.246	1.255	0.179	0.208	1.302	0.185	1.324	1.249	0.241	0.132	1.272	1.314	0.255	1.238	0.292
MnO	0.692	0.701	pu	0.635	0.803	1.152	pu	pu	0.683	pu	0.621	pu	0.653	pu	0.672	0.670	pu	0.700	0.775	pu	pu	0.762	pu	0.629	0.730	pu	0.068	0.688	699.0	pu	0.667	pu
Og Og	23.5	24.2	5.4	24.0	15.6	21.5	2.8	0.9	22.9	15.8	22.7	14.9	23.0	15.4	23.5	23.4	13.9	23.1	23.5	15.3	15.3	24.2	1.9	23.6	23.1	12.5	12.5	23.5	22.8	12.6	22.6	15.3
K <sub>2</sub> O	3.3	3.3	<u>~</u> .	5.0	8.5	5.1	3.0	3.2	3.	0.0	3.	0.0	3.	pu	3.3	3.2	4.0	3.2	3.3	pu	0.3	3.3	pu	3.2	3.2	0.0	pu	3.2	3.	0.0	3.1	0.0
Ū	0.3	0.3	4.0	pu	0.3	pu	9.0	0.7	9.0	pu	0.3	pu	9.0	pu	0.3	0.3	pu	4.0	0.3	pu	pu	0.3	pu	0.3	0.3	pu	pu	0.3	0.3	pu	0.3	pu
SO3	9.0	9.0	pu	9.0	1.5	<u> </u>	pu	pu	3.8	0.3	6:1	0.7	5.8	<u> </u>	4.0	<u></u>	0.7	2.4	2.2	0.8	9.0	0.7	0.8	<u>-</u> .	2.3	6.0	0.5	pu	<u>8</u> .	6.0	1.7	9.0
$P_2O_5$	2.0	2.0	pu	2.5	2.4	2.6	pu	pu	2.6	pu	6:1	pu	3.	pu	6:	2.1	pu	2.3	2.4	pu	pu	2.2	pu	2.2	2.2	pu	pu	2.0	1.7	pu	<u>~</u>	pu
SiO <sub>2</sub>	62.9	0.69	68.9	62.5	59.1	68.3	74.4	77.4	63.1	78.0	64.3	79.3	62.4	77.3	66.3	65.8	78.3	63.4	0.89	1.08	76.1	69.2	81.2	70.3	6.99	79.2	79.0	67.7	9.59	79.3	8.99	78.0
$Al_2O_3$	2.1	2.4	pu	3	3	2.7	pu	pu	2.3	pu	2.2	pu	2.2	pu	2.2	2.1	6.0	2.0	2.5	pu	pu	2.3	pu	2.7	2.4	pu	pu	2.3	2.3	pu	2.3	9.0
OgM	2.0	2.5	pu	pu	3.0	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	2.2	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu	pu
Ъ	35	36	37	_	7	$\sim$	4	2	9	_	8	6	0	=	12	<u>~</u>	4	15	9		<u>∞</u>	6	20	21	22	23	24	25	26	27	28	29
≥	w69.3	w69.3	w69.3	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.1	w70.I

$ZrO_2$	900.0	0.025	0.005	0.025	0.01	0.012	900.0	0.002	0.025	0.023	0.002	0.023	0.002	0.023	0.015	0.003	0.004	0.004	0.005	0.005	0.021	0.005	0.002	0.005	0.008	0.027	0.005	0.026	0.004	0.025	0.005	0.011
SrO	0.002	690.0	0.002	0.061	0.029	0.029	0.002	900'0	0.071	0.067	900'0	0.067	0.007	990.0	0.047	0.352	900.0	0.325	0.325	0.018	990.0	0.262	0.015	0.008	0.038	0.063	0.014	990.0	910.0	0.062	0.009	0.029
$Rb_2O$	pu	0.003	pu	0.003	0.014	0.015	pu	pu	0.003	0.002	pu	0.003	pu	0.003	0.004	0.00	pu	0.00	0.00	0.00	0.002	0.00	pu	0.00	0.004	0.003	pu	0.003	pu	0.002	0.001	0.015
$As_2O_3$	pu	0.147	pu	0.125	0.012	0.020	pu	pu	0.143	0.14	pu	0.137	900.0	0.14	pu	0.009	pu	0.011	0.012	0.413	0.14	pu	0.484	pu	pu	0.124	0.214	0.080	0.019	0.082	pu	pu
ZnO	0.013	0.030	0.013	0.031	0.035	0.034	0.014	pu	0.023	0.026	pu	0.034	pu	0.029	0.023	0.002	0.00	0.003	0.00	0.003	0.024	0.00	0.005	0.002	0.022	0.022	pu	0.022	0.015	0.018	0.003	0.033
CnO	0.159	0.008	0.162	0.007	0.008	0.013	0.159	pu	900.0	0.003	pu	0.005	pu	0.010	0.011	0.002	pu	pu	pu	pu	0.008	pu	0.003	pu	0.005	0.003	0.002	0.010	0.052	0.005	0.001	0.004
$Fe_2O_3$	910.0	1.346	0.021	1.197	0.478	0.494	0.018	0.184	1.314	1.268	0.177	1.273	0.167	1.278	1.40	0.442	0.149	0.650	0.476	0.245	1.086	0.428	0.225	0.207	1.030	1.466	0.259	1.482	0.921	1.456	0.186	0.488
MnO	pu	0.730	pu	909.0	0.844	0.873	pu	pu	0.677	0.679	pu	0.729	pu	0.675	0.321	0.040	pu	0.003	0.012	0.031	0.652	0.010	pu	pu	0.044	0.627	0.061	0.634	2.009	0.561	pu	0.883
$C_{aO}$	5.6	24.4	5.8	22.6	15.2	16.5	5.9	15.5	25.0	22.6	4.	23.6	16.0	23.2	23.8	0.	6.01	11.2	0.	15.2	23.8	<u>4.</u> –.	12.9	13.0	20.9	21.4	12.9	23.1	12.1	22.5	13.0	4.4
$K_2O$	2.7	3.5	2.9	3.6	8.8	8.7	3.0	pu	3.6	3.4	pu	3.3	pu	3.3	5.6	3.5	0.1	3.8	3.6		2.9	3.0	pu	9.0	5.1	2.7	pu	2.9	pu	2.9	0.5	9.5
Ū	0.5	0.3	0.5	0.3	9.0	0.3	9.0	pu	0.3	9.0	pu	0.3	pu	0.3	pu	0.5	pu	0.5	0.5	pu	0.3	0.5	pu	pu	pu	0.5	pu	9.0	pu	9.4	pu	4.0
SO3	0.2	=:	4.0	<u>4</u> .	<u>4</u> .	<u>1.5</u>	pu	0.8	9.0	3.3	6.0	0.8	0.8	<u>1.5</u>	0.8	pu	0.8	pu	0.3	6.0	pu	4.0	0.8	0.5	0.7	3.5	0.5	pu	9.0	0:	9.0	0.8
$P_2O_5$	pu	2.2	pu	<u>~</u>	2.7	2.5	pu	pu	2.0	2.6	pu	2.1	pu	2.1	2.6	<u>.</u> 5	pu	1.2	9:	pu	2.0	1.2	pu	pu	9.	2.3	pu	2.1	pu	6.	pu	3.
$SiO_2$	67.7	68.5	73.7	54.8	64.9	65.2	79.0	9.77	69.5	65.8	73.1	67.5	76.9	64.2	66.5	78.6	77.5	80.1	77.6	78.2	67.9	78.7	77.2	79.1	0.99	68.7	77.9	73.0	67.8	9.89	9.62	61.1
$Al_2O_3$	pu	2.7	pu	4.	7.	7.	pu	pu	2.5	2.1	pu	2.2	pu	2.2	2.7	=:	0.5	9.1	<u>~</u>	0.8	2.2	<u>.</u> 5	pu	<u></u>	<u></u>	2.3	9.0	2.4	9.0	2.4	<u></u>	<u>-</u> .
OgM	pu	pu	pu	pu	3.5	3.3	pu	pu	pu	pu	pu	pu	pu	pu	2.2	4.0	pu	3.9	3.9	pu	pu	3.0	pu	pu	pu	pu	pu	pu	pu	pu	pu	4.0
Ь	30	3	32	33	_	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12	<u> </u>	4	15	91	17	<u>8</u>	6	20	21	22	23	24	25	26	27	_
>	w70.1	w70.1	w70.1	w70.1	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.2	w70.3

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ZrO	0.00	0.012	0.01	0.00	0.05	0.00	0.023	0.00	0.05	0.00	0.022	0.00	0.00	0.05	0.023	0.00	0.02	0.02	0.00	0.00	0.00
SrO	0.002	0.031	0.030	0.017	0.066	0.008	0.067	0.318	0.062	0.014	0.068	0.318	0.017	0.069	0.068	0.015	0.068	0.073	0.009	0.015	0.124
$Rb_2O$	pu	910.0	0.015	pu	0.003	pu	0.003	0.00	0.003	0.00	0.003	0.00	0.00	0.002	0.003	0.00	0.003	0.003	0.00	pu	pu
$As_2O_3$	pu	0.014	0.014	0.007	0.158	pu	0.155	0.007	0.119	0.475	0.140	0.022	0.329	0.141	0.154	0.456	0.139	0.154	0.098	0.242	0.015
ZnO	0.011	0.037	0.030	0.008	0.032	pu	0.024	0.004	0.033	0.002	0.026	0.002	0.003	0.027	0.023	pu	0.029	0.030	0.003	0.003	900'0
CnO	091.0	0.011	0.008	pu	0.012	pu	900.0	pu	0.007	pu	0.008	pu	0.00	0.011	0.009	pu	0.005	0.007	pu	pu	0.001
$Fe_2O_3$	0.003	0.547	0.510	0.231	1.276	0.309	1.268	0.572	1.227	0.172	1.280	0.537	0.247	1.337	1.294	0.217	1.374	1.147	0.179	0.272	0.905
MnO	pu	698.0	0.827	pu	0.590	pu	0.712	0.015	0.706	0.019	0.664	0.017	0.047	0.628	0.689	0.003	0.677	0.720	pu	0.035	0.017
CaO	5.9	15.8	1.9	12.5	23.8	15.9	23.6	10.2	23.8	0.91	23.0	6.6	15.7	24.4	23.4	14.8	24.6	25.0	13.7	15.0	24.0
$K_2O$	2.9	0:01	8.8	0.	3.5	0.	3.2	3.6	3.5	0:	3.	3.4	6.0	3.4	3.	=	3.4	3.	9.0	0.8	9.1
D	0.7	4.0	4.0	pu	4.0	pu	0.3	4.0	4.0	pu	0.3	0.5	pu	0.3	0.3	pu	0.3	4.0	pu	pu	0.3
SO3	pu	=:	<u>.</u> 5	0.8	2.7	0.7	2.0	pu	0.7	1.2	<u>~</u>	pu	1.2	0.5	<u>~</u>	0:	0.8	0.7	9.0	1.2	2.4
$P_2O_5$	pu	3.4	2.7	pu	2.5	pu	<u>~</u>	<u></u>	2.1	pu	2.2	<u>-</u> .	pu	2.2	2.1	pu	2.1	2.3	pu	pu	pu
$SiO_2$	76.4	65.2	65.4	7.67	67.4	75.3	9.69	77.5	71.0	78.0	68.3	76.0	82.4	70.8	70.9	9.62	2.69	6.69	79.2	80.2	70.7
$Al_2O_3$	pu	<u>~</u>	.5	pu	2.5	pu	2.2	1.5	2.4	0.7	2.5	<u>-</u> .	0.7	2.5	2.6	6.0	2.6	3.0	0.	0.7	2.0
MgO	pu	4.6	3.5	pu	2.3	pu	pu	3.9	2.2	pu	pu	3.9	pu	2.8	pu	pu	2.3	pu	pu	pu	2.5
Ь	2	$\sim$	4	2	9	7	$\infty$	6	0	=	12	13	4	15	91		<u>8</u>	6	20	21	22
<b></b>	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3	w70.3













## ENGLISH HERITAGE RESEARCH DEPARTMENT

English Heritage undertakes and commissions research into the historic environment, and the issues that affect its condition and survival, in order to provide the understanding necessary for informed policy and decision making, for sustainable management, and to promote the widest access, appreciation and enjoyment of our heritage.

The Research Department provides English Heritage with this capacity in the fields of buildings history, archaeology, and landscape history. It brings together seven teams with complementary investigative and analytical skills to provide integrated research expertise across the range of the historic environment. These are:

- \* Aerial Survey and Investigation
- \* Archaeological Projects (excavation)
- \* Archaeological Science
- \* Archaeological Survey and Investigation (landscape analysis)
- \* Architectural Investigation
- \* Imaging, Graphics and Survey (including measured and metric survey, and photography)
- \* Survey of London

The Research Department undertakes a wide range of investigative and analytical projects, and provides quality assurance and management support for externally-commissioned research. We aim for innovative work of the highest quality which will set agendas and standards for the historic environment sector. In support of this, and to build capacity and promote best practice in the sector, we also publish guidance and provide advice and training. We support outreach and education activities and build these in to our projects and programmes wherever possible.

We make the results of our work available through the Research Department Report Series, and through journal publications and monographs. Our publication Research News, which appears three times a year, aims to keep our partners within and outside English Heritage up-to-date with our projects and activities. A full list of Research Department Reports, with abstracts and information on how to obtain copies, may be found on www.english-heritage. org.uk/researchreports

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